

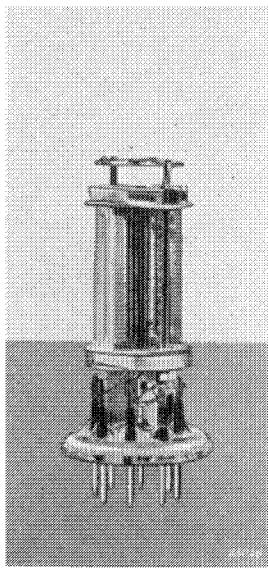
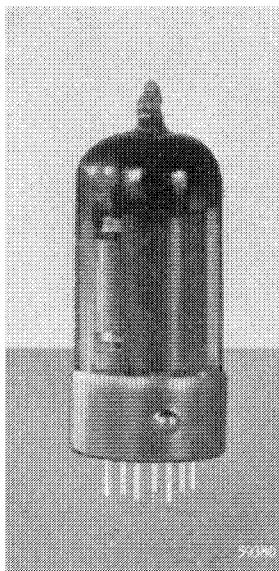
**UF 41 Variable-mu R.F. pentode**

Fig. 1  
The UF 41, showing the electrode system (approximately actual size).

The UF 41 is a variable-mu pentode employing sliding screen grid voltage. It is intended for I.F. and R.F. amplification. At the working point, the mutual conductance is 2.2 mA/V at an applied voltage of 170 V, or 1.9 mA/V at 100 V. Since the heater current of the valve is 100 mA, the heater can be connected in series with the heaters of other U-type Rimlock valves. As the characteristics of the UF 41 are wholly identical with those of the EF 41, reference may be made to the description of the latter for further particulars.

**TECHNICAL DATA OF THE R.F. PENTODE UF 41****Heater data**

Heating : indirect, A.C. or D.C., series feed

Heater current . . . . .	$I_f$	=	100 mA
Heater voltage . . . . .	$V_f$	=	12.6 V

**Capacitances (cold valve)**

Input capacitance . . . . .	$C_{g1}$	=	5.3 pF
Output capacitance . . . . .	$C_a$	=	5.9 pF
Anode - control grid . . . . .	$C_{ag1}$	<	0.002 pF
Heater - control grid . . . . .	$C_{g1f}$	<	0.05 pF

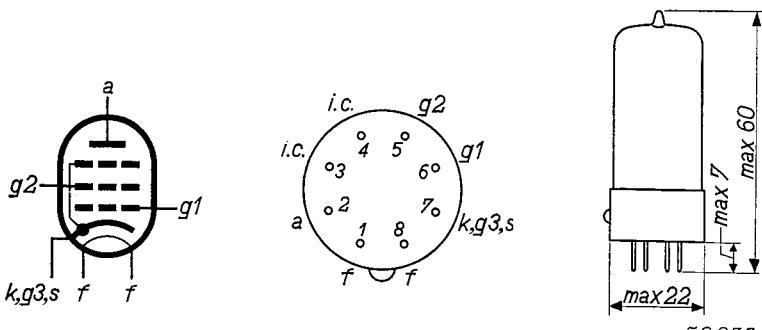


Fig. 2

Electrode arrangement, electrode connections and maximum dimensions in mm of the UF 41.

### Operating characteristics of the UF 41 used as R.F. or I.F. amplifier (see Figs. 6 and 7)

#### A. With fixed screen grid voltage

Anode voltage . . . . .	$V_a$	=	100	V
Screen grid voltage . . . . .	$V_{g2}$	=	100	V
Bias resistor . . . . .	$R_k$	=	325	$\Omega$
Grid bias . . . . .	$V_{g1}$	=	$\overbrace{-2.5}^{} - \overbrace{16.5}^{}$	V
Anode current . . . . .	$I_a$	=	6.0	— mA
Screen grid current . . . . .	$I_{g2}$	=	1.75	— mA
Mutual conductance . . . . .	$S$	=	2200	$22 \mu\text{A/V}$
Internal resistance . . . . .	$R_i$	=	0.6	$> 10 \text{ M}\Omega$
Equivalent noise resistance . . . . .	$R_{eq}$	=	6.5	— k $\Omega$
Amplification factor, grid 2 with respect to grid 1 . . . . .	$\mu_{g2g1}$	=	18	—

#### B. With sliding screen grid voltage

Anode and supply voltage . . .	$V_a = V_b =$	100	170	V
Screen grid series resistor . . .	$R_{g2}$	=	40	$40 \text{ k}\Omega$
Bias resistor . . . . .	$R_k$	=	325	$\Omega$
Grid bias . . . . .	$V_{g1}$	=	$\overbrace{-1.4}^{} - \overbrace{17}^{}$	$\overbrace{-2.5}^{} - \overbrace{28}^{}$ V
Anode current . . . . .	$I_a$	=	3.3	— mA
Screen grid current . . . . .	$I_{g2}$	=	1.0	— mA
Mutual conductance . . . . .	$S$	=	1900	$19 \text{ } 2200 \text{ } 22 \mu\text{A/V}$
Internal resistance . . . . .	$R_i$	=	0.8	$> 10 \text{ M}\Omega$
Equivalent noise resistance . . . . .	$R_{eq}$	=	5.5	— k $\Omega$
Amplification factor, grid 2 with respect to grid 1 . . . . .	$\mu_{g2g1}$	=	18	— 18

## UF 41

Anode and supply voltage . . .	$V_a = V_b$	=	200	V
Screen grid series resistor . . .	$R_{g2}$	=	40	kΩ
Bias resistor . . . . .	$R_k$	=	325	Ω
Grid bias . . . . .	$V_{g1}$	=	-3	-34 V
Anode current . . . . .	$I_a$	=	7.2	— mA
Screen grid current . . . . .	$I_{g2}$	=	2.1	— mA
Mutual conductance . . . . .	$S$	=	2300	23 μA/V
Internal resistance . . . . .	$R_i$	=	1.0	>10 MΩ
Equivalent noise resistance . . .	$R_{eq}$	=	7.0	kΩ
Amplification factor, grid 2 with respect to grid 1 . . . . .	$\mu_{g2g1}$	=	18	—

**Operating characteristics of the UF 41 used as R.F. or I.F. amplifier,** with screen grid, together with that of frequency changer UCH 41 fed by means of a common potentiometer

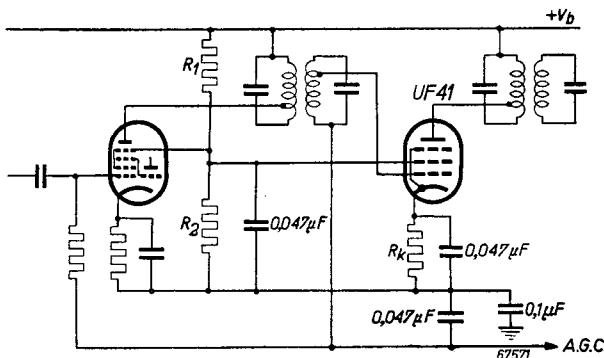


Fig. 3

Anode and supply voltage . . .	$V_a = V_b =$	100	170	V
Potentiometer for screen grid supply . . . . .	$\left\{ \begin{array}{l} R_1 = 12 \\ R_2 = 27 \end{array} \right.$	12	12	kΩ
Bias resistor . . . . .	$R_k = 235$	235	235	Ω
Grid bias . . . . .	$V_{g1} = -1.0$	-12	-1.8	-20 V
Screen grid voltage . . . . .	$V_{g2} = 53$	69	87	117 V
Anode current . . . . .	$I_a = 3.3$	—	6.0	— mA
Screen grid current . . . . .	$I_{g2} = 1.0$	—	1.75	— mA
Mutual conductance . . . . .	$S = 1900$	19	2200	22 μA/V
Internal resistance . . . . .	$R_i = 0.8$	>10	1.0	>10 MΩ
Equivalent noise resistance . . .	$R_{eq} = 5.5$	—	6.5	kΩ
Amplification factor, grid 2 with respect to grid 1 . . . . .	$\mu_{g2g1} = 18$	—	18	—

**Limiting values**

Anode voltage, with valve biased to cut-off . . . . .	$V_{a_0}$	= max. 550 V
Anode voltage . . . . .	$V_a$	= max. 250 V
Anode dissipation . . . . .	$W_a$	= max. 2 W
Screen grid voltage, valve biased to cut-off . . . . .	$V_{g2_0}$	= max. 550 V
Screen grid voltage, valve con- trolled . . . . .	$V_{g2}(I_a < 4\text{mA})$	= max. 250 V
Screen grid voltage, valve uncon- trolled . . . . .	$V_{g2}(I_a = 7.2\text{mA})$	= max. 150 V
Screen grid dissipation . . . . .	$W_{g2}$	= max. 0.3 W
Cathode current . . . . .	$I_k$	= max. 10 mA
Grid current starting point . . . . .	$V_{g1}(I_{g1} = +0.3\mu\text{A})$	= max. -1.3 V
External resistance between grid 1 and cathode . . . . .	$R_{g1}$	= max. $3 \text{ M}\Omega^1)$
External resistance between heater and cathode . . . . .	$R_{fk}$	= max. $20 \text{ k}\Omega$
Voltage between heater and cathode . . . . .	$V_{fk}$	= max. 150 V

<sup>1)</sup> This value is applicable where grid bias is obtained from a cathode resistor.

# UF 41

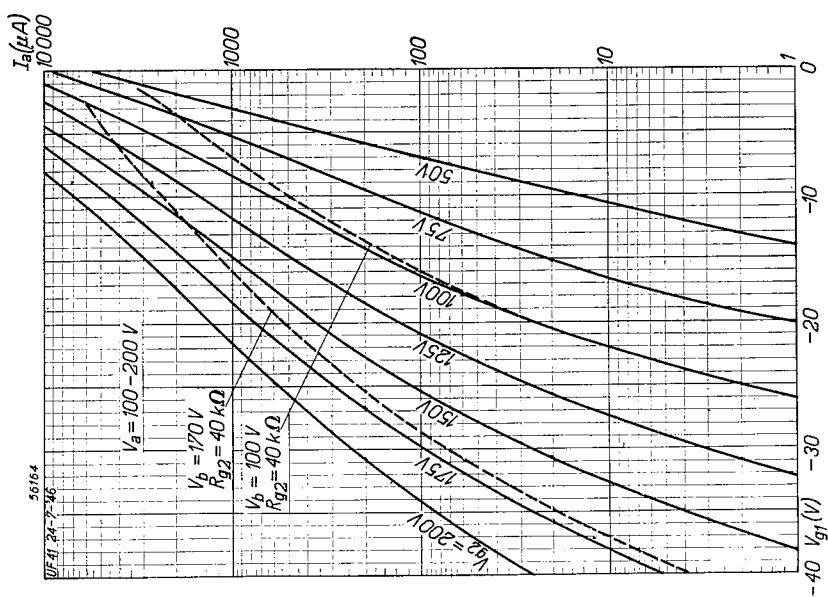
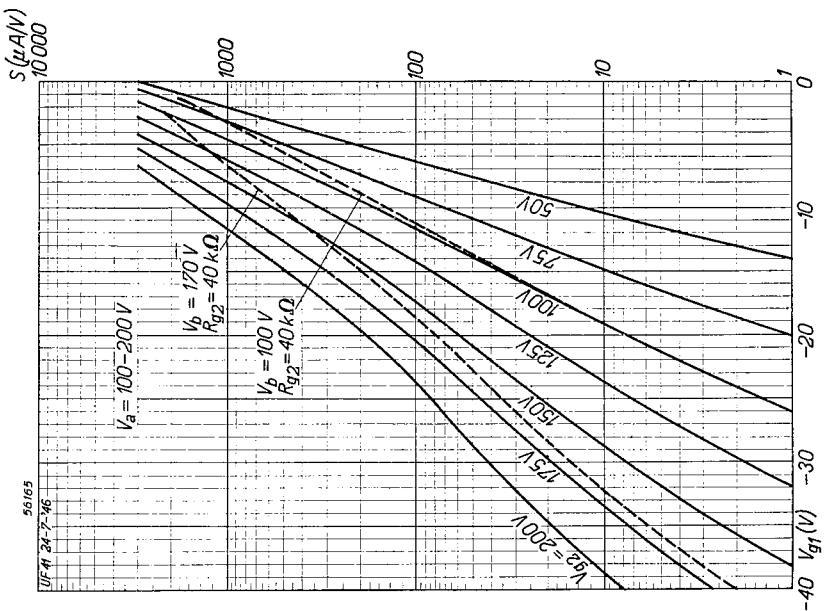


Fig. 4  
Anode current ( $I_a$ , Fig. 4) and mutual conductance ( $S$ , Fig. 5) of the UF 41 as functions of the grid bias voltages ( $V_g$ ). The dotted lines represent the anode current and mutual conductance with a series resistor ( $R_{g2}$ ) of  $40 \text{ k}\Omega$  in the screen grid circuit, at supply voltages of  $100 \text{ V}$  and  $170 \text{ V}$ .

Fig. 5  
Fig. 5 of the UF 41  
lines represent the anode current and mutual conductance with a series resistor ( $R_{g2}$ ) of  $40 \text{ k}\Omega$  in the screen grid circuit, at supply voltages of  $100 \text{ V}$  and  $170 \text{ V}$ .

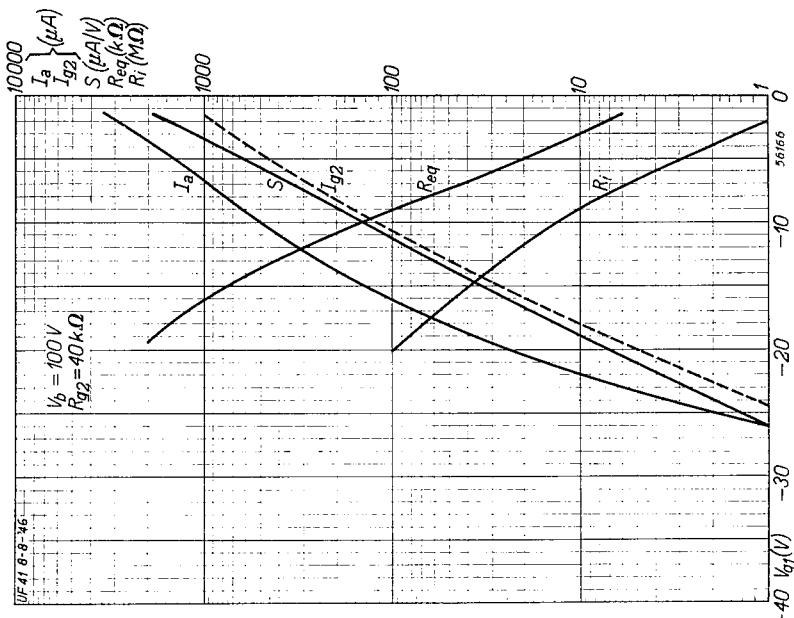
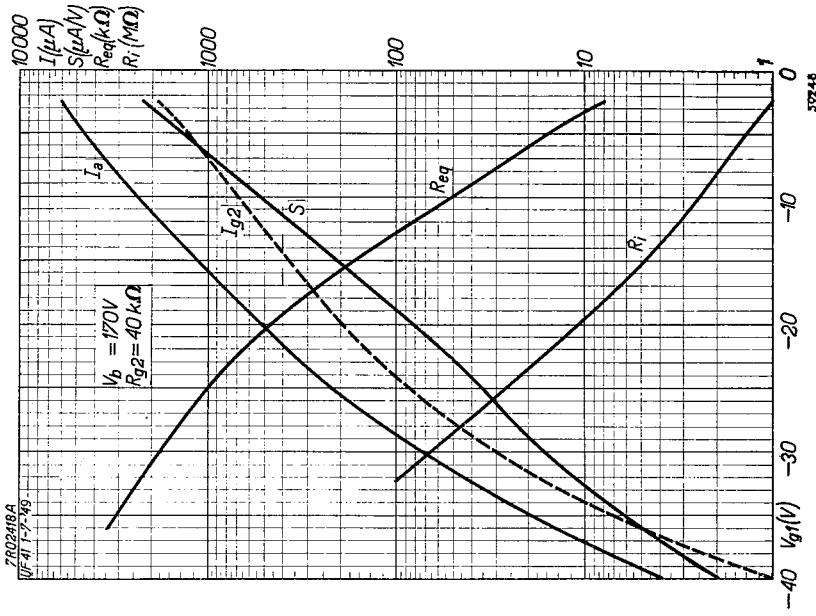


Fig. 6  
Anode current ( $I_a$ ), screen grid current ( $I_{g2}$ ), mutual conductance ( $S$ ), internal resistance ( $R_i$ ) and equivalent noise resistance ( $R_{eq}$ ) as functions of the grid bias ( $V_{g1}$ ); screen grid series resistor  $R_{g2} = 40 \text{ k}\Omega$ , supply voltage  $V_b = 100 \text{ V}$  (Fig. 7), and  $170 \text{ V}$  (Fig. 7).

Fig. 7  
Mutual conductance ( $S$ ), internal resistance ( $R_i$ ) and equivalent noise resistance ( $R_{eq}$ ) as functions of the grid bias ( $V_{g1}$ ); screen grid series resistor  $R_{g2} = 40 \text{ k}\Omega$ , supply voltage  $V_b = 100 \text{ V}$  (Fig. 6) and  $170 \text{ V}$  (Fig. 7).

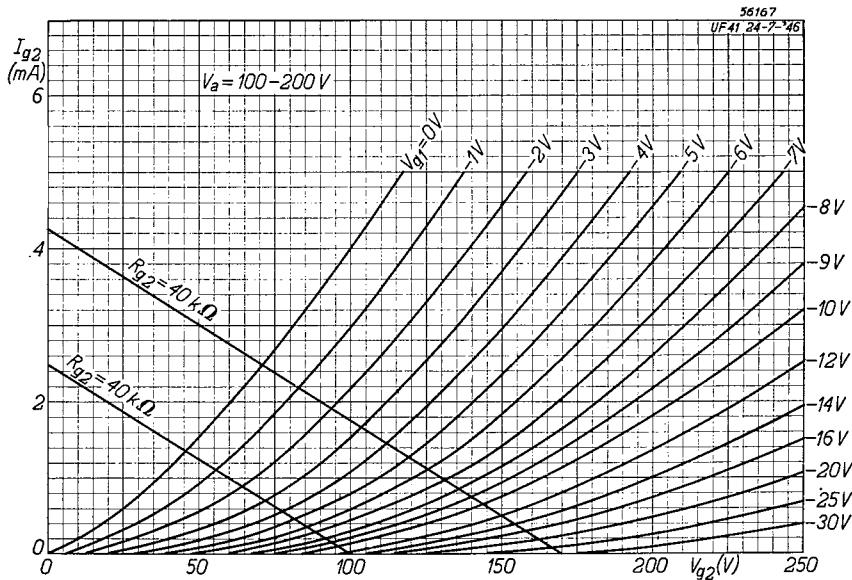
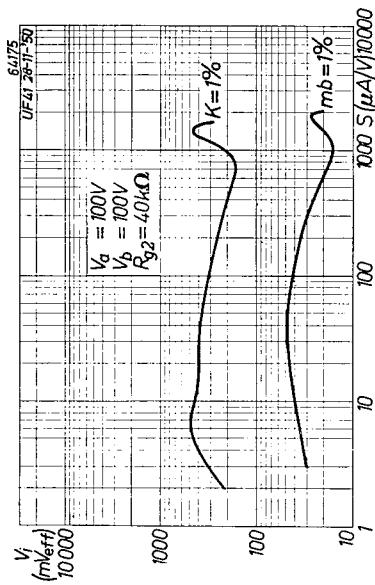
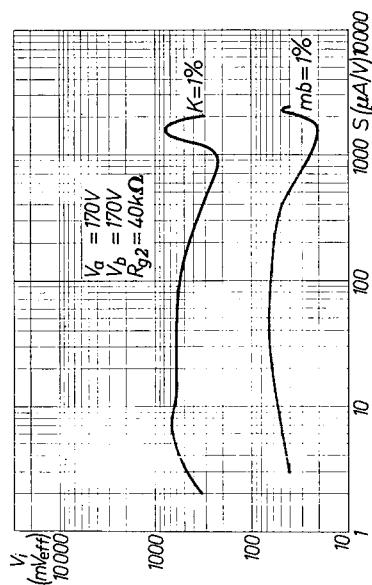


Fig. 8

Screen grid current ( $I_{g2}$ ) of the UF 41 as a function of the screen grid voltage ( $V_{g2}$ ) with grid bias ( $V_{g1}$ ) as parameter. The straight lines are applicable with  $40\text{ k}\Omega$  series resistor in the screen grid circuit, with a supply voltage of 100 and 170 V.



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The graph shows the effective voltage  $V_{eff}$  of an interfering signal at the control grid of the UF 41, producing  $1\%$  cross-modulation (curve  $K = 1\%$ ); also the effective voltage ( $V_{eff}$ ) of a ripple signal at the control grid, causing  $1\%$  modulation hum (curve  $m_b = 1\%$ ). Both as function of the slope  $S$ .