

Smart Highside High Current Power Switch

Reverse Save

- Reverse battery protection by self turn on of power MOSFET

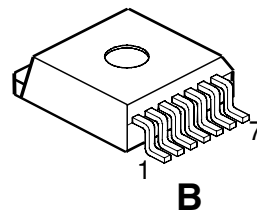
Features

- Overload protection
- Current limitation
- Short circuit protection
- Overtemperature protection
- Overvoltage protection (including load dump)
- Clamp of negative voltage at output
- Fast deenergizing of inductive loads ¹⁾
- Low ohmic inverse current operation
- Diagnostic feedback with load current sense
- Open load detection via current sense
- Loss of V_{bb} protection ²⁾
- Electrostatic discharge (ESD) protection

Product Summary

Overvoltage protection	$V_{bb(AZ)}$	62	V
Output clamp	$V_{ON(CL)}$	44	V
Operating voltage	$V_{bb(on)}$	5.0 ... 34	V
On-state resistance	R_{ON}	6.0	mΩ
Load current (ISO)	$I_L(ISO)$	70	A
Short circuit current limitation	$I_L(SC)$	130	A
Current sense ratio	$I_L : I_{IS}$	14 000	

TO 220-7

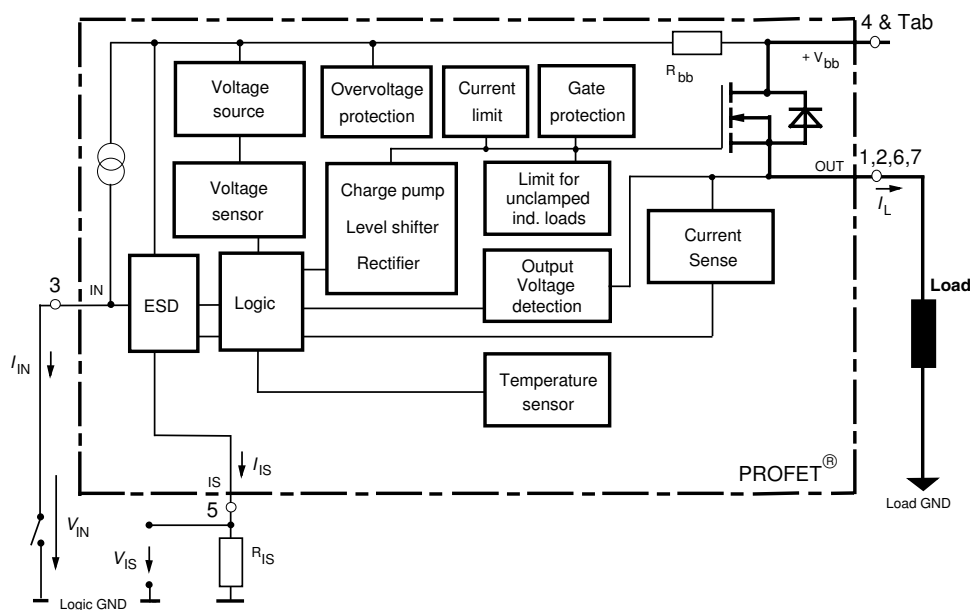


Application

- Power switch with current sense diagnostic feedback for 12 V and 24 V DC grounded loads
- Most suitable for loads with high inrush current like lamps and motors; all types of resistive and inductive loads
- Replaces electromechanical relays, fuses and discrete circuits

General Description

N channel vertical power FET with charge pump, current controlled input and diagnostic feedback with load current sense, integrated in Smart SiPMOS® chip on chip technology. Fully protected by embedded protection functions.



¹⁾ With additional external diode.

²⁾ Additional external diode required for energized inductive loads (see page 8).

Pin	Symbol	Function
1	OUT O	Output to the load. The pins 1,2,6 and 7 must be shorted with each other especially in high current applications! ³⁾
2	OUT O	Output to the load. The pins 1,2,6 and 7 must be shorted with each other especially in high current applications! ³⁾
3	IN I	Input, activates the power switch in case of short to ground
4	V _{bb} +	Positive power supply voltage, the tab is electrically connected to this pin. In high current applications the tab should be used for the V _{bb} connection instead of this pin ⁴⁾ .
5	IS S	Diagnostic feedback providing a sense current proportional to the load current; zero current on failure (see Truth Table on page 6)
6	OUT O	Output to the load. The pins 1,2,6 and 7 must be shorted with each other especially in high current applications! ³⁾
7	OUT O	Output to the load. The pins 1,2,6 and 7 must be shorted with each other especially in high current applications! ³⁾

Maximum Ratings at $T_j = 25\text{ °C}$ unless otherwise specified

Parameter	Symbol	Values	Unit
Supply voltage (overvoltage protection see page 4)	V_{bb}	40	V
Supply voltage for short circuit protection, $T_{j,start} = -40 \dots +150\text{ °C}$: (E_{AS} limitation see diagram on page 9)	V_{bb}	34	V
Load current (short circuit current, see page 5)	I_L	self-limited	A
Load dump protection $V_{LoadDump} = V_A + V_s$, $V_A = 13.5\text{ V}$ $R_l^{5)} = 2\text{ }\Omega$, $R_L = 0.54\text{ }\Omega$, $t_d = 200\text{ ms}$, IN, IS = open or grounded	$V_{Load\ dump}^{6)}$	75	V
Operating temperature range	T_j	-40 ... +150	°C
Storage temperature range	T_{stg}	-55 ... +150	°C
Power dissipation (DC), $T_C \leq 25\text{ °C}$	P_{tot}	170	W
Inductive load switch-off energy dissipation, single pulse $V_{bb} = 12\text{ V}$, $T_{j,start} = 150\text{ °C}$, $T_C = 150\text{ °C}$ const., $I_L = 20\text{ A}$, $Z_L = 7.5\text{ mH}$, $0\text{ }\Omega$, (see diagrams on page 9)	E_{AS}	1.5	J
Electrostatic discharge capability (ESD) Human Body Model acc. MIL-STD883D, method 3015.7 and ESD assn. std. S5.1-1993, C = 100 pF, R = 1.5 k Ω	V_{ESD}	4	kV
Current through input pin (DC)	I_{IN}	+15, -250	mA
Current through current sense status pin (DC) see internal circuit diagrams on page 7	I_{IS}	+15, -250	mA

³⁾ Not shorting all outputs will considerably increase the on-state resistance, reduce the peak current capability and decrease the current sense accuracy

⁴⁾ Otherwise add about 0.3 m Ω to the R_{ON} if the pin is used instead of the tab.

⁵⁾ R_l = internal resistance of the load dump test pulse generator.

⁶⁾ $V_{Load\ dump}$ is setup without the DUT connected to the generator per ISO 7637-1 and DIN 40839.

Thermal Characteristics



Parameter and Conditions	Symbol	Values			Unit
		min	typ	max	
Thermal resistance chip - case:	$R_{thJC}^{(7)}$	--	--	0.75	K/W
junction - ambient (free air):	R_{thJA}	--	60	--	
SMD version, device on PCB ⁽⁸⁾ :			33		

Electrical Characteristics

Parameter and Conditions	Symbol	Values			Unit
		min	typ	max	

at $T_j = -40 \dots +150^\circ\text{C}$, $V_{bb} = 12\text{ V}$ unless otherwise specified

Load Switching Capabilities and Characteristics

On-state resistance (Tab to pins 1,2,6,7)					
$I_L = 20\text{ A}$, $T_j = 25^\circ\text{C}$:	R_{ON}	--	4.4	6.0	mΩ
$V_{IN} = 0$, $I_L = 20\text{ A}$, $T_j = 150^\circ\text{C}$:			7.9	10.5	
$I_L = 90\text{ A}$, $T_j = 150^\circ\text{C}$:			--	10.7	
$V_{bb} = 6\text{ V}^{(9)}$, $I_L = 20\text{ A}$, $T_j = 150^\circ\text{C}$:	$R_{ON(Static)}$	--	10	17	
Nominal load current ⁽¹⁰⁾ (Tab to pins 1,2,6,7)	$I_{L(ISO)}$	55	70	--	A
ISO 10483-1/6.7: $V_{ON} = 0.5\text{ V}$, $T_C = 85^\circ\text{C}^{(11)}$					
Nominal load current ⁽¹⁰⁾ , device on PCB ⁽⁸⁾)	$I_{L(NOM)}$	13.6	17	--	A
$T_A = 85^\circ\text{C}$, $T_j \leq 150^\circ\text{C}$ $V_{ON} \leq 0.5\text{ V}$,					
Maximum load current in resistive range					
(Tab to pins 1,2,6,7) $V_{ON} = 1.8\text{ V}$, $T_C = 25^\circ\text{C}$:	$I_{L(Max)}$	250	--	--	
see diagram on page 12 $V_{ON} = 1.8\text{ V}$, $T_C = 150^\circ\text{C}$:		150	--	--	A
Turn-on time ⁽¹²⁾ I_{IN}  to 90% V_{OUT} :	t_{on}	150	230	470	μs
Turn-off time I_{IN}  to 10% V_{OUT} :	t_{off}	80	130	200	
$R_L = 1\ \Omega$, $T_j = -40\dots+150^\circ\text{C}$					
Slew rate on ⁽¹²⁾ (10 to 30% V_{OUT})	dV/dt_{on}	0.1	0.25	0.6	V/μs
$R_L = 1\ \Omega$, $T_j = 25^\circ\text{C}$					
Slew rate off ⁽¹²⁾ (70 to 40% V_{OUT})	$-dV/dt_{off}$	0.15	0.35	0.6	V/μs
$R_L = 1\ \Omega$, $T_j = 25^\circ\text{C}$					

⁷⁾ Thermal resistance R_{thCH} case to heatsink (about 0.5 ... 0.9 K/W with silicone paste) not included!

⁸⁾ Device on 50mm*50mm*1.5mm epoxy PCB FR4 with 6cm² (one layer, 70μm thick) copper area for V_{bb} connection. PCB is vertical without blown air.

⁹⁾ Decrease of V_{bb} below 10 V causes slowly a dynamic increase of R_{ON} to a higher value of $R_{ON(Static)}$. As long as $V_{bIN} > V_{bIN(u) \max}$, R_{ON} increase is less than 10 % per second for $T_j < 85^\circ\text{C}$.

¹⁰⁾ Not tested, specified by design.

¹¹⁾ T_j is about 105°C under these conditions.

¹²⁾ See timing diagram on page 13.

Inverse Load Current Operation

On-state resistance (Pins 1,2,6,7 to pin 4) $V_{bIN} = 12\text{ V}$, $I_L = -20\text{ A}$ see page 9	$T_j = 25^\circ\text{C}$: $T_j = 150^\circ\text{C}$:	$R_{ON(inv)}$	--	4.4 7.9	6.0 10.5	$\text{m}\Omega$
Nominal inverse load current (Pins 1,2,6,7 to Tab) $V_{ON} = -0.5\text{ V}$, $T_C = 85^\circ\text{C}^{11)}$		$I_{L(inv)}$	55	70	--	A
Drain-source diode voltage ($V_{out} > V_{bb}$) $I_L = -20\text{ A}$, $I_{IN} = 0$, $T_j = +150^\circ\text{C}$		$-V_{ON}$	--	0.6	0.7	V

Operating Parameters

Operating voltage ($V_{IN} = 0$) ^{9, 13)}	$V_{bb(on)}$	5.0	--	34	V
Undervoltage shutdown ¹⁴⁾	$V_{bIN(u)}$	1.5	3.0	4.5	V
Undervoltage start of charge pump see diagram page 14	$V_{bIN(ucp)}$	3.0	4.5	6.0	V
Overvoltage protection ¹⁵⁾ $I_{bb} = 15\text{ mA}$	$T_j = -40^\circ\text{C}$: $T_j = 25\dots+150^\circ\text{C}$:	$V_{bIN(Z)}$	60 62	-- 66	-- V
Standby current $I_{IN} = 0$	$T_j = -40\dots+25^\circ\text{C}$: $T_j = 150^\circ\text{C}$:	$I_{bb(off)}$	-- --	15 25	25 50 μA

¹³⁾ If the device is turned on before a V_{bb} -decrease, the operating voltage range is extended down to $V_{bIN(u)}$. For all voltages 0 ... 34 V the device is fully protected against overtemperature and short circuit.

¹⁴⁾ $V_{bIN} = V_{bb} - V_{IN}$ see diagram on page 7. When V_{bIN} increases from less than $V_{bIN(u)}$ up to $V_{bIN(ucp)} = 5\text{ V}$ (typ.) the charge pump is not active and $V_{OUT} \approx V_{bb} - 3\text{ V}$.

¹⁵⁾ See also $V_{ON(CL)}$ in circuit diagram on page 8.

Protection Functions

Short circuit current limit (Tab to pins 1,2,6,7) $V_{ON} = 12\text{ V}$	$T_c = -40^\circ\text{C}$: $T_c = 25^\circ\text{C}$: $T_c = +150^\circ\text{C}$:	$I_{L(SC)}$ $I_{L(SC)}$ $I_{L(SC)}$	-- 45 --	110 130 115	-- 180 --	A
Output clamp ¹⁶⁾ (inductive load switch off) see diagram Ind. and overvolt. output clamp page 7	$I_L = 40\text{ mA}$:	$-V_{OUT(CL)}$	14	17	20	V
Output clamp (inductive load switch off) at $V_{OUT} = V_{bb} - V_{ON(CL)}$ (e.g. overvoltage) $I_L = 40\text{ mA}$		$V_{ON(CL)}$	40	44	47	V
Thermal overload trip temperature		T_{jt}	150	--	--	$^\circ\text{C}$
Thermal hysteresis		ΔT_{jt}	--	10	--	K

Reverse Battery

Reverse battery voltage ¹⁷⁾	$-V_{bb}$	--	--	32	V
On-state resistance (Pins 1,2,6,7 to pin 4) $T_j = 25^{\circ}\text{C}$: $V_{bb} = -12\text{V}$, $V_{IN} = 0$, $I_L = -20\text{A}$, $R_{IS} = 1\text{k}\Omega$ $T_j = 150^{\circ}\text{C}$:	$R_{ON(rev)}$	--	5.4 8.9	7.0 12.3	m Ω
Integrated resistor in V_{bb} line	R_{bb}	--	120	--	Ω

Diagnostic Characteristics

Current sense ratio, static on-condition, $k_{ILIS} = I_L : I_{IS}$, $V_{ON} < 1.5 V^{1b)}$, $V_{IS} < V_{OUT} - 5V$, $V_{bIN} > 4.0 V$ see diagram on page 11	$I_L = 90 A, T_i = -40^{\circ}C$: $T_i = 25^{\circ}C$: $T_i = 150^{\circ}C$: $I_L = 20 A, T_i = -40^{\circ}C$: $T_i = 25^{\circ}C$: $T_i = 150^{\circ}C$: $I_L = 10 A, T_i = -40^{\circ}C$: $T_i = 25^{\circ}C$: $T_i = 150^{\circ}C$: $I_L = 4 A, T_i = -40^{\circ}C$: $T_i = 25^{\circ}C$: $T_i = 150^{\circ}C$:	k_{ILIS}	12 500 12 500 11 500 12 500 12 000 11 500 12 500 11 500 11 500 11 000 11 000 11 200	14 200 13 700 13 000 14 500 14 000 13 400 15 000 14 300 13 500 18 000 15 400 14 000	16 000 16 000 14 500 17 500 16 500 15 000 19 000 17 500 15 500 28 500 22 000 19 000	
$I_{IS}=0$ by $I_{IN}=0$ (e.g. during deenergizing of inductive loads):						
Sense current saturation		$I_{IS,lim}$	6.5	--	--	mA
Current sense leakage current	$I_{IN}=0$:	$I_{IS(LL)}$	--	--	0.5	μA
	$V_{IN}=0, I_L \leq 0$:	$I_{IS(LH)}$	--	2	--	

¹⁶⁾ This output clamp can be "switched off" by using an additional diode at the IS-Pin (see page 7). If the diode is used, V_{OUT} is clamped to $V_{bb} - V_{ON(CL)}$ at inductive load switch off.

¹⁷⁾ The reverse load current through the intrinsic drain-source diode has to be limited by the connected load (as it is done with all polarity symmetric loads). Note that under off-conditions ($I_{IN} = I_{IS} = 0$) the power transistor is not activated. This results in raised power dissipation due to the higher voltage drop across the intrinsic drain-source diode. The temperature protection is not active during reverse current operation! Increasing reverse battery voltage capability is simply possible as described on page 8.

¹⁸⁾ If V_{ON} is higher, the sense current is no longer proportional to the load current due to sense current saturation, see $I_{IS,lim}$.

Current sense overvoltage protection $T_j = -40^\circ\text{C}$: $I_{bb} = 15\text{ mA}$	$V_{bIS(Z)}$	60	--	--	V
$T_j = 25\dots+150^\circ\text{C}$:		62	66	--	
Current sense settling time ¹⁹⁾	$t_{s(IS)}$	--	--	500	μs

Input

Input and operating current (see diagram page 12) IN grounded ($V_{IN} = 0$)	$I_{IN(on)}$	--	0.8	1.5	mA
Input current for turn-off ²⁰⁾	$I_{IN(off)}$	--	--	80	μA

Truth Table

	Input current level	Output level	Current Sense I_{IS}	Remark
Normal operation	L H	L H	0 nominal	$=I_L / k_{IIS}$, up to $I_{IS}=I_{IS,lim}$
Very high load current	H	H	$I_{IS, lim}$	up to $V_{ON}=V_{ON(Fold\ back)}$ I_{IS} no longer proportional to I_L
Current-limitation	H	H	0	$V_{ON} > V_{ON(Fold\ back)}$
Short circuit to GND	L H	L L	0 0	
Over-temperature	L H	L L	0 0	
Short circuit to V_{bb}	L H	H H	0 <nominal ²¹⁾	
Open load	L H	Z ²²⁾ H	0 0	
Negative output voltage clamp	L	L	0	
Inverse load current	L H	H H	0 0	

L = "Low" Level

H = "High" Level

Overtemperature reset by cooling: $T_j < T_{jt}$ (see diagram on page 14)

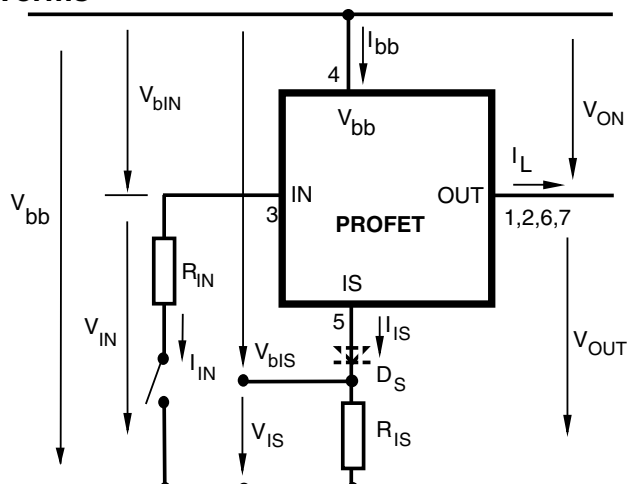
¹⁹⁾ Not tested, specified by design.

²⁰⁾ We recommend the resistance between IN and GND to be less than 0.5 k Ω for turn-on and more than 500k Ω for turn-off. Consider that when the device is switched off ($I_{IN} = 0$) the voltage between IN and GND reaches almost V_{bb} .

²¹⁾ Low ohmic short to V_{bb} may reduce the output current I_L and can thus be detected via the sense current I_{IS} .

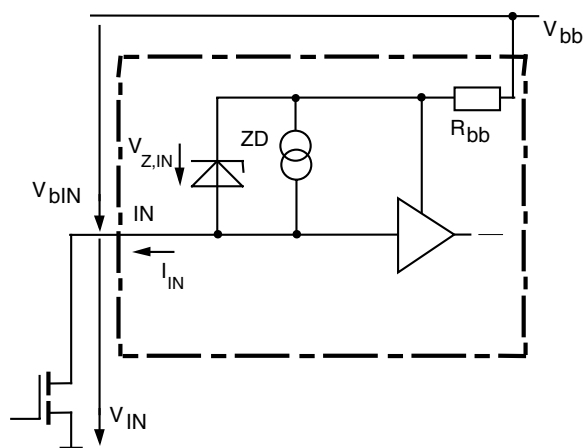
²²⁾ Power Transistor "OFF", potential defined by external impedance.

Terms



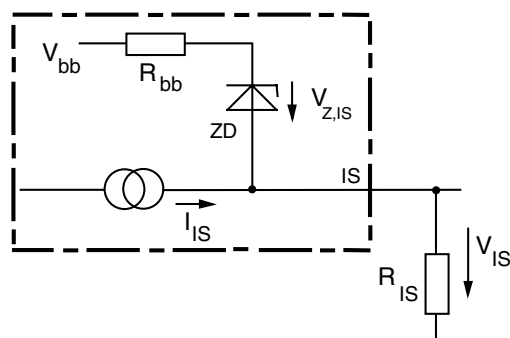
Two or more devices can easily be connected in parallel to increase load current capability.

Input circuit (ESD protection)



When the device is switched off ($I_{IN} = 0$) the voltage between IN and GND reaches almost V_{bb} . Use a mechanical switch, a bipolar or MOS transistor with appropriate breakdown voltage as driver.
 $V_{ZIN} = 66 \text{ V (typ)}$.

Current sense status output

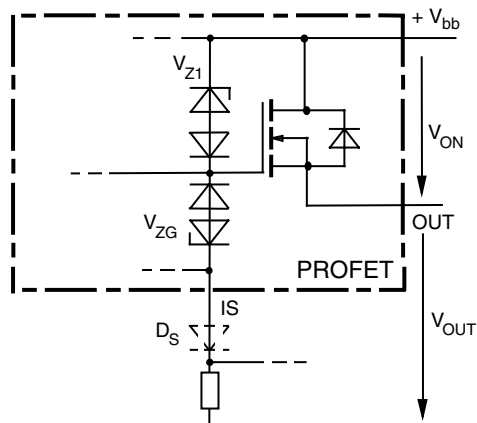


$V_{Z,IS} = 66\text{V}$ (typ.), $R_{IS} = 1\text{ k}\Omega$ nominal (or $1\text{ k}\Omega/n$, if n devices are connected in parallel). $I_S = I_L/K_{IIS}$ can be driven only by the internal circuit as long as $V_{out} - V_{IS} > 5\text{ V}$. If you want measure load currents up to $I_{L(M)}$, R_{IS} should be less than $\frac{V_{bb} - 5\text{ V}}{I_{L(M)} / K_{IIS}}$.

Note: For large values of R_{IS} the voltage V_{IS} can reach almost V_{bb} . See also overvoltage protection.

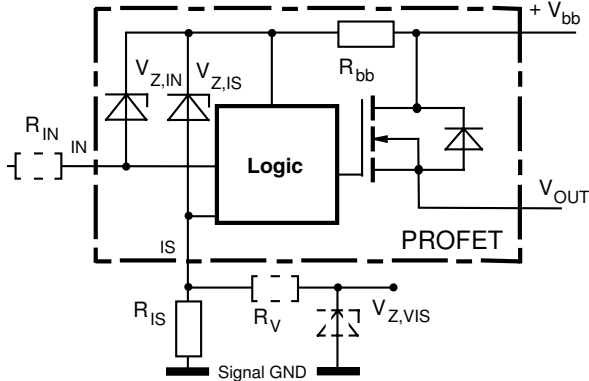
If you don't use the current sense output in your application, you can leave it open.

Inductive and overvoltage output clamp



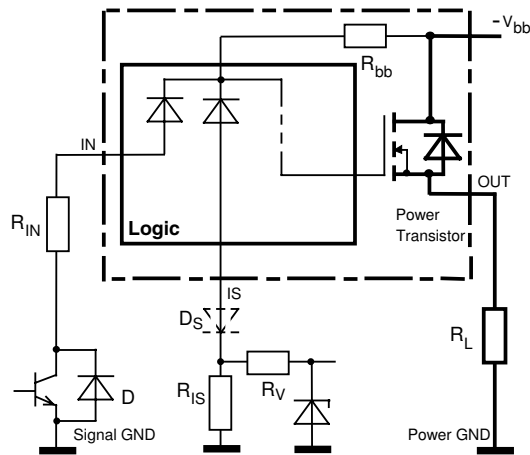
V_{ON} is clamped to $V_{ON(CL)} = 42\text{ V}$ typ. At inductive load switch-off without D_S , V_{OUT} is clamped to $V_{OUT(CL)} = -19\text{ V}$ typ. via V_{ZG} . With D_S , V_{OUT} is clamped to $V_{bb} - V_{ON(CL)}$ via V_{Z1} . Using D_S gives faster deenergizing of the inductive load, but higher peak power dissipation in the PROFET.

Overvoltage protection of logic part



$R_{bb} = 120\ \Omega$ typ., $V_{Z,IN} = V_{Z,IS} = 66\text{ V}$ typ., $R_{IS} = 1\text{ k}\Omega$ nominal. Note that when overvoltage exceeds 71 V typ. a voltage above 5V can occur between IS and GND, if R_V , $V_{Z,VIS}$ are not used.

Reverse battery protection



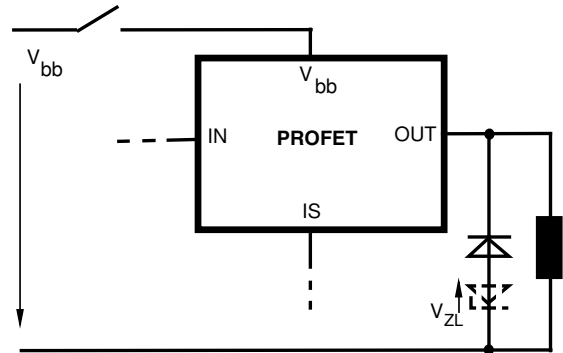
$R_V \geq 1\text{ k}\Omega$, $R_{IS} = 1\text{ k}\Omega$ nominal. Add R_{IN} for reverse battery protection in applications with V_{bb} above 16 V¹⁷⁾; recommended value: $\frac{1}{R_{IN}} + \frac{1}{R_{IS}} + \frac{1}{R_V} = \frac{0.1\text{ A}}{|V_{bb}| - 12\text{ V}}$ if D_S is not used (or $\frac{1}{R_{IN}} = \frac{0.1\text{ A}}{|V_{bb}| - 12\text{ V}}$ if D_S is used).

To minimize power dissipation at reverse battery operation, the summarized current into the IN and IS pin should be about 120mA. The current can be provided by using a small signal diode D in parallel to the input switch, by using a MOSFET input switch or by proper adjusting the current through R_{IS} and R_V .

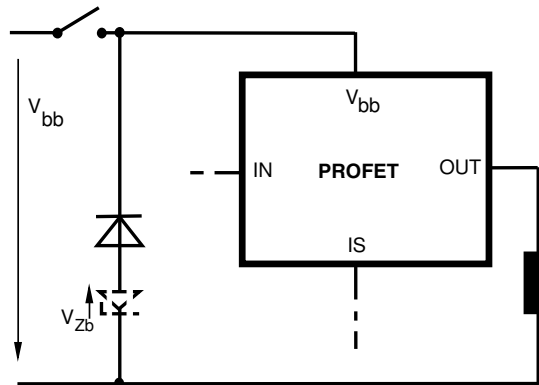
V_{bb} disconnect with energized inductive load

Provide a current path with load current capability by using a diode, a Z-diode, or a varistor. ($V_{ZL} < 72\text{ V}$ or $V_{Zb} < 30\text{ V}$ if $R_{IN}=0$). For higher clamp voltages currents at IN and IS have to be limited to 250 mA.

Version a:

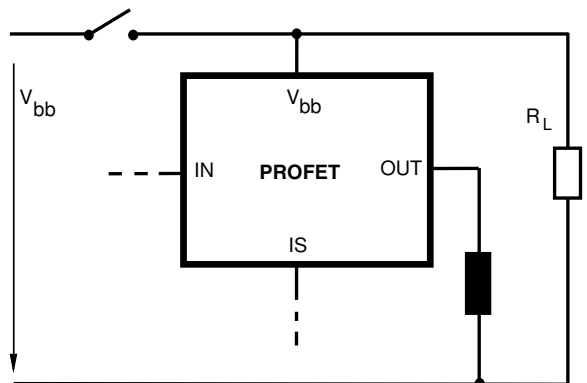


Version b:

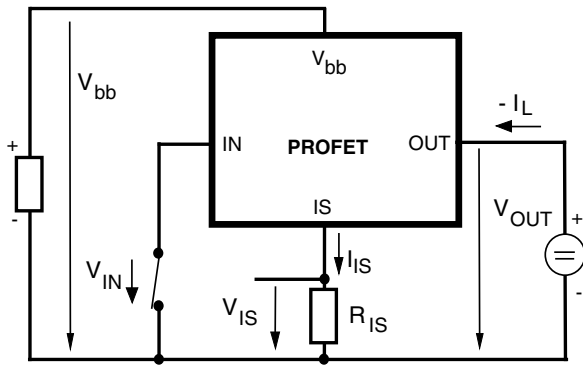


Note that there is no reverse battery protection when using a diode without additional Z-diode V_{ZL} , V_{Zb} .

Version c: Sometimes a necessary voltage clamp is given by non inductive loads R_L connected to the same switch and eliminates the need of clamping circuit:



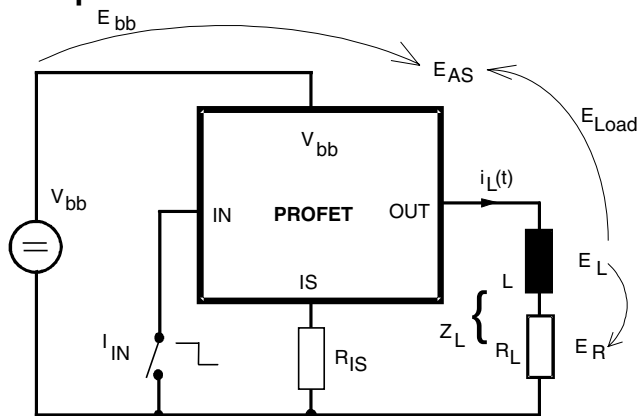
Inverse load current operation



The device is specified for inverse load current operation ($V_{OUT} > V_{bb} > 0V$). The current sense feature is not available during this kind of operation ($I_{IS} = 0$). With $I_{IN} = 0$ (e.g. input open) only the intrinsic drain source diode is conducting resulting in considerably increased power dissipation. If the device is switched on ($V_{IN} = 0$), this power dissipation is decreased to the much lower value $R_{ON(INV)} \cdot I^2$ (specifications see page 4).

Note: Temperature protection during inverse load current operation is not possible!

Inductive load switch-off energy dissipation



Energy stored in load inductance:

$$E_L = \frac{1}{2} \cdot L \cdot I_L^2$$

While demagnetizing load inductance, the energy dissipated in PROFET is

$$E_{AS} = E_{bb} + E_L - E_R = \int V_{ON(CL)} \cdot i_L(t) dt,$$

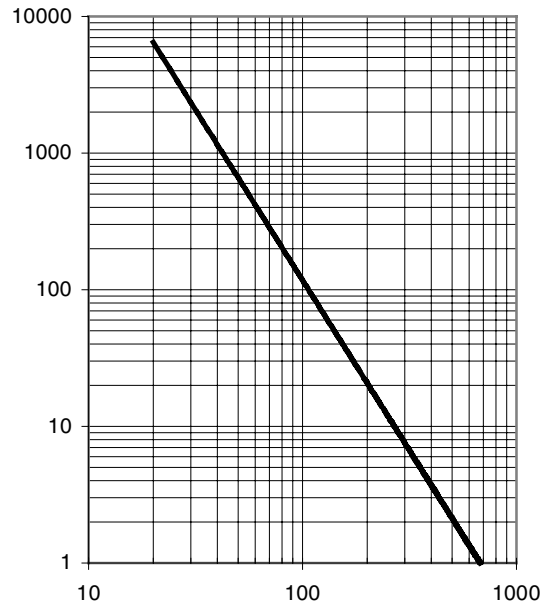
with an approximate solution for $R_L > 0\Omega$:

$$E_{AS} = \frac{I_L \cdot L}{2 \cdot R_L} (V_{bb} + |V_{OUT(CL)}|) \ln \left(1 + \frac{I_L \cdot R_L}{|V_{OUT(CL)}|} \right)$$

Maximum allowable load inductance for a single switch off

$$L = f(I_L); T_{j,start} = 150^\circ C, V_{bb} = 12V, R_L = 0\Omega$$

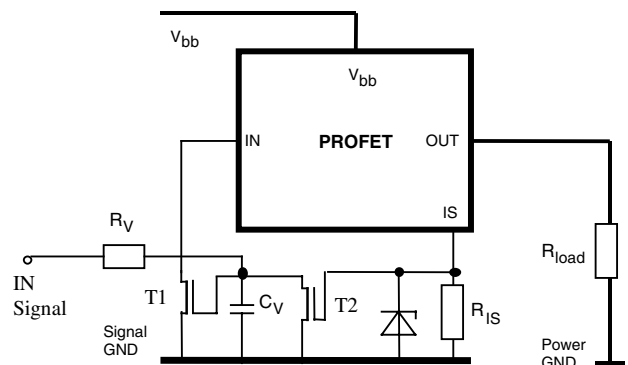
L [μH]



IL [A]

Externally adjustable current limit

If the device is conducting, the sense current can be used to reduce the short circuit current and allow higher lead inductance (see diagram above). The device will be turned off, if the threshold voltage of T2 is reached by $I_S \cdot R_{IS}$. After a delay time defined by $R_V \cdot C_V$ T1 will be reset. The device is turned on again, the short circuit current is defined by $I_{L(SC)}$.



Options Overview

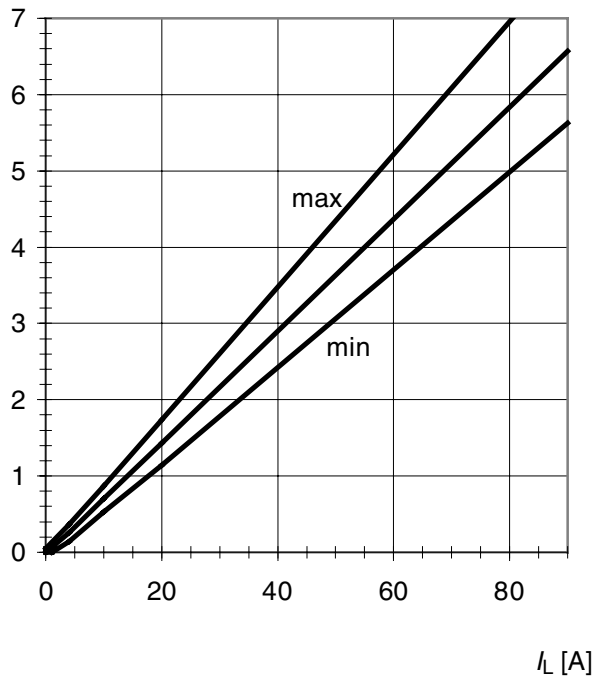
Type	BTS	6510P	550P 650P	555
Overtemperature protection with hysteresis $T_j > 150\text{ }^{\circ}\text{C}$, latch function ²³⁾		X	X	X X
$T_j > 150\text{ }^{\circ}\text{C}$, with auto-restart on cooling		X	X	
Short circuit to GND protection with overtemperature shutdown switches off when $V_{ON} > 6\text{ V}$ typ. (when first turned on after approx. 180 μs)		X	X	X
Overvoltage shutdown		-	-	-
Output negative voltage transient limit to $V_{bb} - V_{ON(CL)}$ to $V_{OUT} = -19\text{ V}$ typ		X X ²⁴⁾	X X ²⁴⁾	X X ²⁴⁾

²⁴⁾ Can be "switched off" by using a diode D_S (see page 8) or leaving open the current sense output.

Characteristics

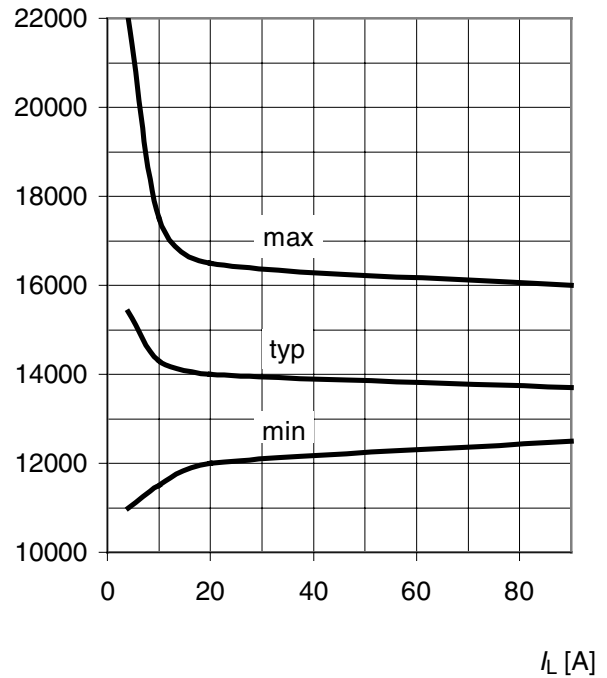
Current sense versus load current:

$$I_{IS} = f(I_L), T_J = -40 \dots +150 \text{ }^{\circ}\text{C}$$

 $I_{IS} \text{ [mA]}$


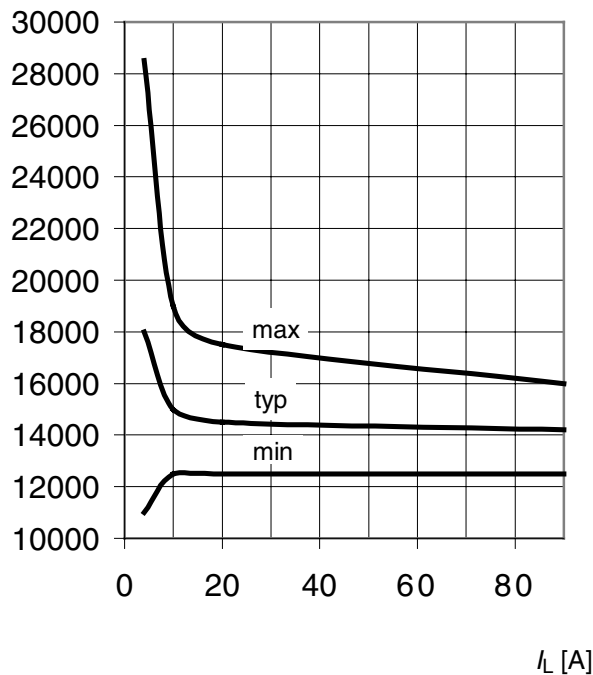
Current sense ratio:

$$I_{IS} = f(I_L), T_J = 25 \text{ }^{\circ}\text{C}$$

 K_{ILIS}


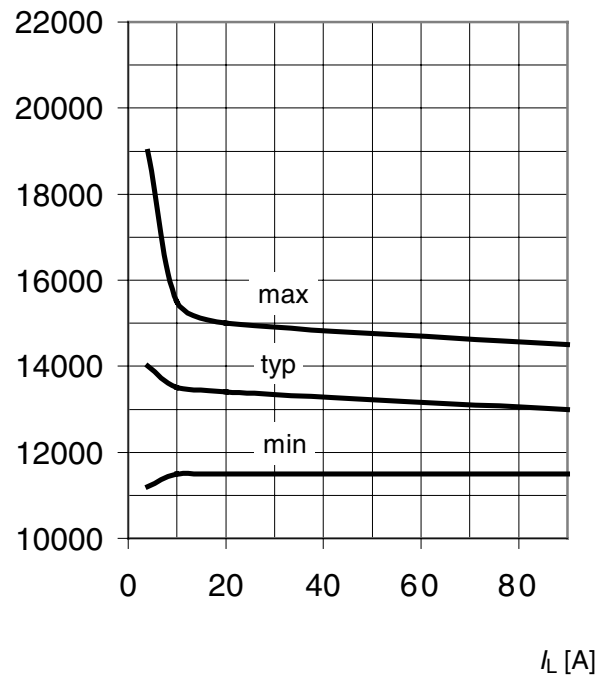
Current sense ratio:

$$K_{ILIS} = f(I_L), T_J = -40 \text{ }^{\circ}\text{C}$$

 K_{ILIS}


Current sense ratio:

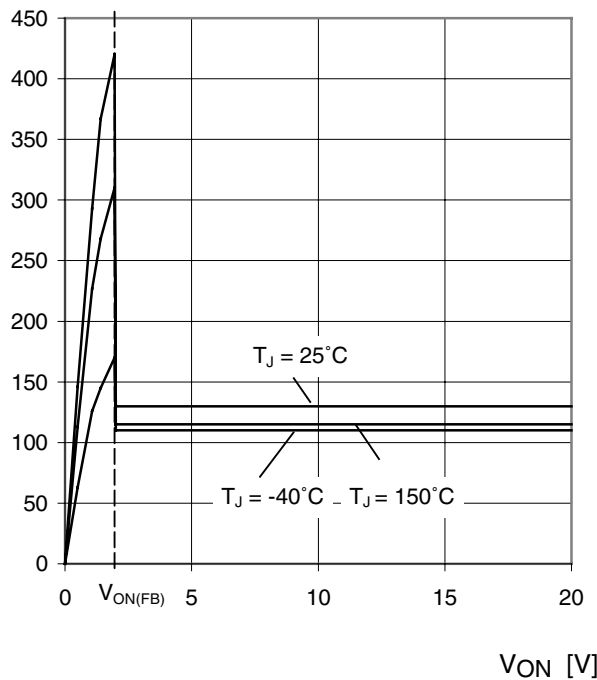
$$K_{ILIS} = f(I_L), T_J = 150 \text{ }^{\circ}\text{C}$$

 K_{ILIS}


Typ. current limitation characteristic

$$I_L = f(V_{ON}, T_j)$$

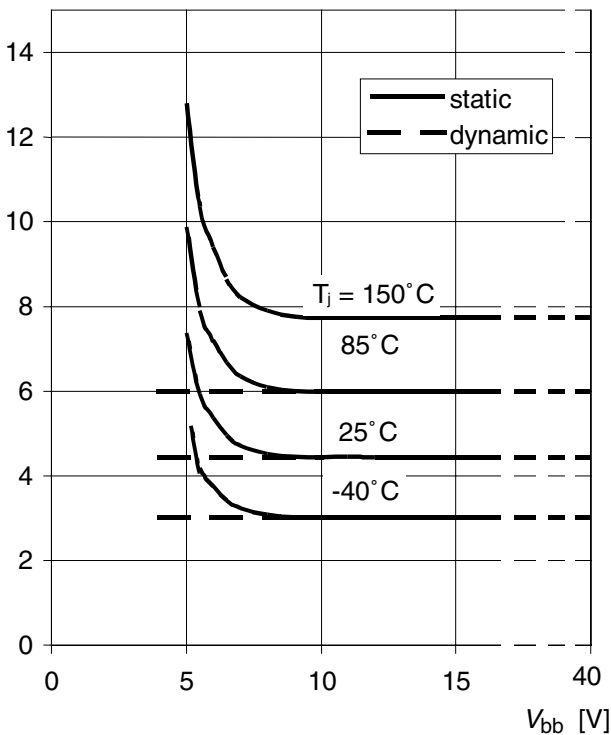
I_L [A]



Typ. on-state resistance

$$R_{ON} = f(V_{bb}, T_j); I_L = 20 \text{ A}; V_{IN} = 0$$

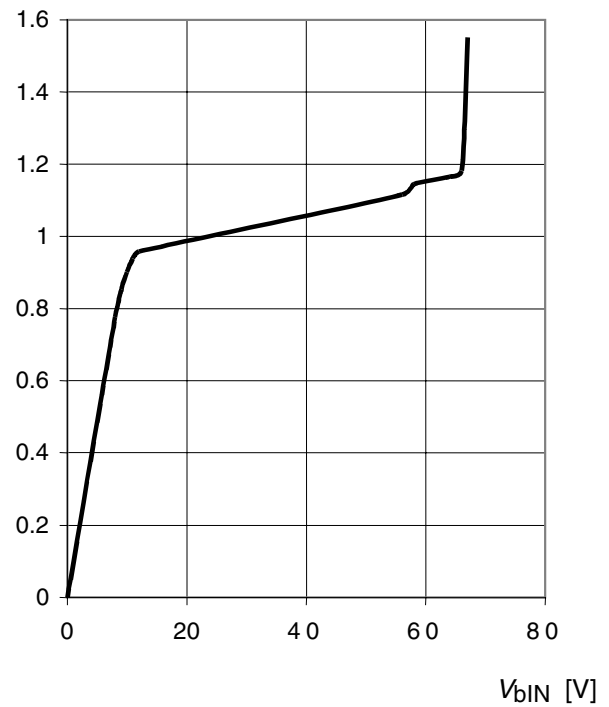
R_{ON} [mOhm]



Typ. input current

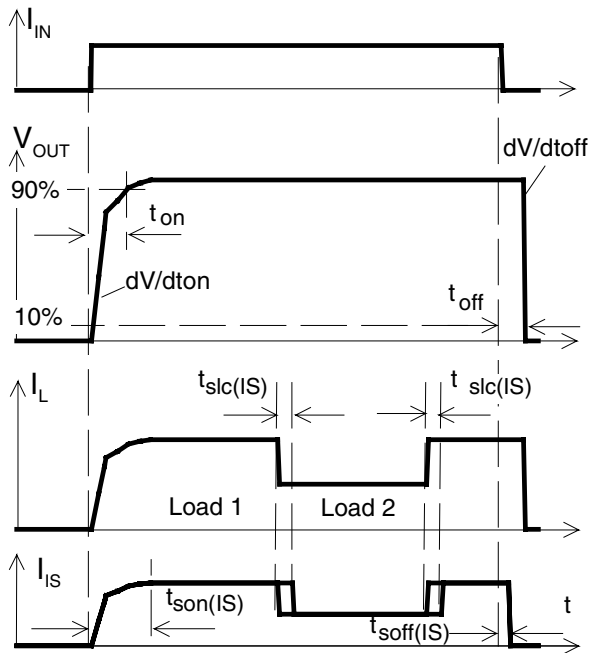
$$I_{IN} = f(V_{bIN}), V_{bIN} = V_{bb} - V_{IN}$$

I_{IN} [mA]



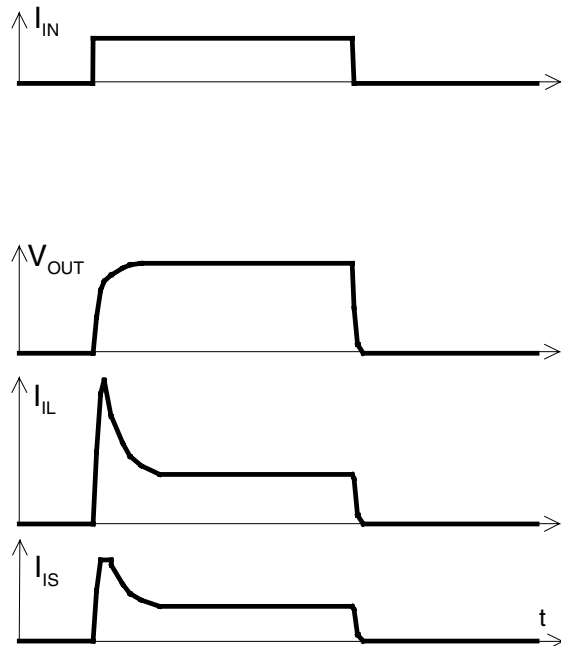
Timing diagrams

Figure 1a: Switching a resistive load, change of load current in on-condition:



The sense signal is not valid during a settling time after turn-on/off and after change of load current.

Figure 2a: Switching motors and lamps:



Sense current saturation can occur at very high inrush currents (see $I_{IS,lim}$ on page 5).

Figure 2b: Switching an inductive load:

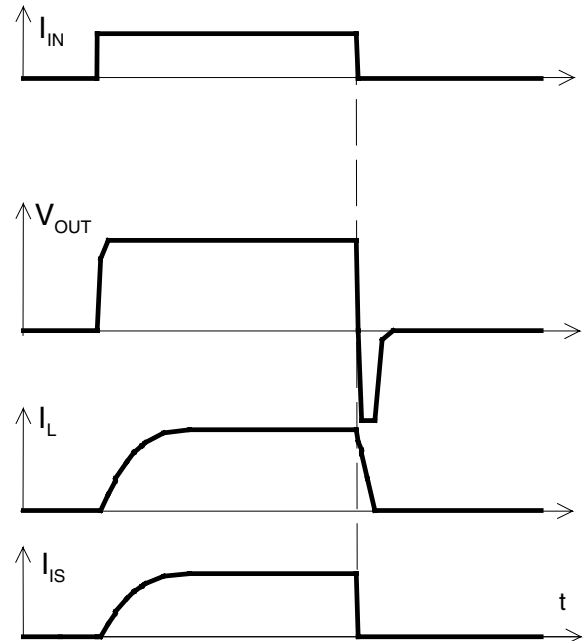


Figure 3a: Short circuit:

shut down by overtemperature detection with auto restart on cooling

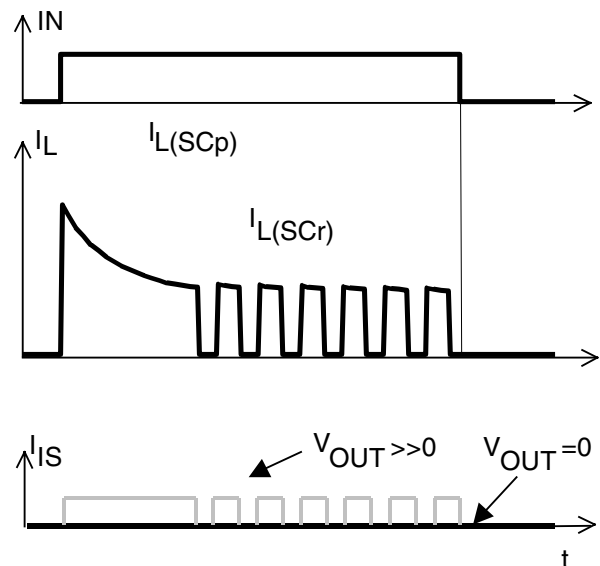


Figure 4a: Overtemperature
Reset if $T_j < T_{jt}$

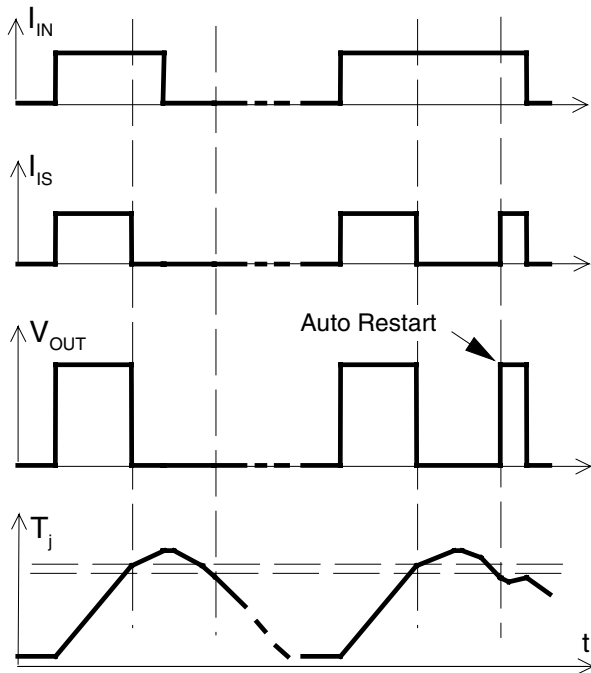
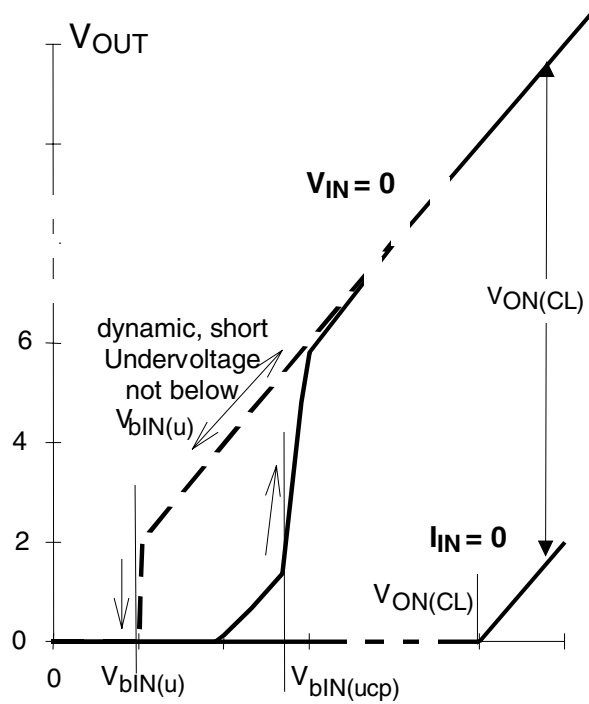


Figure 6a: Undervoltage restart of charge pump, overvoltage clamp



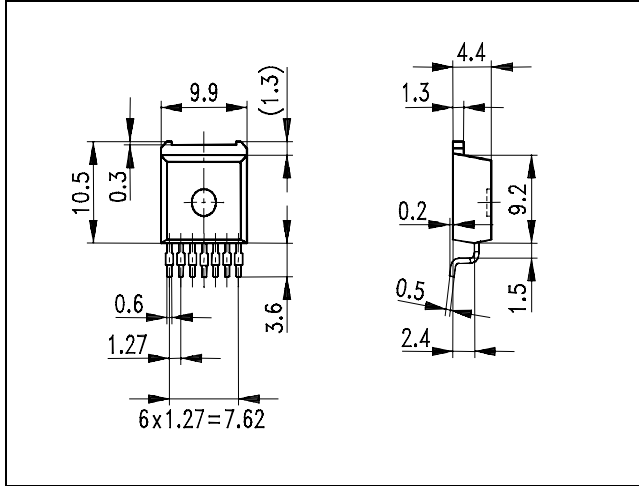
Package and Ordering Code

All dimensions in mm

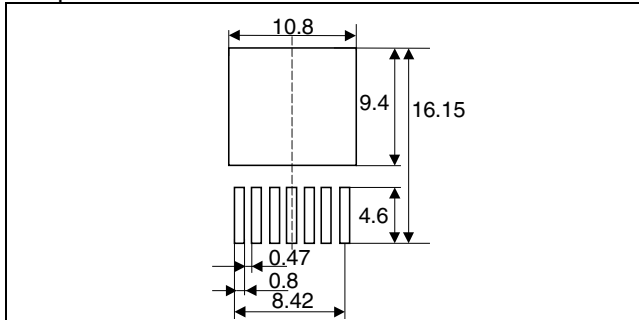
SMD TO 220-7,

Ordering code

BTS 6510 B	T&R:	Q67060-S6311
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