

UCH 42 Triode-hexode frequency changer

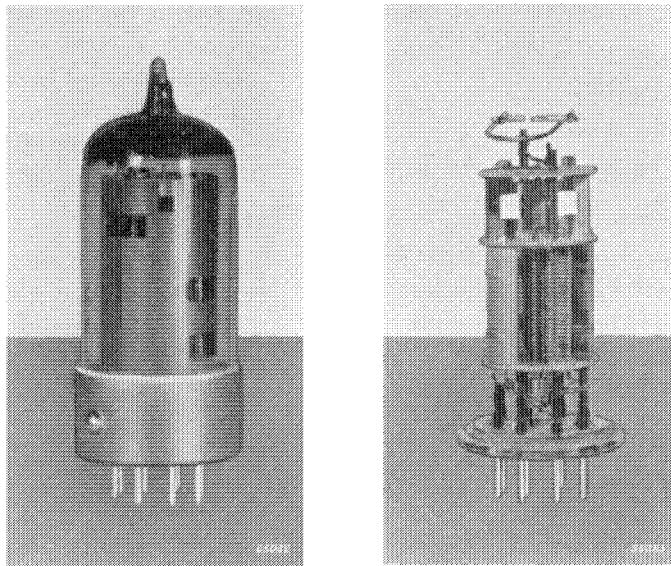


Fig. 1
The UCH 42, showing the electrode system (approximately actual size).

The triode-hexode UCH 42 is a frequency changer with a conversion conductance of 670 $\mu\text{A}/\text{V}$ at an applied voltage of 170 V, or 530 $\mu\text{A}/\text{V}$ at 100 V. It is designed for A.C./D.C. receivers in which the heaters, connected in series, take a current of 100 mA.

Further particulars will be found in the description of the ECH 42, the corresponding E-type valve.

TECHNICAL DATA OF THE TRIODE-HEXODE UCH 42

Heater data

Heating : indirect, A.C. or D.C., series feed

Heater current	I_f	=	100 mA
Heater voltage	V_f	=	14 V

Capacitances (measured on cold valve)

Hexode section

Input capacitance	C_{g1}	=	4.0 pF
Output capacitance	C_a	=	9.4 pF
Anode - control grid	C_{ag_1}	<	0.1 pF
Heater - control grid	C_{g1f}	<	0.15 pF

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Triode section

Input capacitance	C_{gT+g3}	=	5.9 pF
Output capacitance	C_a	=	2.4 pF
Anode - grid	$C_{(gT+g3)a}$	=	1.3 pF

Between triode and hexode sections

Hexode control grid - triode grid	$C_{g1H-(gT+g3)}$	<	0.35 pF
Hexode anode - triode grid	$C_{aH-(gT+g3)}$	<	0.2 pF

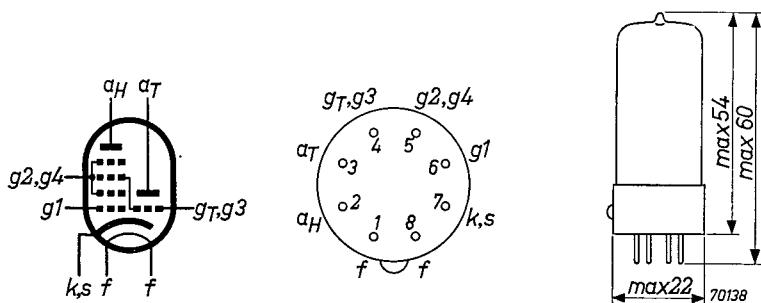


Fig. 2
Electrode arrangement, electrode connections and maximum dimensions in mm of the UCH 42.

Operating characteristics of the hexode section used as frequency changer
(screen grids fed by means of a potentiometer, see Figs. 6 to 15 incl.)

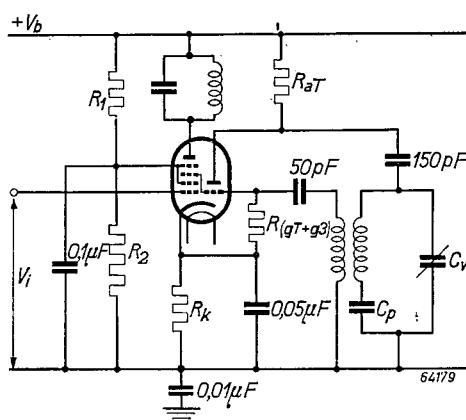


Fig. 3

Anode and supply voltage . . .	$V_a = V_b =$	100	170	V
Resistor between supply voltage and screen grids	R_1 =	18	18	kΩ
Resistor between screen grids and chassis	R_2 =	27	27	kΩ
Bias resistor	R_k =	180	180	Ω
Oscillator grid leak	R_{gT+g3} =	22	22	kΩ
Oscillator grid current	I_{gT+g3} =	175 ¹⁾	350 ¹⁾	μA
Grid bias	V_{g1} =	—1.0 —13.5	—1.85 —25	V
Screen grid voltage	V_{g2+g4} =	43 57	70 100	V
Anode current	I_a =	1.2 —	2.1 —	mA
Screen grid current	I_{g2+g4} =	1.46 —	2.6 —	mA
Conversion conductance	S_c =	530 5.3	670 6.7	μA/V
Internal resistance	R_i =	>1 >5	>1 >5	MΩ
Equivalent noise resistance	R_{eq} =	50 —	85 —	kΩ
Anode and supply voltage	$V_a = V_b =$	200	200	V
Resistor between supply voltage and screen grids	R_1 =	18	18	kΩ
Resistor between screen grids and chassis	R_2 =	27	27	kΩ
Bias resistor	R_k =	180	180	Ω
Oscillator grid leak	R_{gT+g3} =	22	22	kΩ
Oscillator grid current	I_{gT+g3} =	350 ¹⁾	350 ¹⁾	μA
Grid bias	V_{g1} =	—2 —27.5	—2 —27.5	V
Screen grid voltage	V_{g2+g4} =	85 119	85 119	V
Anode current	I_a =	3.0 —	3.0 —	mA
Screen grid current	I_{g2+g4} =	3.0 —	3.0 —	mA
Conversion conductance	S_c =	750 7.5	750 7.5	μA/V
Internal resistance	R_i =	>1 >5	>1 >5	MΩ
Equivalent noise resistance	R_{eq} =	100 —	100 —	kΩ

Typical characteristics of the triode section (see Figs. 17 and 18)

Anode voltage	V_a	=	100	V
Grid voltage	V_{gT+g3}	=	0	V
Anode current	I_a	=	10	mA
Mutual conductance	S	=	2.8	mA/V
Amplification factor	μ	=	22	

¹⁾ If the grid leak R_{gT+g3} equals 47 kΩ, the recommended value for I_{gT+g3} is 200 μA for supply voltages of 200 and 170 V, and 100 μA for a supply voltage of 100 V.

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Operating characteristics of the triode section used as oscillator
(see Figs. 19 to 22 incl.)

Supply voltage . . .	V_b	=	100	170	200	V
Anode resistor . . .	R_a	=	10	10	22	kΩ
Oscillator voltage . . .	V_{osc}	=	4	8	8	V_{RMS}
Oscillator grid leak . . .	R_{gT+g_3}	=	22	47	22	kΩ
Oscillator grid current . . .	I_{gT+g_3}	=	175	100	350	200 μA
Anode current . . .	I_a	=	3.4	3.1	6.5	5.7 mA
Effective slope . . .	S_{eff}	=	0.7	0.6	0.75	0.65 mA/V

Operating characteristics of the UCH 42 used as phase inverter

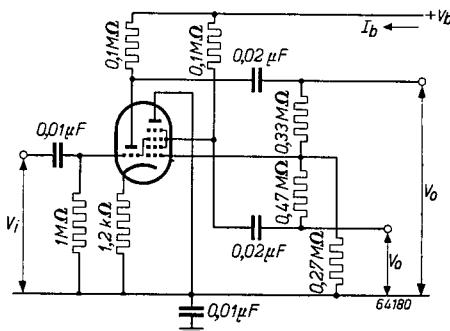


Fig. 4.

Supply voltage V_b (V)	Total current I_b (mA)	Amplification V_o/V_i	Distortion (%) at an output voltage of	
			5 V_{RMS}	10 V_{RMS}
100	1.4	11	1.9	—
165	2.4	11	1.5	1.6

Operating characteristics of the hexode section used as frequency changer, with screen grids, together with that of the UAF 42, fed by means of a common potentiometer (see Figs. 23 to 25 incl.)

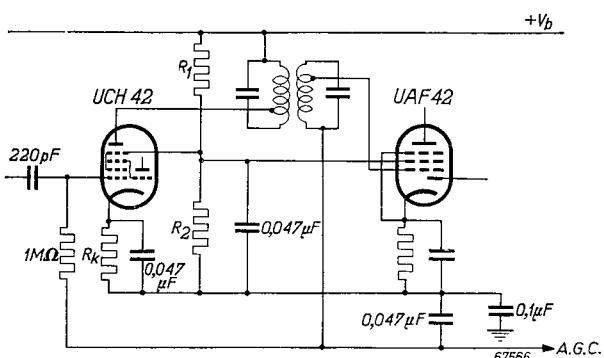


Fig. 5

Anode and supply voltage . . .	$V_a = V_b =$	100	170	V
Resistor between supply voltage and screen grids	R_1	=	15	kΩ
Resistor between screen grids and chassis	R_2	=	22	kΩ
Bias resistor	R_k	=	180	Ω
Oscillator grid leak	R_{gT+g3}	=	22	kΩ
Oscillator grid current	I_{gT+g3}	=	175 ¹⁾	μA
Grid bias	V_{g1}	=	-1.0 -9.6 -1.8 -15.5	V
Screen grid voltage	V_{g2}	=	43 58 70 99	V
Anode current	I_a	=	1.2 — 2.1	mA
Screen grid current	I_{g2+g4}	=	1.46 — 2.6	mA
Conversion conductance	S_c	=	530 14 670 20	$\mu A/V$
Internal resistance	R_i	=	>1 >2 >1 >4	MΩ
Equivalent noise resistance	R_{eq}	=	60 — 66	kΩ

Limiting values of the hexode section

Anode voltage, cut-off condition	V_{a_0}	= max.	550	V
Anode voltage	V_a	= max.	250	V
Anode dissipation	W_a	= max.	1.5	W
Screen grid voltage, cut-off condition	$V_{(g2+g4)_c}$	= max.	550	V
Screen grid voltage, valve con- trolled	$V_{g2+g4}(I_a < 1mA)$	= max.	250	V
Screen grid voltage, valve un- controlled	$V_{g2+g4}(I_a = 3mA)$	= max.	125	V
Screen grid dissipation . . .	W_{g2+g4}	= max.	0.3	W
Grid current starting point . .	$V_{g1}(I_{g1} = +0.3\mu A)$	= max.	-1.3	V
Cathode current	I_k	= max.	10	mA
External resistance between grid 1 and cathode	R_{g1}	= max.	3	$M\Omega^2)$
External resistance between grid 3 and cathode	R_{g3}	= max.	3	MΩ
External resistance between heater and cathode	R_{hk}	= max.	20	kΩ
Voltage between heater and cathode	V_{hk}	= max.	150	V

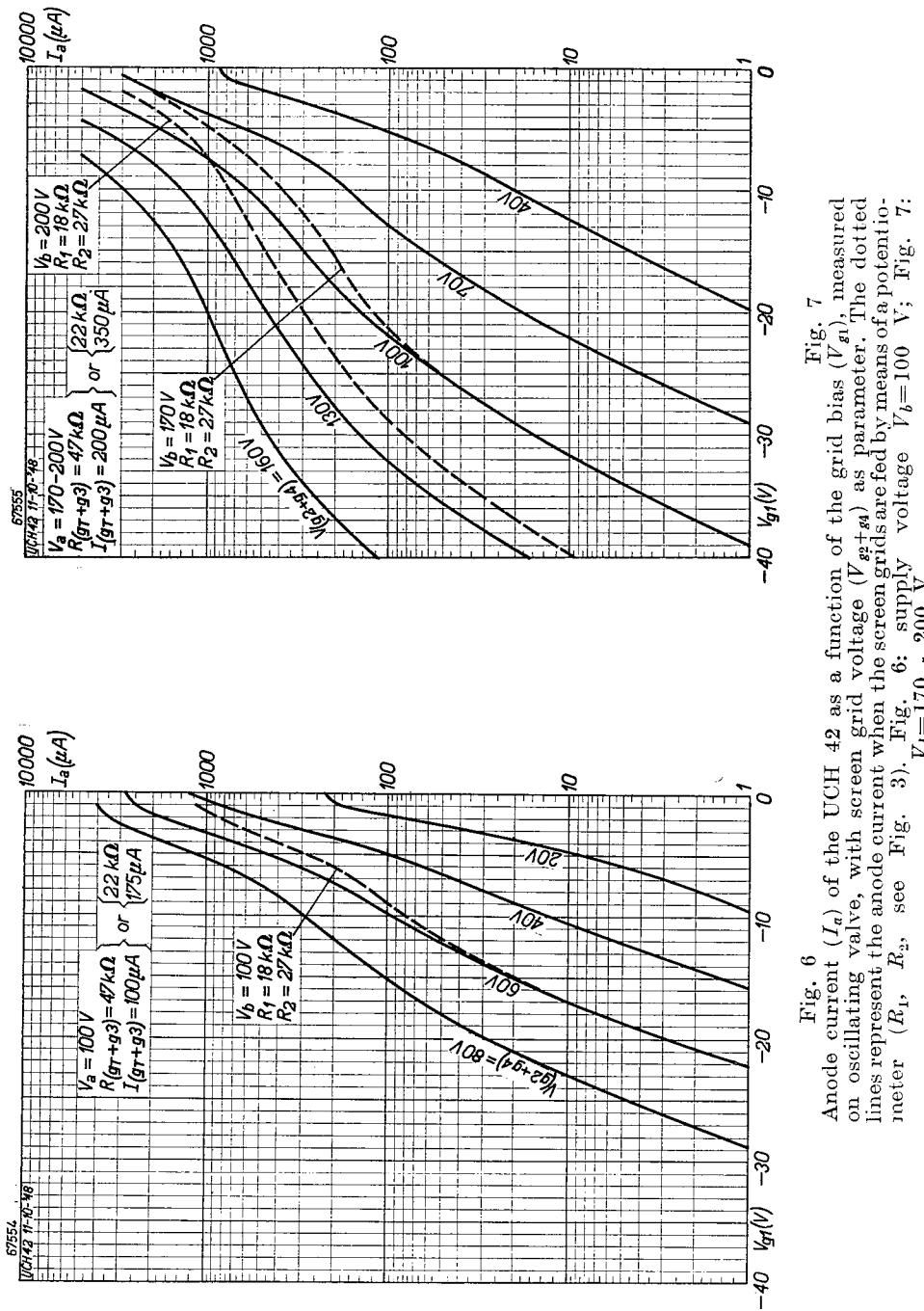
¹⁾ See note on page 213.

²⁾ This value is applicable where the grid bias is derived from a cathode resistor.

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Limiting values of the triode section

Anode voltage, cut-off condition	V_{a_0}	= max. 550 V
Anode voltage	V_a	= max. 175 V
Anode dissipation	W_a	= max. 0.8 W
Grid current starting point . . .	$V_g (I_g = +0.3\mu A)$	= max. -1.3 V
Cathode current	I_k	= max. 6 mA
External resistance between grid and cathode	R_g	= max. 3 MΩ
External resistance between heater and cathode	R_{fk}	= max. 20 kΩ
Voltage between heater and cathode	V_{fk}	= max. 150 V



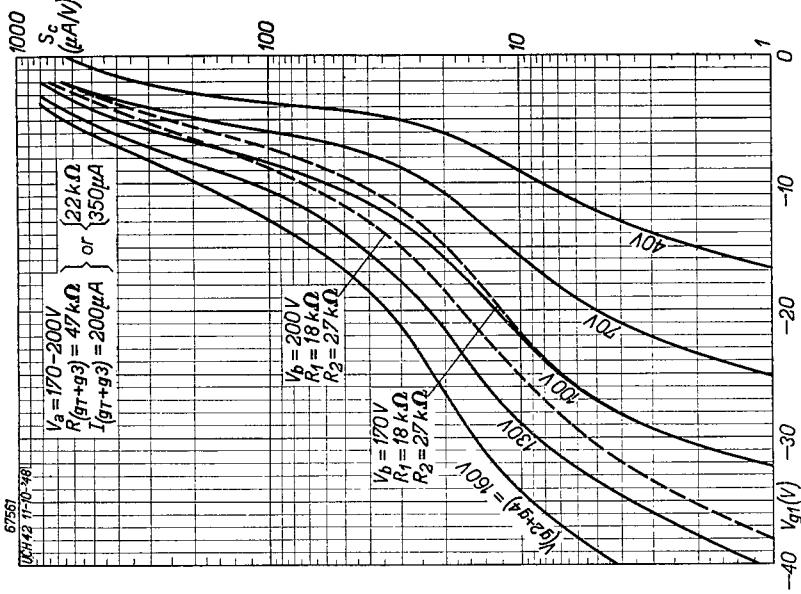
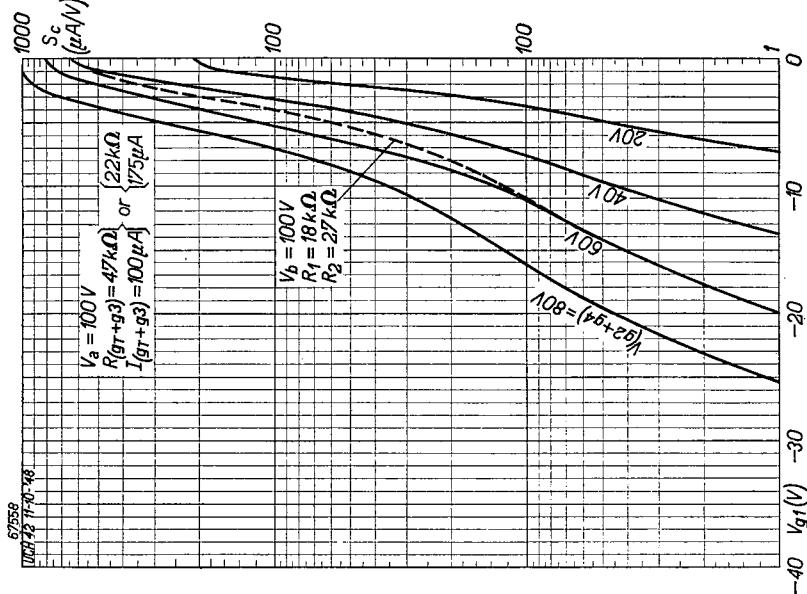


Fig. 8
Conversion conductance (S_c) of UCH 42 in oscillating condition, as a function of the grid bias (V_{g1}) with screen grid voltage (V_{g2+g3}) as parameter. The dotted lines indicate the conversion conductance when the screen grid voltage is derived from a potentiometer (R_1, R_2 in Fig. 3).

Fig. 9
Fig. 9
Conversion conductance (S_c) of UCH 42 in oscillating condition, as a function of the grid bias (V_{g1}) with screen grid voltage (V_{g2+g3}) as parameter. The dotted lines indicate the conversion conductance when the screen grid voltage is derived from a potentiometer (R_1, R_2 in Fig. 3). Fig. 8 : supply voltage $V_b = 100V$; Fig. 9 : $V_b = 170 - 200V$.

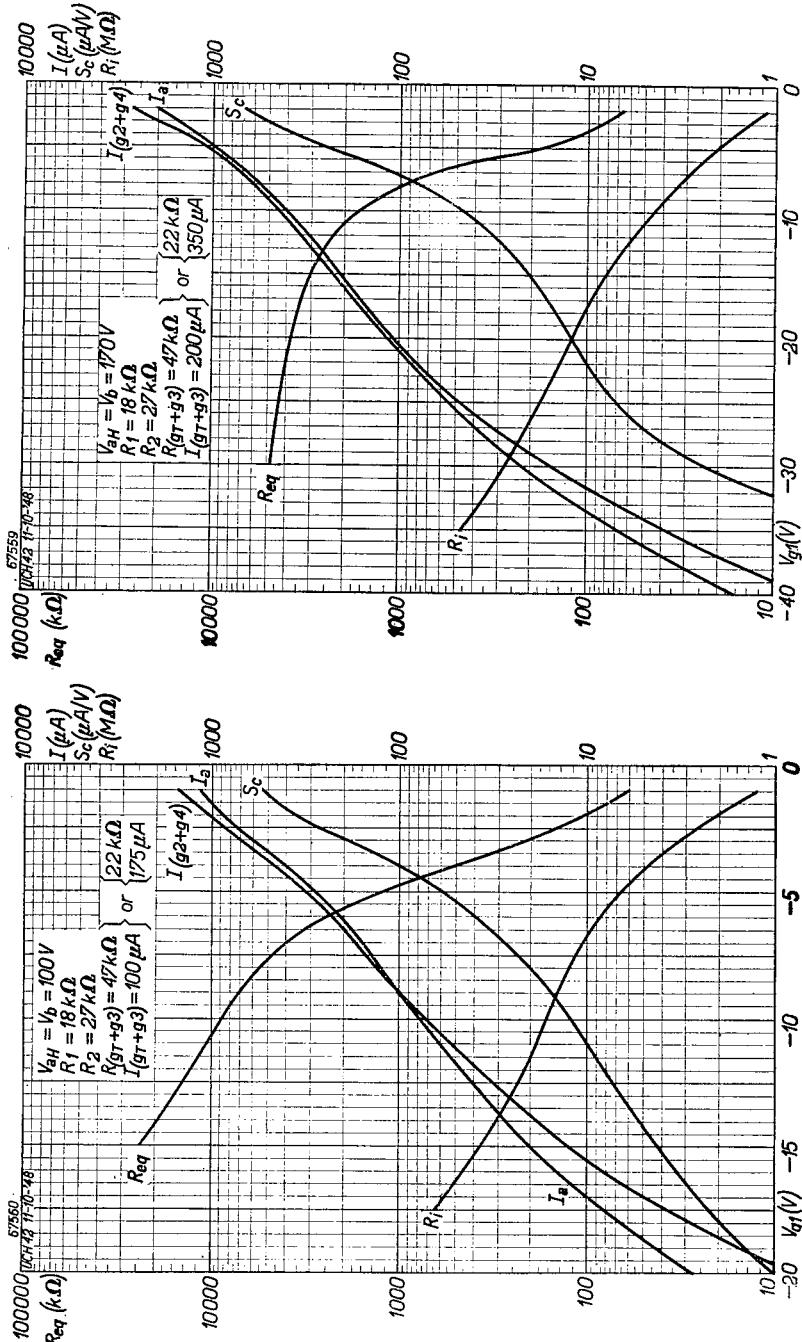


Fig. 10
Anode current (I_a), screen grid current (I_{g2+g4}), conversion conductance (S_c), internal resistance (R_i) and equivalent noise resistance (R_{eq}) of the UCH 42 in oscillating condition, as functions of the grid bias (V_g). Measured in the circuit shown in Fig. 3. Fig. 10 : supply voltage $V_b = 100V$. Fig. 11 : $V_b = 170V$.

Fig. 11
 I_a , conversion conductance (S_c), measured in the circuit shown in Fig. 3. Fig. 11 : $V_b = 170V$.

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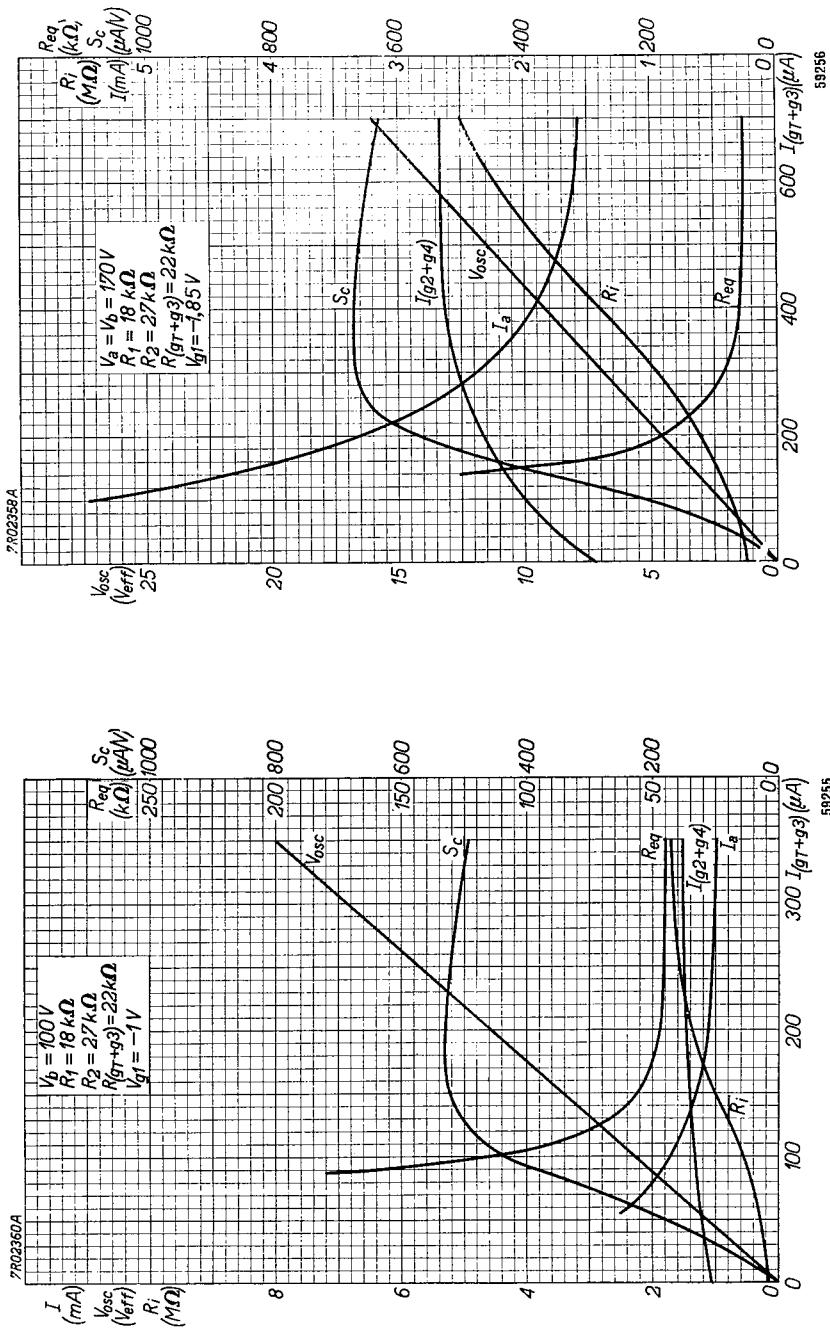
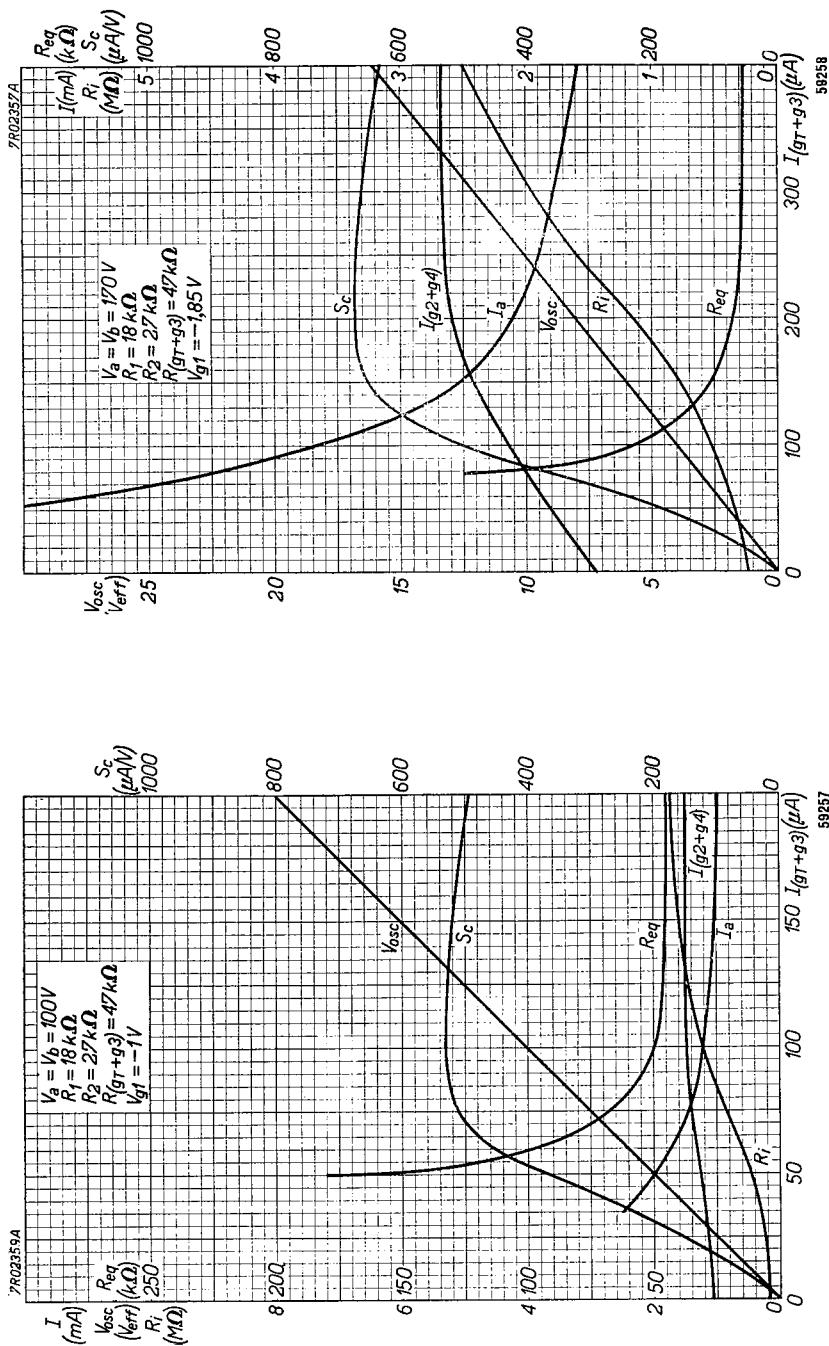


Fig. 12
Anode current (I_a), conversion conductance (S_c), oscillator voltage (V_{osc}), internal resistance (R_i) and equivalent noise resistance (R_{eq}) of the UCH 4.2 as functions of the oscillator grid current (I_{gr+g3}) for a grid leak R_{gr+g3} of 22 k Ω . Measured in the circuit shown in Fig. 3. Fig. 12 : supply voltage $V_b = 100\text{ V}$; Fig. 13 : $V_b = 170\text{ V}$.

Fig. 13
Anode current (I_a), conversion conductance (S_c), oscillator voltage (V_{osc}), internal resistance (R_i) and equivalent noise resistance (R_{eq}) of the UCH 4.2 as functions of the oscillator grid current (I_{gr+g3}) for a grid leak R_{gr+g3} of 22 k Ω . Measured in the circuit shown in Fig. 3. Fig. 12 : supply voltage $V_b = 100\text{ V}$; Fig. 13 : $V_b = 170\text{ V}$.



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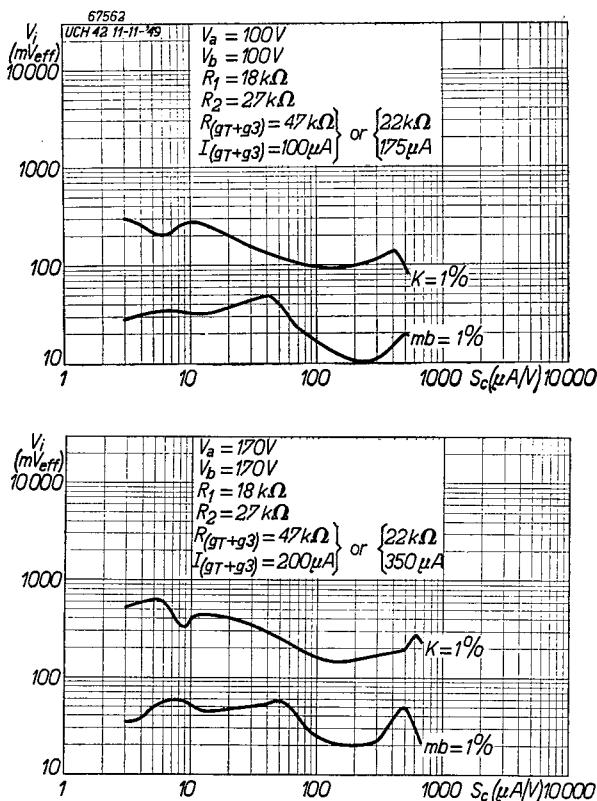


Fig. 16

- 1) The effective voltage (V_i) of an interfering signal at the control grid of the UCH 42 producing 1% cross modulation (curve $K=1\%$) and
- 2) the effective voltage (V_i) of a ripple signal at the control grid producing 1% modulation hum (curve $mb=1\%$), both as function of the conversion conductance S_c and measured in the circuit shown in Fig. 3. Upper figure: supply voltage $V_b = 100$ V; lower figure: $V_b = 170$ V.

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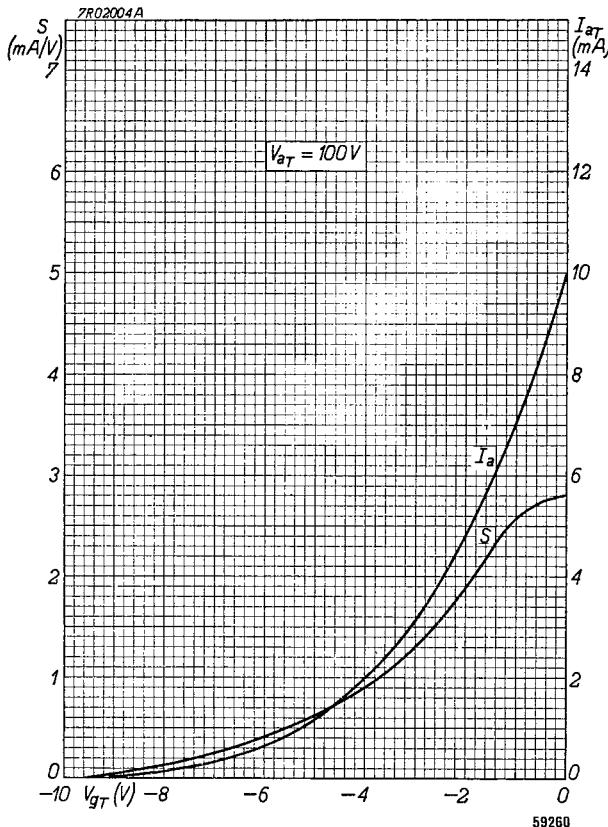


Fig. 17
 I_a/V_g and S/V_g characteristics of the triode section of the UCH 42.

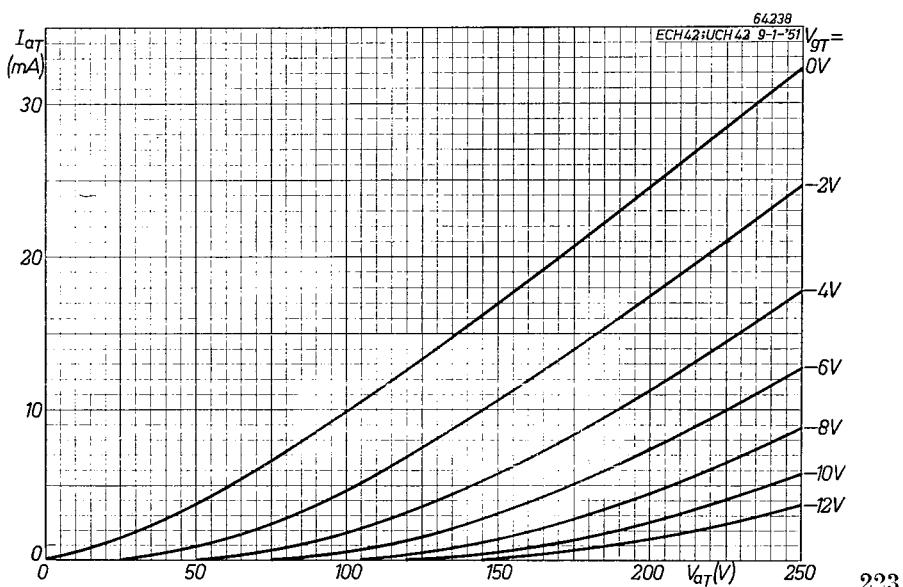


Fig. 18
 I_a/V_a characteristics relative to the triode section of the UCH 42.

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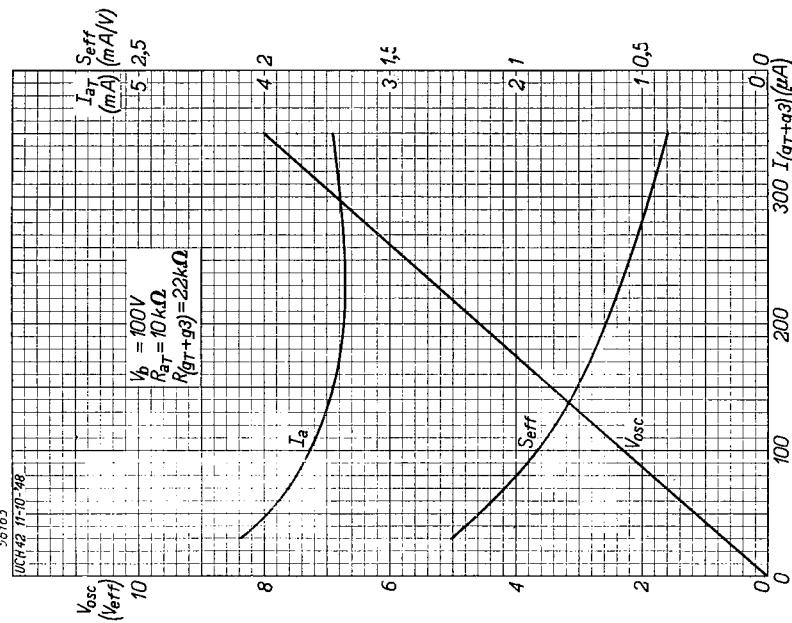


Fig. 19

Anode current (I_a), oscillator voltage (V_{osc}) and effective slope (S_{eff}) of the triode section of the UCH 42 as functions of the oscillator grid current (I_{gr+g3}), with grid leak (R_{gr+g3}) of 22 k Ω . Fig. 19: supply voltage $V_b = 100$ V; Fig. 20: $V_b = 170$ V.

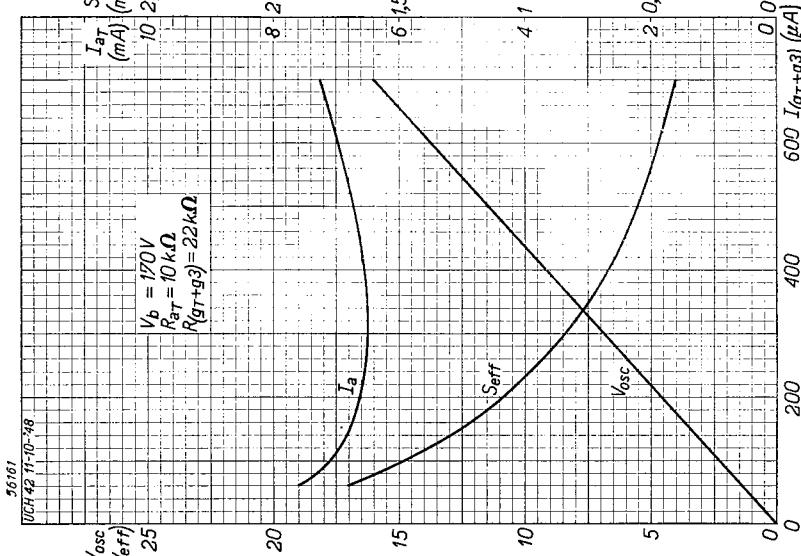


Fig. 20

Anode current (I_a), oscillator voltage (V_{osc}) and effective slope (S_{eff}) of the triode section of the UCH 42 as functions of the oscillator grid current (I_{gr+g3}), with grid leak (R_{gr+g3}) of 22 k Ω . Fig. 19: supply voltage $V_b = 100$ V; Fig. 20: $V_b = 170$ V.

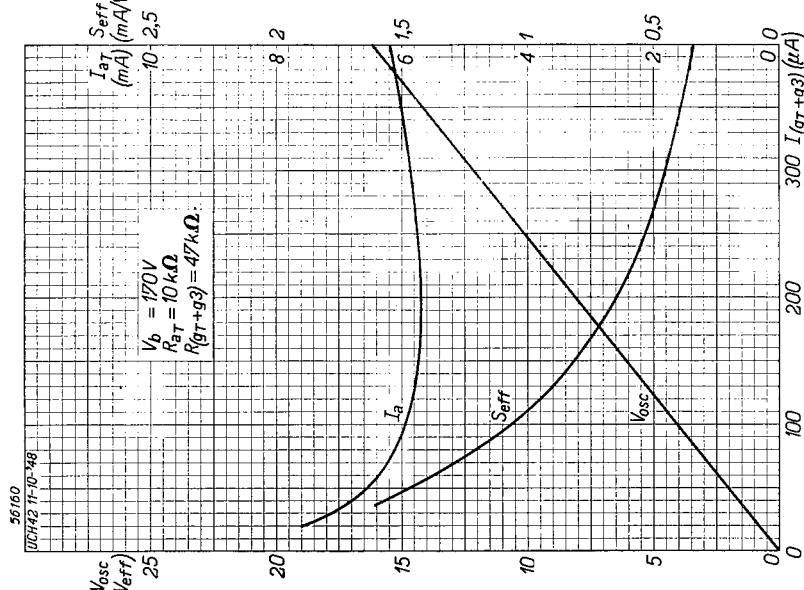
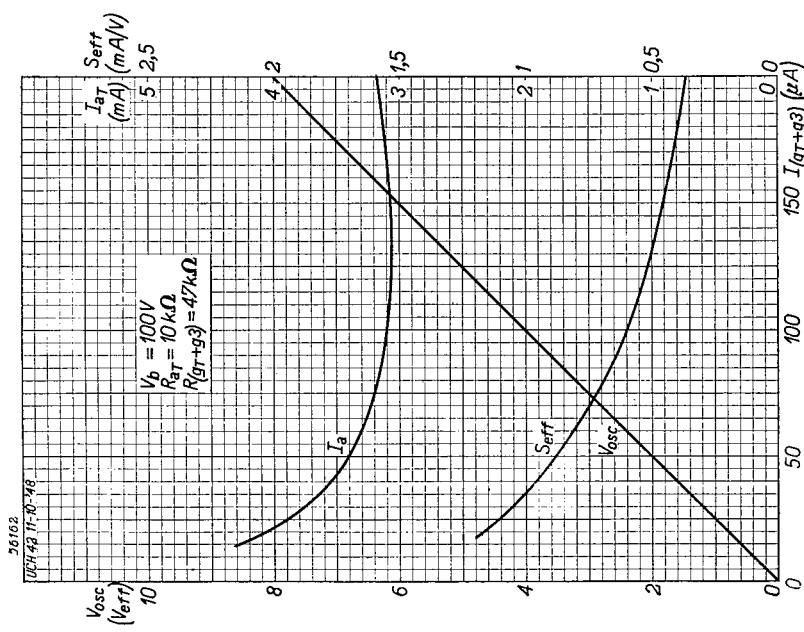


Fig. 21
As Figs. 19 and 20, but with a grid leak $R_{(gr+g3)}$ of 47 kΩ.

Fig. 22

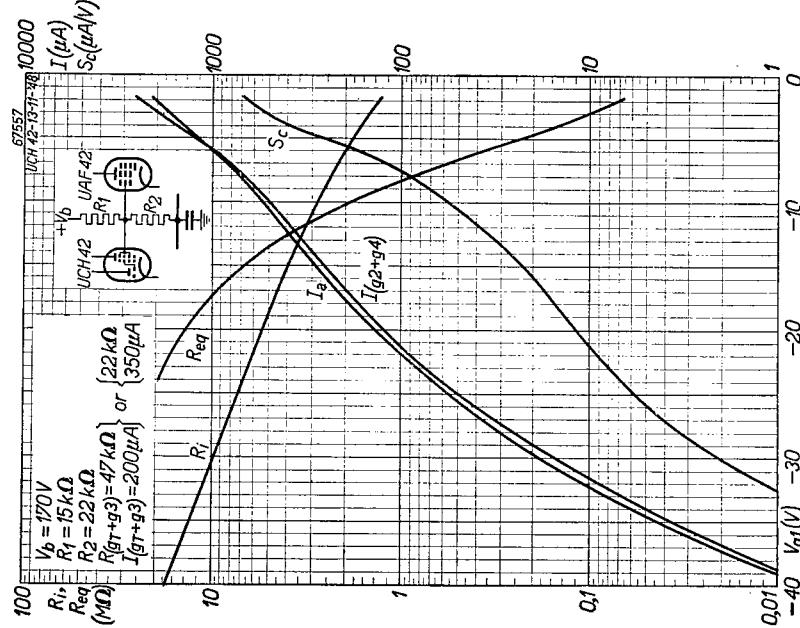
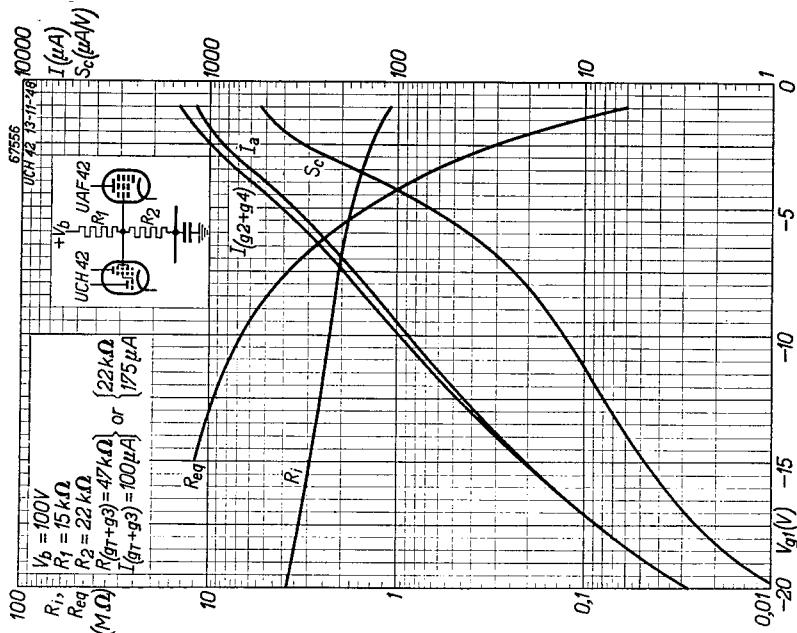


Fig. 23
As Figs. 10 and 11, but with the screen grid voltage of the UCH 42 together with that of the UAF 42 fed by means of a common potentiometer. Measured in the circuit shown in Fig. 5. Fig. 23 : supply voltage V_b = 100 V ; Fig. 24 : V_b = 170 V.

Fig. 24
UCH 42-13-11-38
V_b = 170 V
R₁,
R₂
(MΩ)
R₁ = 15 kΩ
R₂ = 22 kΩ
R₁ = 22 kΩ
R₂ = 350 μA
I_{g1+g2} = 200 μA or 350 μA
R_{eq}

I (μA)

S_c (μA/V)

Y_{g1} (V)

I (μA)

S_c (μA/V)

Y_{g1} (V)

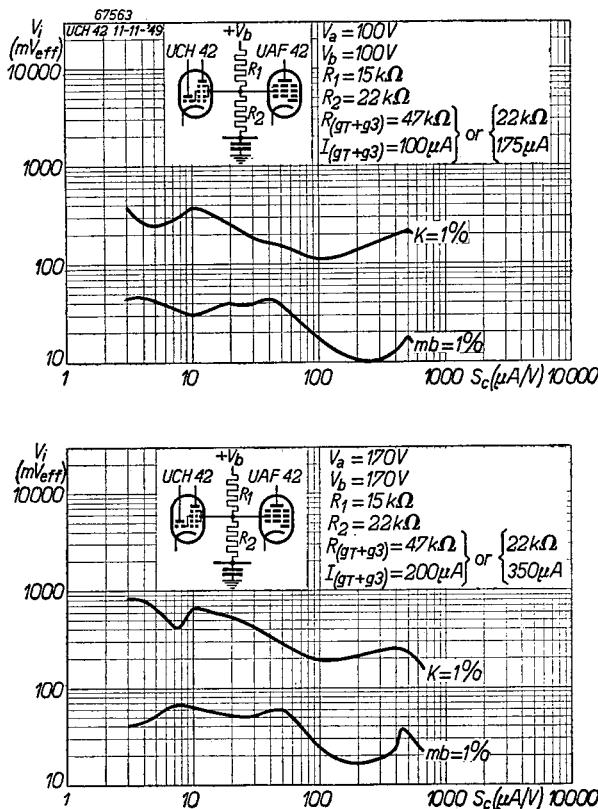


Fig. 25
As Fig. 16, but with the screen grids of the
UAF 42 and UCH 42 fed by means of a
common potentiometer.