CF 50 Microphone pre amplifier pentode

The CF 50 was specially designed for the amplification of very low voltages. Hum, background noise and microphony have all been reduced to a minimum and the principal application of the valve is as a pre-amplifier in crystal or ribbon-microphone equipment. This valve is capable of being operated to give a stage gain of about 300, producing an effective alternating output voltage of 3 V with less than 1 % distortion or, if required, a gain factor of between 395 and 45 with distortion less than 0.4 $_{00}^{0/}$ and an output voltage of 0.1 V_{eff} . This versatility of the valve may be ascribed to the fact that the input signals in this case are extremely small.

Details of the operating possibilities of this valve are set out in Tables I and II.

In view of the fact that the valve is specially intended for the amplification of very small signals, extra care must be taken to prevent Dimensions in mm. hum, since otherwise the level of the hum will quickly approach that of the input signal itself. For this latter reason the valve is equipped with a bifiliar filament, in consequence of which the external magnetic field is very weak; as this field is proportional to the g3 strength of the current, the heater current has been kept as low as gf possible, namely 200 mA, so that, in effect, there is hardly any external field at all. To ensure

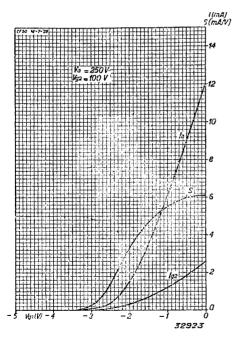


Fig. 3 Anode current Ia, screen-grid current Ig2 and mutual conductance S as functions of the grid bias Vg_1 with Vu = 250 V and $Vg_2 = 100$ V.

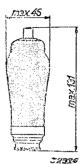


Fig. 1

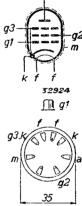


Fig. 2 Arrangement of electrodes and base connections.

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fact that the voltage delivered by the microphone is of the order of 1 mV, it may be claimed that the ripple level is very low indeed. In a cathode resistor without a decoupling capacitor the induced ripple voltage will be about 20 μ V.

sufficient emission from

the cathode on this cur-

rent it has been necessary to employ a heater voltage of 30 V. The

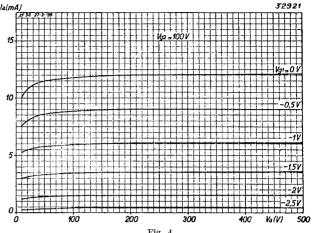
ultimate result is that, using a grid impedance

of 0.5 megohm, the voltage on the grid corresponding to the hum on both grid and anode is

less than 1 μ V. Taking

into consideration the

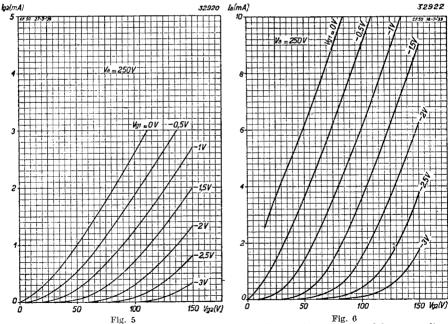
The equivalent noise resistance of the CF 50 is 2,500 ohms, which corresponds to an effective value of 0.7 μ V for the noise voltage on the grid at a bandwidth of 10,000 c/s and this, compared with the voltages applied to the grid, is also extremely low. In fact, the equivalent noise resistance gives the impression of being unnecessarily low in comparison with the custom- lalmA ary value of the grid leak, but it should be remembered that crystal microphones have a markedly capacitive character, due to which fact the noise resistance of the microphone, for the greater part of the frequency range, is considerably lower than the matching resistance based on the response over a relatively small range of low frequencies. The low value of the equivalent noise resistance of the CF 50 is a result of the high mutual conductance with a low



 $\begin{array}{c} {\rm Fig.~4} \\ {\rm Anode~current~as~a~function~of~the~anode~voltage~for~different~values} \\ {\rm of~grid~bias,~at~a~screen~potential~of~100~V.} \end{array}$

anode current (S = 3.3 mA/V, $I_a = 1.5 \text{ mA}$).

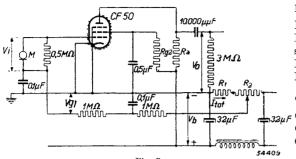
Finally it may be noted that microphony is eliminated as far as possible by the use of special double mica supports for the system of electrodes; on the whole, then, the CF 50 is an excellent valve for the pre-amplification stage of the more sensitive type



Screen-grid current as a function of the screen voltage for different values of grid bias, with 250 V anode voltage.

Anode current as a function of the screen voltage for different values of grid bias, with 250 V anode voltage.

of amplifier, more especially on account of the low noise resistance in cases where the voltage to be amplified comes from a source of which the noise resistance is also comparatively low.



HEATER RATINGS

Heating: indirect, A.C. or D.C., series or parallel supply. Heater voltage $V_f = 30$ V. Heater current $I_f = 0.200$ A.

CAPACITANCES

 $C_{ag1} < 0.03 \ \mu\mu F \ C_{g1} = 13 \ \mu\mu F \ C_{a} = 14.5 \ \mu\mu F$

Fig. 7 Circuit diagram showing the CF 50 used as a microphone pre-amplifier.

STATIC RATINGS

Anode voltage $\dots \dots \dots$	250 V										
Screen-grid voltage $V_{g_2} = 100 \text{ V}$	100 V										
Grid bias $V_{g_1} = -2 \text{ V}$	-2 V										
Anode current $I_a = 1.5 \text{ mA}$	1.5 mA										
Screen-grid current $I_{g2} = 0.3 \text{ mA}$	$0.3 \mathrm{mA}$										
Mutual conductance $S = 3.3 \text{ mA/V}$	$3.3~\mathrm{mA/V}$										
Internal resistance $R_i = 2$ M ohms	s 2.5 M ohms										
Amplification factor; screen with respect to control											
grid	45										
Equivalent noise resistance in the frequency range											
50 to 10,000 c/s $R_{eq} = -$	2,500 ohms										

TABLE I
OPERATING DATA: CF 50 used as resistance-coupled A.F. amplifier without
gain control (see Fig. 7)

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	Supply voltage	Anode resistor	Screen- grid series resistor	Cathode resistor	Anode current	Screen current	Voltage gain	Output voltage	Total distortion
	<i>Vb</i> (V)	Ra (M ohm)	Rg_2 (M ohm)	Rk (ohms)	Ia (mA)	$Ig_2 \pmod{MA}$	Vo/Vi	Vo $(Veff)$	₫ tot (%)
	250 200 100	0.3 0.3 0.3	0.9 0.8 0.4	2,000 3,000 7,000	0.7 0.5 0.2	0.18 0.15 0.07	315 260 150	3 3	<1 <1 <1
	250 200 100	0.2 0.2 0.2	$0.7 \\ 0.64 \\ 0.32$	1,800 2,000 5,000	0.9 0.7 0.3	0.22 0.18 0.09	295 245 145	3 3 3	< l < l < l
	250 200 100	0.1 0.1 0.1	0.64 0.56 0.28	1,800 2,200 5,000	0.9 0.7 0.3	0.22 0.19 0.09	280 230 140	3 3 3	<1 <1 <1

TABLE II

OPERATING DATA: CF 50 used as a resistance-coupled A.F. amplifier with control of the amplification (see Fig. 7)

Supply voltage	Anode resistor	Screen- grid series resistor	Grid bias	Anode current	Screen- grid current	Voltage gain	Output voltage	Total distortion
(V)	Ra (M ohm)	Ry_3 (M ohm)	$Vg_1 \ (V)$	Ia (mA)	<i>Ig</i> ₂ (mA)	Vo/Vi	Vo (Veff)	d an tot (%)
450 450 450 450 450	0.3 0.3 0.3 0.3 0.3	1.0 1.0 1.0 1.0	$ \begin{array}{r} -2 \\ -6 \\ -10 \\ -11 \\ -12 \end{array} $	1.4 0.72 0.22 0.11 0.04	0.38 0.18 0.06 0.04 0.02	395 260 90 45	0.1 0.1 0.1 0.1	$egin{array}{c} 0.2 \\ 0.2 \\ 0.2 \\ 0.4 \\ 3 \\ \end{array}$
450 450 450 450 450	0.2 0.2 0.2 0.2 0.2	0.8 0.8 0.8 0.8	$ \begin{array}{r} -2 \\ -6 \\ -10 \\ -11 \\ -12 \end{array} $	1.78 0.94 0.18 0.08 0.03	0.44 0.23 0.05 0.02 0.01	350 230 45 20 3	0.1 0.1 0.1 0.1 0.1	
450 450 450 450 450	0.1 0.1 0.1 0.1 0.1	0.5 0.5 0.5 0.5 0.5	$ \begin{array}{r} 2 \\ 6 \\ 10 \\ 11 \\ 12 \end{array} $	2.8 1.5 0.25 0.09 0.03	0.64 0.33 0.05 0.02 0.01	245 180 38 15	0.1 0.1 0.1 0.1 0.1	$ < 0.2 \\ < 0.2 \\ $

MAXIMUM RATINGS

Anode voltage in cold condition	$V_{ao} = \text{max. } 550 \text{ V}$
Anode voltage	$V_n = \text{max. } 250 \text{ V}$
Anode dissipation	$W_a = \max I W$
Screen voltage in cold condition	$V_{g_{20}} = \text{max. } 550 \text{ V}$
Screen voltage at $I_{\alpha} = 1.5 \text{ mA} \dots \dots$	$V_{g_2} = \text{max. } 125 \text{ V}$
Screen voltage at $I_a < 0.25 \text{ mA} \dots$	$V_{g_2} = \text{max. } 450 \text{ V}$
Screen dissipation	$W_{g_2} = \text{max. } 0.5 \text{ W}$
Cathode current	$I_k = \text{max. } 10 \text{ mA}$
Grid voltage at grid current start $(I_{g1} = + 0.3 \mu A)$	$V_{g_1} = \text{max.} -1.3 \text{ V}$
External resistance between control grid and cathode	$R_{q_1k} = \text{max. 3 M ohms}$
External resistance between heater and cathode	$R_{fk} = 20,000 \text{ ohms}$
Voltage between heater and cathode	$V_{fk} = \text{max. } 100 \text{ V}$