Advance Information

Switchmode™ Power Rectifier

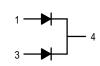
... using the Schottky Barrier principle with a proprietary barrier metal. These state—of—the—art devices have the following features:

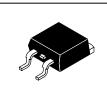
Features:

- Dual Diode Construction May be Paralleled for Higher Current Output
- · Guardring for Stress Protection
- Low Forward Voltage Drop
- 125°C Operating Junction Temperature
- Maximum Die Size
- Short Heat Sink Tab Manufactured Not Sheared!

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SCHOTTKY BARRIER RECTIFIER 30 AMPERES 30 VOLTS





CASE 418B-02 D2PAK Plastic

MAXIMUM RATINGS

Rating			Value	Unit
Peak Repetitive Reverse Voltage Working Peak Reverse Voltage DC Blocking Voltage		VRRM VRWM VR	30	V
Average Rectified Forward Current (At Rated V_R , $T_C = 115$ °C)	Per Device	lo	15 30	А
Peak Repetitive Forward Current (At Rated V _R , Square Wave, 20 kHz, T _C = 115°C)		IFRM	30	Α
Non-Repetitive Peak Surge Current (Surge Applied at Rated Load Conditions, Halfwave, Single Phase, 60 Hz)		IFSM	300	Α
Peak Repetitive Reverse Surge Current (1.0 µs, 1.0 kHz)		IRRM	2.0	Α
Storage Temperature Range		T _{stg}	- 55 to 150	°C
Operating Junction Temperature Range		TJ	- 55 to 125	°C
Voltage Rate of Change (Rated V_R , $T_J = 25$ °C)		dv/dt	10,000	V/μs
Reverse Energy, Unclamped Inductive Surge $(T_J = 25^{\circ}C, L = 3.0 \text{ mH})$		EAS	224.5	mJ

THERMAL CHARACTERISTICS

Thermal Resistance — Junction–to–Case	R _{tjc}	1.0	°C/W
Thermal Resistance — Junction–to–Ambient (1)	R _{tja}	50	°C/W

ELECTRICAL CHARACTERISTICS

Maximum Instantaneous Forward Voltage (2)	٧F		V
$(I_F = 15 \text{ A}, T_J = 25^{\circ}\text{C})$		0.44	
$(I_F = 30 \text{ A}, T_J = 25^{\circ}\text{C})$		0.51	
Maximum Instantaneous Reverse Current	IR		mA
(Rated V_R , $T_J = 25$ °C)		2.0	
(Rated V_R , $T_J = 125$ °C)		195	

- (1) Mounted using minimum recommended pad size on FR-4 board.
- (2) Pulse Test: Pulse Width = 250 μ s, Duty Cycle \leq 2.0%.

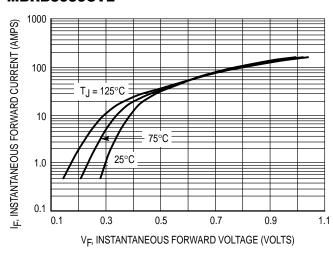
All device data is "Per Leg" except where noted.

This document contains information on a new product. Specifications and information herein are subject to change without notice.

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1000 TJ = 125°C TJ = 1

Figure 1. Typical Forward Voltage

Figure 2. Maximum Forward Voltage

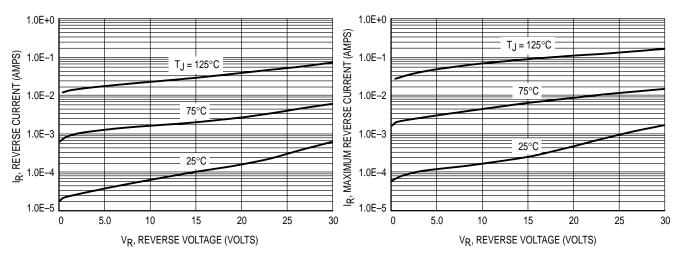
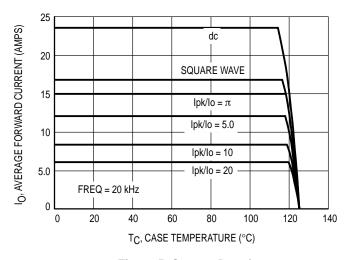


Figure 3. Typical Reverse Current

Figure 4. Maximum Reverse Current





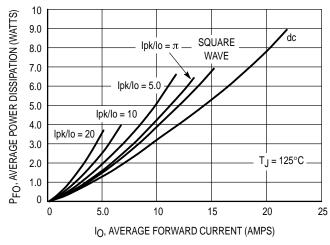


Figure 6. Forward Power Dissipation

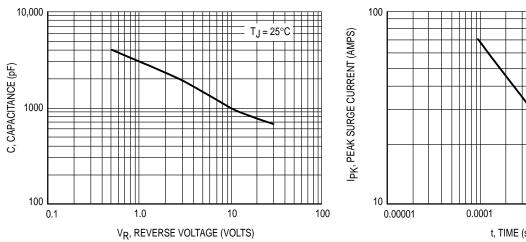


Figure 7. Typical Capacitance

0.001 0.01 t, TIME (seconds)

Figure 8. Typical Unclamped Inductive Surge

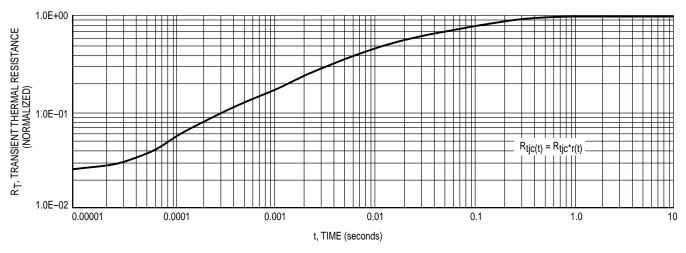


Figure 9. Typical Thermal Response

Modeling Reverse Energy Characteristicsof Power Rectifiers

Prepared by: David Shumate & Larry Walker Motorola Semiconductor Products Sector

ABSTRACT

Power semiconductor rectifiers are used in a variety of applications where the reverse energy requirements often vary dramatically based on the operating conditions of the application circuit. A characterization method was devised using the Unclamped Inductive Surge (UIS) test technique. By testing at only a few different operating conditions (i.e. different inductor sizes) a safe operating range can be established for a device. A relationship between peak avalanche current and inductor discharge time was established. Using this relationship and circuit parameters, the part applicability can be determined. This technique offers a power supply designer the total operating conditions for a device as opposed to the present single—data—point approach.

INTRODUCTION

In today's modern power supplies, converters and other switching circuitry, large voltage spikes due to parasitic inductance can propagate throughout the circuit, resulting in catastrophic device failures. Concurrent with this, in an effort to provide low–loss power rectifiers, i.e. devices with lower forward voltage drops, schottky technology is being applied to

devices used in this switching power circuitry. This technology lends itself to lower reverse breakdown voltages. This combination of high voltage spikes and low reverse breakdown voltage devices can lead to reverse energy destruction of power rectifiers in their applications. This phenomena, however, is not limited to just schottky technology.

In order to meet the challenges of these situations, power semiconductor manufacturers attempt to characterize their devices with respect to reverse energy robustness. The typical reverse energy specification, if provided at all, is usually given as energy—to—failure (mJ) with a particular inductor specified for the UIS test circuit. Sometimes, the peak reverse test current is also specified. Practically all reverse energy characterizations are performed using the UIS test circuit shown in Figure 10. Typical UIS voltage and current waveforms are shown in Figure 11.

In order to provide the designer with a more extensive characterization than the above mentioned one–point approach, a more comprehensive method for characterizing these devices was developed. A designer can use the given information to determine the appropriateness and safe operating area (SOA) of the selected device.

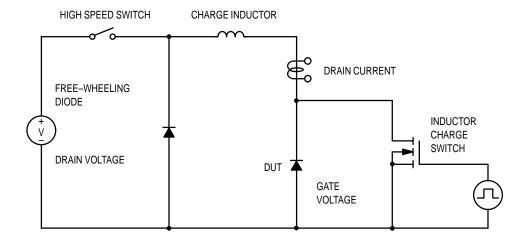


Figure 10. Simplified UIS Test Circuit

Suggested Method of Characterization

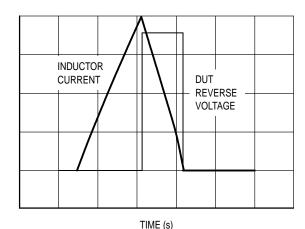


Figure 11. Typical Voltage and Current UIS Waveforms

Utilizing the UIS test circuit in Figure 10, devices are tested to failure using inductors ranging in value from 0.01 to 159 mH. The reverse voltage and current waveforms are acquired to determine the exact energy seen by the device and the inductive current decay time. At least 4 distinct inductors and 5 to 10 devices per inductor are used to generate the characteristic current versus time relationship. This relationship when coupled with the application circuit conditions, defines the SOA of the device uniquely for this application.

Example Application

The device used for this example was an MBR3035CT, which is a 30 A (15 A per side) forward current, 35 V reverse breakdown voltage rectifier. All parts were tested to destruction at 25°C. The inductors used for the characterization were 10, 3.0, 1.0 and 0.3 mH. The data recorded from the testing were peak reverse current (Ip), peak reverse breakdown voltage (BVR), maximum withstand energy, inductance and inductor discharge time (see Table 1). A plot of the Peak Reverse Current versus Time at device destruction, as shown in Figure 12, was generated. The area under the curve is the region of lower reverse energy or lower stress on the device. This area is known as the safe operating area or SOA.

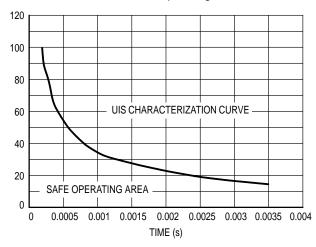


Figure 12. Peak Reverse Current versus Time for DUT

Table 1. UIS Test Data

PART NO.	I _P (A)	B _{VR} (V)	ENERGY (mJ)	L (mH)	TIME (μs)	
1	46.6	65.2	998.3	1	715	
2	41.7	63.4	870.2	1	657	
3	46.0	66.0	1038.9	1	697	
4	42.7	64.8	904.2	1	659	
5	44.9	64.8	997.3	1	693	
6	44.1	64.1	865.0	1	687	
7	26.5	63.1	1022.6	3	1261	
8	26.4	62.8	1024.9	3	1262	
9	24.4	62.2	872.0	3	1178	
10	27.6	62.9	1091.0	3	1316	
11	27.7	63.2	1102.4	3	1314	
12	17.9	62.6	1428.6	10	2851	
13	18.9	62.1	1547.4	10	3038	
14	18.8	60.7	1521.1	10	3092	
15	19.0	62.6	1566.2	10	3037	
16	74.2	69.1	768.4	0.3	322	
17	77.3	69.6	815.4	0.3	333	
18	75.2	68.9	791.7	0.3	328	
19	77.3	69.6	842.6	0.3	333	
20	73.8	69.1	752.4	0.3	321	
21	75.6	69.2	823.2	0.3	328	
22	74.7	68.6	747.5	0.3	327	
23	78.4	70.3	834.0	0.3	335	
24	70.5	66.6	678.4	0.3	317	
25	78.3	69.4	817.3	0.3	339	

The procedure to determine if a rectifier is appropriate, from a reverse energy standpoint, to be used in the application circuit is as follows:

- a. Obtain "Peak Reverse Current versus Time" curve from data book.
- b. Determine steady state operating voltage (OV) of circuit.
- c. Determine parasitic inductance (L) of circuit section of interest.
- d. Obtain rated breakdown voltage (BVR) of rectifier from data book.
- e. From the following relationships,

$$V = L \cdot \frac{d}{dt}i(t)$$

$$I = \frac{(BVR - OV) \cdot t}{L}$$

a "designer" I versus t curve is plotted alongside the device characteristic plot.

f. The point where the two curves intersect is the current level where the devices will start to fail. A peak inductor current below this intersection should be chosen for safe operating.

As an example, the values were chosen as L = 200 μ H, OV = 12 V and BVR = 35 V.

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Figure 13 illustrates the example. Note the UIS characterization curve, the parasitic inductor current curve and the safe operating region as indicated.

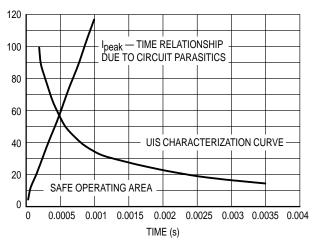


Figure 13. DUT Peak Reverse and Circuit Parasitic Inductance Current versus Time

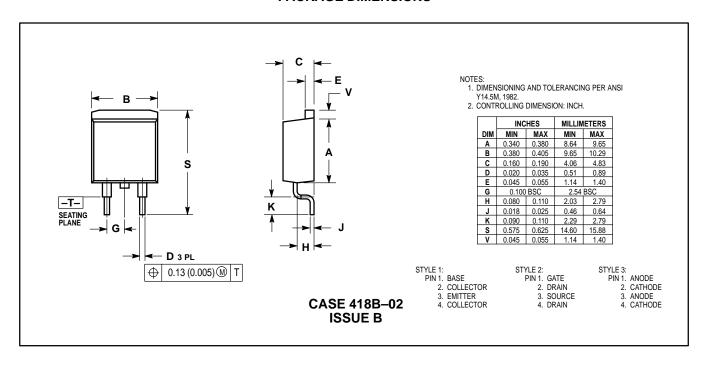
SUMMARY

Traditionally, power rectifier users have been supplied with single—data—point reverse—energy characteristics by the supplier's device data sheet; however, as has been shown here and in previous work, the reverse withstand energy can vary significantly depending on the application. What was done in this work was to create a characterization scheme by which the designer can overlay or map their particular requirements onto the part capability and determine quite accurately if the chosen device is applicable. This characterization technique is very robust due to its statistical approach, and with proper guardbanding (6 σ) can be used to give worst—case device performance for the entire product line. A "typical" characteristic curve is probably the most applicable for designers allowing them to design in their own margins.

References

- Borras, R., Aliosi, P., Shumate, D., 1993, "Avalanche Capability of Today's Power Semiconductors, "<u>Proceedings</u>, <u>European Power Electronic Conference</u>," 1993, Brighton, England
- 2. Pshaenich, A., 1985, "Characterizing Overvoltage Transient Suppressors," <u>Powerconversion International</u>, June/July

PACKAGE DIMENSIONS



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