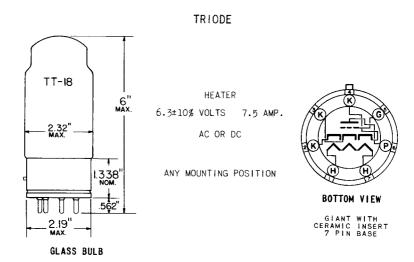
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THE 7241 IS A LONG LIFE, HIGH POWER TRIODE DEVELOPED ESPECIALLY FOR USE AS A PASSING TUBE IN THE SERIES REGULATED POWER SUPPLIES. FOR THIS SERVICE, A TUBE MUST BE ABLE TO PASS LARGE CURRENTS OVER A WIDE VOLTAGE RANGE AND STILL EXHIBIT A LOW INTRINSIC VOLTAGE DROP WHEN OPERATED "WIDE OPEN". THE 7241 ADEQUATELY MEETS THESE REQUIREMENTS. ONE TYPE 7241 CAN PASS MORE THAN ONE AMPERE AT 100 WATTS PLATE DISSIPATION.

THE 7241 FEATURES ONE LARGE ZIRCONIUM COATED GRAPHITE ANODE, WITH THREE SEPARATE GRID—CATHODES STRUCTURES. THIS ANODE, WHILE LIGHTER IN WEIGHT THAN SIMILAR METAL ANODES, REMAINS WARP FREE DURING LIFE AND PROVIDES ONE OF THE BEST GAS "GETTERING" MEANS KNOWN. THE ANODE IS SUPPORTED BY CERAMIC INSULATORS. THE USE OF THESE INSULATORS AND THE HARD GLASS ENVELOPE PERMIT THE TUBE TO BE OUTGASSED AT HIGH TEMPERATURES DURING THE MANUFACTURING EXHAUST PROCESS. THIS ALLOWS THE TUBE TO BE RUN AT HIGH TEMPERATURES DURING OPERATION, WITHOUT THE EVOLUTION OF HARMFUL GAS FROM THE TUBE PARTS.

MASSIVE CATHODES PROVIDE ADEQUATE EMISSION CURRENT RESERVE. GOLD PLATED MOLYBDENUM WIRES ARE EMPLOYED IN THE RUGGED GRID STRUCTURE. THE TUBE MOUNT IS BUILT ON A RUGGED BUTTON STEM, AND IS SUPPORTED FROM THE BULB BY MEANS OF FLEXIBLE METAL VIBRATION SNUBBERS.

IN MANY CIRCUITS, ONE 7241 CAN REPLACE FOUR TYPE 6080WA OR 6AS7G REGULATOR TUBES. FOR EVEN HIGHER LEVELS OF CURRENT OR POWER, SEVERAL 7241 TUBES CAN BE PARALLELED AS EXPLAINED IN THE APPLICATION NOTES.

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## ELECTRICAL DATA

HEATER VOLTAGE	6.3±10%	VOLTS
HEATER CURRENT (Ef = 6.3 V.)	7.5	AMP.
MINIMUM CATHODE HEATING TIME	30	SECONDS
TRANSCONDUCTANCE	40 000	$\mu$ MHOS
AMPLIFICATION FACTOR	2.7	
PLATE RESISTANCE	67	OHMS

## MECHANICAL DATA

MOUNTING POSITION	ANY			
(IF TUBE IS TO BE MOUNTED IN A HO	RIZONTAL POSITION IT IS			
RECOMMENDED THAT IT BE MOUNTED S	O THAT THE BASE LUG KEY			
BE EITHER DIRECTLY UP OR DIRECTL	Y DOWN)			
BULB	TT 18 NO	NEX		
BASE GIANT 7 PIN WITH CERAMIC				
	INSERT, JETEC #A7-17			
SOCKET E.F. JOHNS	ON #122-237 OR EQUIVALENT			
AVERAGE NET WEIGHT	6.0 οι	INCES		
MAXIMUM SHOCK RATING (NAVY HI IMPACT	SHOCK MACHINE) 450 G			
MAXIMUM VIBRATION RATING (40 TO 25 CP	s) 2.5 G			

#### RATINGS ABSOLUTE VALUES

TOTAL PLATE DISSIPATION TOTAL PLATE CURRENT DC IF TUBE VOLTAGE DROP IS TO BE SWUNG MORE CURRENT CANNOT BE REALIZED. SEE PLATE CHA			WATTS'	
CURRENT PER CATHODE (DC) PLATE VOLTAGE (DC) HEATER-CATHODE VOLTAGE (DC) GRID VOLTAGE (DC) GRID CURRENT PER GRID HEATER VOLTAGE ENVELOPE TEMPERATURE ALTITUDE FOR FULL RATINGS IF COOLING IS PROVIDED TO KEEP BULB TEMPE	 0 -300 -300  5.7  RATURE WI	400 400 +300 0 0 6.9 300 10,000	MA. VOLTS VOLTS VOLTS MA. VOLTS °C FEET	
RATINGS, ALTITUDE RATING CAN BE EXTENDED TO 60,000 FT.				
TOTAL GRID CIRCUIT RESISTANCE IN REGULATED SERVICE OR WITH FIXED BIAS	500	50,000	онмѕ	
CATHODE BIAS ONLY	500	200,000	OHMS	
RESISTANCE PER GRID LEG WHEN TUBES ARE PARALLELED	500		OHMS	
CATHODE RESISTANCE: MINIMUM CATHODE RESISTANCE PER CATHODE LEG SHALL BE 27 OHMS OR THAT RESISTANCE NECESSARY TO PRO-				

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GREATER.

VIDE 10% OF THE GRID BIAS VOLTAGE, WHICHEVER IS

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## ADDITIONAL TESTS TO INSURE RELIABILITY

RANDOMLY SELECTED SAMPLES ARE SUBJECTED TO THE FOLLOWING TESTS

SHOCK: 30° HAMMER ANGLE IN NAVY, FLYWEIGHT,

HIGH IMPACT MACHINE (450G/MSEC)

LIFE TEST: 1000 HOURS UNDER FLATE CURRENT TEST CONDITIONS

POST SHOCK AND LIFE TEST END POINTS:

PLATE CURRENT (MIN.)
TRANSCONDUCTANCE (MIN.)
HK LEAKAGE (MAX.)
GRID CURRENT (MAX.)

450 MA 27 000 μΜΗΟ 150 μΑ -12 μΑ

### RANGE OF VALUES

conditions:  $\begin{aligned} \mathbf{E}_f &= 6.3\mathbf{v}, \ \mathbf{E}_b &= 490\mathbf{v}. \\ &= \mathbf{e}_c &= 0, \ \mathbf{R}_{\mathbf{k}/\mathbf{k}} &= 200\ \Omega, \ \mathbf{R}_g &= 500\Omega \\ &= 1000\ \mathrm{Readings} \end{aligned}$  Taken after 5 minutes power preheating.

TOTAL PLATE CURRENT 495 60C MA,DC AMPLIFICATION FACTOR 2.0 3.4 TRANSCONDUCTANCE 33 000 48 000 \$\mu\$mhos heater current per tube 7.12 7.88 AMP.

conditions:  $E_f = 6.3V$ ,  $E_b = 200V$ .  $E_c = +100V$ ,  $R_k = 0$ 

CURRENT PER CATHODE 0 10 MA.

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### APPLICATION NOTES

THE 7241 IS WIDELY USED AS A "PASSING" TUBE OR SERIES REGULATOR IN CON-TROLLED POWER SUPPLIES BECAUSE OF ITS HIGH TRANSCONDUCTANCE AT RELATIVELY LOW PLATE VOLTAGES. TO PROVIDE THE DESIRED OUTPUT CURRENT, MANY TRIODE SECTIONS CAN BE PARALLELED. IF TUBE SECTIONS ARE TO BE PARALLELED, HOW-EVER, THE DESIGNER IS STRONGLY URGED TO USE SUFFICIENT RESISTANCE IN EACH CATHODE LEG TO EQUALIZE CURRENT DIVISION AMONG THE TRIODE SECTIONS. RECOMMENDED VALUES FOR VARIOUS OPERATING CURRENTS ARE SHOWN ON THE PLATE CHARACTERISTICS CURVE. IF THE OUTPUT CURRENT OF THE SUPPLY IS NOT FIXED, USE THE RESISTANCE INDICATED FOR THE LOWEST CURRENT THAT APPROACHES THE MAXIMUM PLATE DISSIPATION LINE. CATHODE RESISTANCE IS SUPERIOR TO ANODE RESISTANCE BECAUSE IT PROVIDES MORE BIAS ON THE SECTIONS TAKING GREATER PLATE CURRENT. A CATHODE RESISTOR NEED BE ONLY ONE FOURTH THE VALUE ( R ) OF A PLATE RESISTOR, AND THEREFORE WILL DISSIPATE ONLY ONE FOURTH THE POWER. IN ANY CASE, THE ONLY LOSSES INCURRED IN USING A RESISTOR IS THE INSERTION LOSS OF THE RESISTOR ITSELF (ABOUT TWO WATTS) AND THE ADDITIONAL VOLTAGE (LESS THAN 40 VOLTS) NECESSARY FROM THE UNREGULATED SUPPLY. A CATHODE RESISTOR ADDS A SMALL ADDITIONAL LOSS BY CAUSING THE PASSING TUBE TO WORK WITH HIGHER BIAS AND HENCE WITH GREATER TUBE DROP.

A THIRTY SECOND CATHODE WARMUP TIME IS RECOMMENDED BEFORE THE PLATE VOLTAGE IS APPLIED. THIS IS ESPECIALLY NECESSARY IN CIRCUITS WHERE THE AMPLIFIER TUBE PLATE RESISTOR IS RETURNED TO THE PLATE SIDE OF THE PASS-ING TUBE, AS ILLUSTRATED IN THE SIMPLIFIED CIRCUIT IN FIGURE 4. IN THIS CASE DURING WARMUP THE AMPLIFIER TUBE DRAWS LITTLE CURRENT, THERE IS LITTLE IR DROP ACROSS THE RESISTOR, AND THE GRID OF THE PASSING TURE IS EFFECTIVELY, TIED TO THE PLATE. THE PLATE WILL ATTEMPT TO DRAW EXCESSIVE CURRENT FROM THE PASSING TUBE'S CATHODE AND MAY SERIOUSLY IMPAIR TUBE LIFE. THE CIRCUIT IN FIGURE 2 IS PREFERABLE FROM THE CONSIDERATION OF THE SAFETY OF THE PASSING TUBE BOTH DURING WARMUP AND IN THE EVENT OF TROUBLE IN THE AMPLIFIER CIRCUIT OR IF THE AMPLIFIER TUBE IS REMOVED FROM ITS SOCKET. IT HAS THE ADDITIONAL ADVANTAGE OF PROVIDING A CONSTANT VOLTAGE FOR THE AMPLIFIER CIRCUIT. HOWEVER, IF THE REGULATOR OUTPUT IS LOW (BELOW 250 VOLTS) IT WILL BE NECESSARY TO PROVIDE ADDITIONAL NEGA-TIVE VOLTAGE FOR THE REFERENCE TUBE CIRCUIT. ALSO, IF THE REGULATED OUT-PUT VOLTAGE IS TO BE VARIABLE, IT MAY BE NECESSARY TO FOLLOW FIGURE 1.

PASSING TUBE OPERATION CONDITIONS SHOULD BE CHOSEN TO PROVIDE AS LOW A TUBE DROP AS POSSIBLE. A SAFETY MARGIN OF AT LEAST 5 VOLTS FROM THE ZERO BIAS LINE SHOULD BE ALLOWED HOWEVER, FOR VARIATIONS OF INDIVIDUAL TUBES, SUFFICIENT BIAS EXCURSION SHOULD BE ALLOWED FOR OVERCOMING RIPPLE. THE AMPLIFIER CIRCUIT SHOULD BE ABLE TO COUNTERACT THE EFFECT OF UNBALANCE DUE TO TUBE AGING.

A GRID RESISTOR SHOULD BE USED FOR EACH TRIODE SECTION. THIS SHOULD BE ENOUGH TO PREVENT PARASITIC OSCILLATION BUT NOT LARGE ENOUGH TO PREVENT LOSS OF CONTROL DUE TO A SMALL AMOUNT OF "GAS" GRID CURRENT. A VALUE OF GRID RESISTANCE THAT MEETS BOTH THESE CONDITIONS IS 1,000 0HMS. HEATER VOLTAGE SHOULD BE KEPT AS CLOSE AS POSSIBLE TO 6.3 VOLTS AS MEASURED ON THE TUBE PINS. WHEN CONNECTING MANY HIGH DRAIN TUBE HEATERS ACROSS A SINGLE TRANSFORMER, BUS BARS FEEDING FROM "ALTERNATE ENDS" (FIGURE 3) SHOULD BE USED WITH A STRANDED PAIR FEEDING INDIVIDUAL SOCKETS.

