puts.



General Description

Applications

The MAX1773 highly integrated IC serves as the control

logic for a system with multiple power sources. It direct-

ly drives external P-channel MOSFETs to select from an

AC adapter and dual battery sources for charge and discharge. The selection is made based on the pres-

ence of the power sources and the state of the batter-

ies. The MAX1773 detects low battery conditions using

integrated analog comparators and checks for the

presence of a battery by using battery thermistor out-

The MAX1773 is designed for use with a buck topology

charger. It provides a simple and easily controlled solu-

tion to a difficult analog power control problem. The

MAX1773 provides most of the power source monitoring and selection, freeing the system power manage-

ment microprocessor (µP) for other tasks. This not only

simplifies development of the power management firmware for the μ P but also allows the μ P to enter

standby, thereby reducing system power consumption.

Notebook and Subnotebook Computers

PDAs and Handy-Terminals

Dual-Battery Portable Equipment

Internet Tablets

Power Source Selector for Dual-Battery Systems

Features

- Patented[†] 7-MOSFET Topology Offers Low-Cost Solution
- Automatically Detects and Responds to: Low Battery Voltage Condition Battery Insertion and Removal AC Adapter Presence
- Direct Drive of P-Channel MOSFETs
- ♦ Simplifies Power Management µP Firmware
- Extends Battery Life by Allowing Power Management µP to Enter Standby
- ♦ 4.75V to 28V AC Adapter Input Voltage Range
- Integrated LDO with 1mA Drive Capability
- Small Footprint 20-Pin TSSOP Package

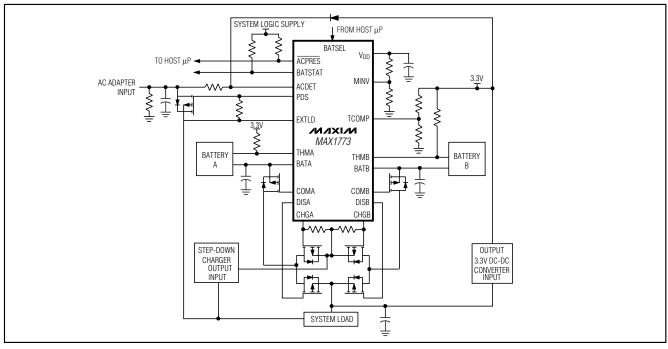
Ordering Information

PART	TEMP. RANGE	PIN-PACKAGE
MAX1773EUP	-40°C to +85°C	20 TSSOP

Pin Configuration appears at end of data sheet.

[†]Covered by U.S. Patent number 5,764,032.

Typical Operating Circuit



_ Maxim Integrated Products 1

For price, delivery, and to place orders, please contact Maxim Distribution at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

ABSOLUTE MAXIMUM RATINGS

VBATA, VBATB tO GND	0.3V to +20V
V _{COMA} to GND	0.3V to (V _{BATA} + 0.3V)
VCOMB to GND	
VCHGA, VCHGB, VEXTLD, VACDET to	o GND0.3V to +30V
VPDS, VDISA, VDISB to GND	0.3V to (V _{EXTLD} + 0.3V)
VDD, VBATSEL, VACPRES, VBATSTA	t, Vtcomp,
V _{MINV} to GND	0.3V to +6V
VTHMA, VTHMB (Note 1)	0.3V to +6V

Continuous Current out of THMA, THMB	20mA
I ACPRES, IBATSTAT Sink Current	30mA
Continuous Power Dissipation ($T_A = +70^{\circ}C$)	
20-Pin TSSOP (derate 7.0mW/°C above +70°C)	560mW
Operating Temperature40°C t	o +85°C
Storage Temperature65°C to	+150°C
Lead Temperature (soldering, 10s)	.+300°C

Note 1: Signals on THMA and THMB below -0.3V are clamped by internal diodes limit forward diode current to maximum continuous current. When voltage on these pins is below -0.3V.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

 $(V_{BATA} = V_{BATB} = 16.8V, C_{VDD} = 3.3\mu F, V_{MINV} = 0.93V, V_{EXTLD} = V_{ACDET} = 28V, V_{TCOMP} = 3V, V_{THMA} = V_{THMB} = 1.65V, V_{BATSEL} = 0, C_{COMA} = C_{COMB} = C_{DISA} = C_{DISB} = C_{CHGA} = C_{CHGB} = C_{PDS} = 5nF, T_{A} = 0^{\circ}C to +85^{\circ}C, unless otherwise noted.)$

PARAMETER	CONDIT	MIN	ТҮР	МАХ	UNITS	
EXTLD Supply Voltage Range	$V_{EXTLD} > V_{BATA}$ and V_{BATB}		4.75		28	V
BATA, BATB Supply Voltage Range			4.75		19	V
	$V_{BATA} = 4.75V$ to 19V,	V _{ACDET} = 28V		5	8	
BATA, BATB Quiescent Current (Current from the higher voltage supply)	$V_{BATB} = 4.75V$ to 19V, IVDD = 0	$V_{ACDET} = 2.2V$ to V_{BATA} and V_{BATB}		40	70	μA
	$V_{BATA} = 4.75V$ to 19V,	V _{ACDET} = 28V		5	8	
BATA, BATB Quiescent Current (Current from the lower voltage supply)	$V_{PATP} = 4.75 V \text{ to } 19 V$			8	13	μA
	VACDET = 28V, VEXTLD =	= 28V		35	55	
EXTLD Quiescent Current	V _{ACDET} = 2.2V to V _{BATA} V _{EXTLD} = 16V		5	8	μA	
LINEAR REGULATOR	·		•			
V _{DD} Output Voltage	$I_{VDD} = 0$ to $100\mu A$		3.234	3.3	3.367	v
	$I_{VDD} = 100 \mu A \text{ to } 1 m A$	3.168	3.3	3.432	v	
	V_{BATA} or $V_{BATB} = 5V$ to			1.0		
Power-Supply Rejection Ratio	$V_{BATA} = V_{BATB} = 5V, V_{E}$	XTLD = 5V to 28V			1.0	mV/V
	V_{BATA} , V_{BATB} , or $V_{EXTLD} = 5V$ to 19V, sawtooth at 10V/µs, other supplies = 12V			1		1110/0
V _{DD} Undervoltage Lockout	Hysteresis is typically 50)mV	2.0	2.5	3.0	V
COMPARATORS						
TCOMP Undervoltage Lockout (Note 2)			0		1.1	V
THM_ Input Voltage Range					5.5	V
THM_ Input Leakage Current	$V_{THM} = 5.5V$		0.1	100	nA	
	$V_{THMA} = V_{THMB} = 0 \text{ to } 5.5V$ $V_{THMA} = V_{THMB} = 0 \text{ to } 5.5V, V_{BATA} = V_{BATB}$ $= V_{EXTLD} = 4.75V$		0		5.5	
TCOMP Input Voltage Range			0		4.3	V

ELECTRICAL CHARACTERISTICS (continued)

 $(V_{BATA} = V_{BATB} = 16.8V, C_{VDD} = 3.3\mu F, V_{MINV} = 0.93V, V_{EXTLD} = V_{ACDET} = 28V, V_{TCOMP} = 3V, V_{THMA} = V_{THMB} = 1.65V, V_{BATSEL} = 0, C_{COMA} = C_{COMB} = C_{DISA} = C_{DISB} = C_{CHGA} = C_{CHGB} = C_{PDS} = 5nF, T_A = 0^{\circ}C to +85^{\circ}C, unless otherwise noted.)$

PARAMETER	CONDI	MIN	ТҮР	МАХ	UNITS	
TCOMP Input Leakage Current	V _{TCOMP} = 5.5V		0.1	100	nA	
THM_ to TCOMP Trip Threshold	THM_ falling with respec	-30		30	mV	
THM_ to TCOMP Hysteresis			15	50		mV
ACDET Operating Voltage Range (Note 3)			2.2		28	V
ACDET Logic Threshold High			2.2			V
	VACDET = 3V, VACDET <	V_{BATA} and V_{BATB}		4	8	
ACDET Input Bias Current	VACDET = 3V, VACDET <	: V _{BATB} , V _{BATA} = 0		5	9	μA
	VACDET = 28V, VACDET	$> V_{BATA}$ and V_{BATB}		6	11	
ACDET to BATA Trip Threshold	VACDET falling with resp	0	50	100	mV	
ACDET to BATA Hysteresis			100	150	200	mV
ACDET to BATB Trip Threshold	VACDET falling with resp	ect to V _{BATB}	0	50	100	mV
ACDET to BATB Hysteresis		100	150	200	mV	
MINV Operating Voltage Range	$V_{BATA} = V_{BATB} = 5 \times V_{N}$	/INV	0.93		2.6	V
MINV Input Bias Current	$V_{MINV} = 0.93V$ to 2.6V		-100		100	nA
DAT Minimum Voltage Trip Threshold	Vara folling	$V_{MINV} = 0.93V$	4.55	4.65	4.75	- v
BAT_ Minimum Voltage Trip Threshold	V _{BAT} _ falling	$V_{MINV} = 2.6V$	12.7	13	13.3	
BATSEL Input Low Voltage	Typical hysteresis is 100)mV			0.8	V
BATSEL Input High Voltage			2.0			V
BATSEL Input Leakage Current	$V_{BATSEL} = 5.5V$			1	μΑ	
BATSEL Action Delay			20		100	μs
GATE DRIVERS						
COM_ Initial Source Current	V _{BAT} = 16.8V, V _{COM} = 14.8V		5			mA
COM Final Source Current	V _{BAT} = 16.8V, V _{COM} = 16.4V		10			
COM_ Final Source Current	V _{BAT} = 16.8V, V _{COM} = 14.8V		50	100	150	μA
COM_ Sink Current (PMOS Turn-On) (Note 4)	V _{COM} _ = 11.8V, V _{BAT} _ =	= 16.8V	4			mA
COM_ Turn-On Clamp Voltage	$V_{BAT} = 8V$ to 19V		-11.5	-9.5	-7.5	
(V _{COM} to V _{BAT})	V _{BAT} = 4.75V to 8V		-8.00		-4.25	V
PDS Source Current (PMOS Turn-Off)	VPDS = 10V, VEXTLD = 1	2V	5			mA
PDS Sink Current (PMOS Turn-On)	V _{PDS} = 2V to 28V	0.8	1.0	1.2	mA	
PDS Leakage Current (PMOS Off)	V _{PDS} = 28V		0.1	2	μA	
CHG_ Sink Current (PMOS Turn-On)	V _{CHG} _ = 2V to 22V	0.7	1.0	1.3	mA	
CHG_ Leakage Current (PMOS Off)	V _{CHG} _ = 28V		0.1	2	μA	
DIS_ Initial Source Current	$V_{EXTLD} = 15V, V_{DIS} = 100$	5			mA	
	$V_{EXTLD} = 15V, V_{DIS} = 14.6V$		10			
DIS_ Final Source Current	V _{EXTLD} = 15V, V _{DIS} = 13V		50	100	150	μA
DIS_ Sink Current (PMOS Turn-On) (Note 5)	V _{EXTLD} = 16.8V, V _{DIS} =		4			mA

ELECTRICAL CHARACTERISTICS (continued)

 $(V_{BATA} = V_{BATB} = 16.8V, C_{VDD} = 3.3\mu F, V_{MINV} = 0.93V, V_{EXTLD} = V_{ACDET} = 28V, V_{TCOMP} = 3V, V_{THMA} = V_{THMB} = 1.65V, V_{BATSEL} = 0, C_{COMA} = C_{COMB} = C_{DISA} = C_{DISB} = C_{CHGA} = C_{CHGB} = C_{PDS} = 5nF, T_A = 0^{\circ}C to +85^{\circ}C, unless otherwise noted.)$

PARAMETER	CONDITIONS	MIN	ТҮР	МАХ	UNITS	
DIS_ Turn-On Clamp Voltage	V _{EXTLD} = 8V to 28V		-9.5	-7.5	v	
(V _{DIS_} to V _{EXTLD})	$V_{EXTLD} = 4.75V$ to 8V	-8.00		-4.25	V	
STATUS OUTPUTS						
ACPRES Sink Current	$V\overline{\text{ACPRES}} = 0.4V$	1			~ ^	
ACPRES SINK Current	$V\overline{\text{ACPRES}} = 5.5V$			30	mA	
BATSTAT Sink Current	VBATSTAT = 0.4V	1			mA	
BATSTAT SIIK Current	VBATSTAT = 5.5V				ША	
ACPRES Leakage Current	$V\overline{\text{ACPRES}} = 5.5V$		0.1	1	μA	
BATSTAT Leakage Current	VBATSTAT = 5.5V		0.1	1	μΑ	
TRANSITION TIMES						
Battery Switchover Delay (Note 6)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			5	μs	
Battery Action Delay (Note 7)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			260	μs	
Thermistor Action Delay (Note 8)	V _{ACDET} = 2.2V, V _{MINV} = 0.93V			12	μs	
AC to Battery Switchover Delay (Note 9)	V _{ACDET} = 2.2V, V _{MINV} = 0.93V			10	μs	
Battery to AC Switchover Delay (Note 10)	V _{ACDET} = 2.2V, V _{MINV} = 0.93V			260	μs	
CHG_Turn-On Delay (Note 11)		130	300	530	μs	

ELECTRICAL CHARACTERISTICS

 $(VBATA = VBATB = 16.8V, CVDD = 3.3\mu F, VMINV = 0.93V, VEXTLD = VACDET = 28V, VTCOMP = 3V, VTHMA = VTHMB = 1.65V, VBATSEL = 0, CCOMA = CCOMB = CDISA = CDISB = CCHGA = CCHGB = CPDS = 5nF, TA = -40°C to +85°C, unless otherwise noted.)$

PARAMETER	COND	MIN	ТҮР	MAX	UNITS	
EXTLD Supply Voltage Range	V _{EXTLD} > V _{BATA} and V	4.75		28	V	
BATA, BATB Supply Voltage Range					19	V
	$V_{BATA} = 4.75V$ to 19V,	V _{ACDET} = 28V			8	
BATA, BATB Quiescent Current (Current from the higher voltage supply)	$V_{BATB} = 4.75V \text{ to } 19V,$ $I_{VDD} = 0$				70	μA
	$V_{BATA} = 4.75V \text{ to } 19V,$	V _{ACDET} = 28V			8	
BATA, BATB Quiescent Current (Current from the lower voltage supply)	$V_{\text{BATB}} = 4.75V \text{ to } 19V,$ $V_{\text{ACDET}} = 2.2V \text{ to}$ $V_{\text{DD}} = 0$ $V_{\text{BATA}} \text{ and } V_{\text{BATB}}$				13	μA
EXTLD Quiescent Current	V _{ACDET} = 28V, V _{EXTLD} = 28V				55	
	$V_{ACDET} = 2.2V$ to V_{BATA} and V_{BATB} , $V_{EXTLD} = 16V$				8	μA
LINEAR REGULATOR						
V _{DD} Output Voltage	$I_{VDD} = 0$ to $100\mu A$		3.234		3.367	V
VDD Output Voltage	$I_{VDD} = 100\mu A$ to 1mA	$I_{VDD} = 100\mu A$ to 1mA			3.432	v
V _{DD} Power-Supply Rejection Ratio	V_{BATA} or $V_{BATB} = 5V$ to	o 19V, V _{EXTLD} = 5V			1.0	mV/V
V_{DD} rower-supply Rejection Ratio $V_{\text{BATA}} = V_{\text{BATB}} = 5V, V_{\text{EXTLD}} = 5V \text{ to } 28V$				1.0	mv/v	
V _{DD} Undervoltage Lockout	Hysteresis is typically 5	2.0		3.0	V	
COMPARATORS						
TCOMP Undervoltage Lockout (Note 2)			0		1.1	V

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ELECTRICAL CHARACTERISTICS (continued)

 $(V_{BATA} = V_{BATB} = 16.8V, C_{VDD} = 3.3 \mu F, V_{MINV} = 0.93V, V_{EXTLD} = V_{ACDET} = 28V, V_{TCOMP} = 3V, V_{THMA} = V_{THMB} = 1.65V, V_{BATSEL} = 0, C_{COMA} = C_{COMB} = C_{DISA} = C_{CHGA} = C_{CHGB} = C_{PDS} = 5nF, T_A = -40^{\circ}C to +85^{\circ}C, unless otherwise noted.)$

PARAMETER	CONDITIONS			TYP	MAX	UNITS	
THM_Input Voltage Range					5.5	V	
THM_Input Leakage Current	V _{THM} _= 5.5V				100	NA	
	VTHMA = VTHMB = 0 to	5.5V	0		5.5		
TCOMP Input Voltage Range	$V_{THMA} = V_{THMB} = 0$ to				V		
	VBATA = VBATB = VEX	(TLD = 4.75V	0		4.3		
TCOMP Input Leakage Current							
THM_ to TCOMP Trip Threshold							
THM_ to TCOMP Hysteresis							
ACDET Operating Voltage Range (Note 3)			2.2		28	V	
ACDET Logic Threshold High			2.2			V	
	VACDET = 3V, VACDET	< VBATA and VBATB			8		
ACDET Input Bias Current	VACDET = 3V, VACDET	r < V _{BATB} , V _{BATA} = 0			9	μA	
	VACDET = 28V, VACDE	$T > V_{BATA}$ and V_{BATB}			11	_	
ACDET to BATA Trip Threshold	VACDET falling with res	spect to V _{BATA}	-35		125	mV	
ACDET to BATA Hysteresis			100		200	mV	
ACDET to BATB Trip Threshold	VACDET falling with res	-35		125	mV		
ACDET to BATB Hysteresis			100		200	mV	
MINV Operating Voltage Range	$V_{BATA} = V_{BATB} = 5 \times V_{MINV}$		0.93		2.6	V	
MINV Input Bias Current	$V_{MINV} = 0.93V$ to 2.6V	1	-100		100	nA	
DAT Minimum Voltage Trip Threshold	Vala folling	$V_{MINV} = 0.93V$	4.55		4.75	i v	
BAT_ Minimum Voltage Trip Threshold	$V_{BAT_}$ falling $V_{MINV} = 2.6V$		12.7		13.3		
BATSEL Input Low Voltage	Typical hysteresis is 1	00mV			0.8	V	
BATSEL Input High Voltage			2.0			V	
BATSEL Input Leakage Current	V _{BATSEL} = 5.5V				1	μΑ	
BATSEL Action Delay			20		100	μs	
GATE DRIVERS							
COM_ Initial Source Current	V _{BAT} = 16.8V, V _{COM}	_ = 14.8V	4			mA	
COM_ Final Source Current	$V_{BAT_} = 16.8V, V_{COM}$	_ = 16.4V	10				
COM_ Final Source Current	V _{BAT} = 16.8V, V _{COM} = 14.8V		50		150	μA	
COM_ Sink Current (PMOS Turn-On) (Note 4)	V _{COM} _ = 11.8V, V _{BAT} .	2			mA		
COM_ Turn-On Clamp Voltage	$V_{BAT_{-}} = 8V \text{ to } 19V$		-11.5		-7.25	v	
(V _{COM} _ to V _{BAT} _)	V _{BAT} = 4.75V to 8V		-8.00		-4.25	v	
PDS Source Current (PMOS Turn-Off)	V _{PDS} = 10V, V _{EXTLD} = 12V		4			mA	
PDS Sink Current (PMOS Turn-On)	$V_{PDS} = 2V \text{ to } 28V$	0.7		1.3	mA		
PDS Leakage Current (PMOS Off)	V _{PDS} = 28V				2	μA	
CHG_ Sink Current (PMOS Turn-On)	V _{CHG} = 2V to 22V		0.6		1.4	mA	

ELECTRICAL CHARACTERISTICS (continued)

(VBATA = VBATB = 16.8V, CVDD = 3.3µF, V_{MINV} = 0.93V, VEXTLD = VACDET = 28V, V_{TCOMP} = 3V, V_{THMA} = V_{THMB} = 1.65V, VBATSEL = 0, CCOMA = CCOMB = CDISA = CDISB = CCHGA = CCHGB = CPDS = 5nF, **TA** = -40°C to +85°C, unless otherwise noted.)

PARAMETER	CONDITIONS	MIN	ТҮР	MAX	UNITS	
CHG_ Leakage Current (PMOS Off)	$V_{CHG_} = 28V$			2	μA	
DIS_ Initial Source Current	$V_{EXTLD} = 15V, V_{DIS} = 13V$	4				
DIS_ Final Source Current	$V_{EXTLD} = 15V, V_{DIS} = 14.6V$	10			μA	
DIS_ Final Source Current	$V_{EXTLD} = 15V, V_{DIS} = 13V$	50		150	μΑ	
DIS_Sink Current (PMOS Turn-On) (Note 5)	V _{EXTLD} = 16.8V, V _{DIS} = 11.8V	2			mA	
DIS_Turn-On Clamp Voltage	$V_{EXTLD} = 8V$ to $28V$	-11.5		-7.25	v	
(V _{DIS} to V _{EXTLD})	$V_{EXTLD} = 4.75V$ to 8V	-8.00		-4.25	v	
STATUS OUTPUTS						
ACPRES Sink Current	$V\overline{\text{ACPRES}} = 0.4V$	1			mA	
ACPRES SINK CUITEIN	$V\overline{\text{ACPRES}} = 5.5V$			30		
BATSTAT Sink Current	VBATSTAT = 0.4V	1	1		- mA	
BATSTAT SINK GUNENI	VBATSTAT = 5.5V	r = 5.5V		30		
ACPRES Leakage Current	$V\overline{\text{ACPRES}} = 5.5V$			1	μA	
BATSTAT Leakage Current	VBATSTAT = 5.5V			1	μA	
TRANSITION TIMES						
Battery Switchover Delay (Note 6)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			5	μs	
Battery Action Delay (Note 7)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			260	μs	
Thermistor Action Delay (Note 8)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			12	μs	
AC to Battery Switchover Delay (Note 9)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			10	μs	
Battery to AC Switchover Delay (Note 10)	$V_{ACDET} = 2.2V, V_{MINV} = 0.93V$			260	μs	
CHG_Turn-On Delay (Note 11)		130		530	μs	

Note 2: TCOMP undervoltage lockout sets the MAX1773's internal status bits for the batteries to be designated as "absent" (VTHM_ > VTCOMP).

Note 3: VACDET must remain above 2.2V, except in power-up.

Note 4: COMA cannot sink current until V_{COMB} > V_{BATB} - 2V. Likewise, COMB cannot sink current until V_{COMA} > V_{BATA} - 2V.

Note 5: DISA cannot sink current until V_{DISB} > V_{EXTLD} - 2V. Likewise, DISB cannot sink current until V_{DISA} > V_{EXTLD} - 2V.

Note 6: Battery Switchover Delay starts when either V_{COM} or V_{DIS} of the connected battery begins to rise and ends when both V_{COM} and V_{DIS} of the other battery have fallen 3V below their sources (Figures 1 and 2).

Note 7: Battery Action Delay starts when the connected battery's voltage falls below $5 \times V_{MINV}$ and ends when both V_{COM} and V_{DIS} of the other battery have fallen 3V below their sources (Figures 1 and 2).

Note 8: Thermistor Action Delay begins when V_{THM} of the connected battery rises above V_{TCOMP} and ends when both V_{COM} and V_{DIS} of the other battery have fallen 3V below their sources (Figures 3 and 4).

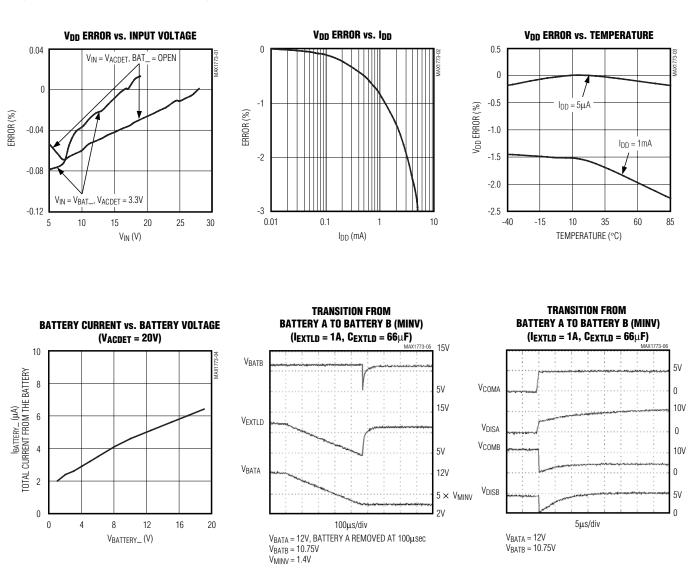
Note 9: AC to Battery Switchover Delay begins when V_{ACDET} falls below its threshold and ends when both V_{COM} and V_{DIS} of the battery being switched to have fallen 3V below their sources (Figure 5).

Note 10: Battery to AC Switchover Delay begins when VACDET rises above its threshold and ends when VDIS_ of the battery being switched from has begun to rise (Figure 6).

Note 11: CHG_Turn-on Delay begins when V_{CHG} of the battery being switched from begins to rise and ends when V_{CHG} of the battery being switched to begins to fall (Figures 7 and 8).



Typical Operating Characteristics

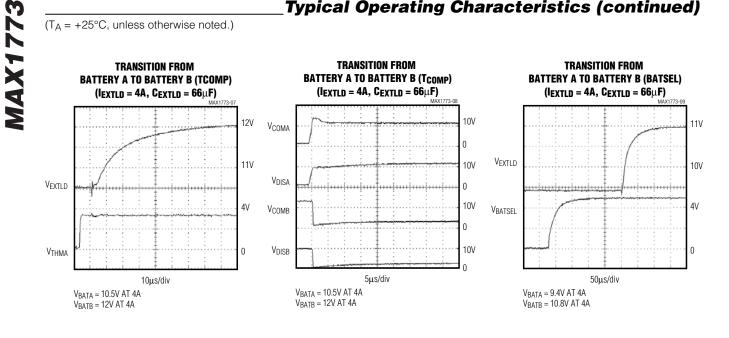


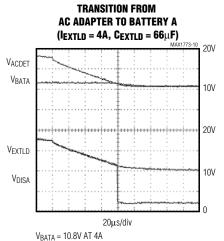
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 $(T_A = +25^{\circ}C, unless otherwise noted.)$

Typical Operating Characteristics (continued)

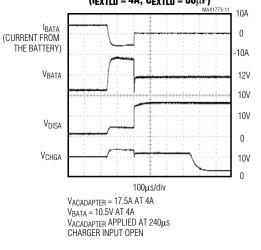
 $(T_A = +25^{\circ}C, \text{ unless otherwise noted.})$





VACADAPTER = 17.5V AT 4A

TRANSITION FROM TRANSITION FROM BATTERY A TO AC ADAPTER (IEXTLD = 4A, CEXTLD = 66 μ F)



Pin Description

	[
PIN	NAME	FUNCTION					
1	BATA	attery A Connection					
2	THMA	Thermistor A Input					
3	CHGA	Open-Drain Gate Driver for Charge Path MOSFET to Battery A					
4	DISA	Gate Driver for Discharge Path MOSFET to Battery A. Switches from VEXTLD to (VEXTLD - 9.5V).					
5	COMA	Gate Driver for Common Path MOSFET to Battery A. Switches from V_{BATA} to (V_{BATA} - 9.5V).					
6	GND	Ground					
7	MINV	Minimum Operating Voltage Set Point. The battery voltage switchover set point is $5 \times V_{MINV}$.					
8	EXTLD	External Load Connection. Source connection for the PDS, DISA, and DISB MOSFETs.					
9	PDS	Gate Driver for the AC Adapter MOSFET					
10	ACDET	AC Adapter Detection Input					
11	BATSTAT	Open-Drain Battery Status Output. Use a pullup resistor to the system logic supply.					
12	ACPRES	Open-Drain AC Presence Output. Use a pullup resistor to the system logic supply.					
13	BATSEL	Battery Select Digital Input. Selects which battery to charge or discharge.					
14	TCOMP	Externally Set Thermistor Trip Point. Sets the thermistor voltage level for detecting the battery's presence.					
15	V _{DD}	Linear Regulator Output					
16	COMB	Gate Driver for Common Path MOSFET to Battery B. Switches from V_{BATB} to (V_{BATB} - 9.5V).					
17	DISB	Gate Driver for Discharge Path MOSFET to Battery B. Switches from VEXTLD to (VEXTLD - 9.5V).					
18	CHGB	Open-Drain Gate Driver for Charge Path MOSFET to Battery B					
19	THMB	Thermistor B Input					
20	BATB	Battery B Connection					

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(V_{COM_GS} = COM_ turn-on clamp voltage, V_{DIS_GS} = DIS_ turn-on clamp voltage, V_{CHARGER} = system step-down charger output.)

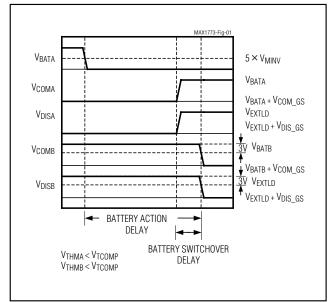


Figure 1. Battery Delay (Battery A to Battery B)

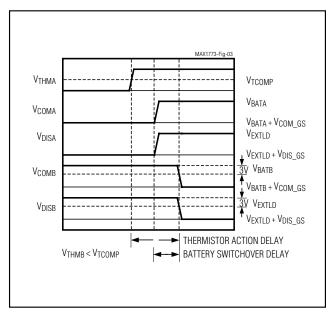


Figure 3. Thermistor Switchover Delay (Battery A to Battery B)

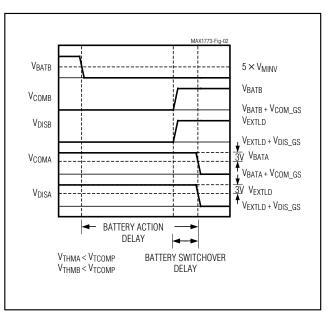


Figure 2. Battery Delay (Battery B to Battery A)

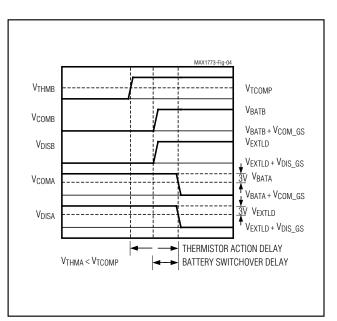


Figure 4. Thermistor Switchover Delay (Battery B to Battery A)

Transition Time Diagrams



_Transition Time Diagrams (continued)

(V_{COM_GS} = COM_ turn-on clamp voltage, V_{DIS_GS} = DIS_ turn-on clamp voltage, V_{CHARGER} = system step-down charger output.)

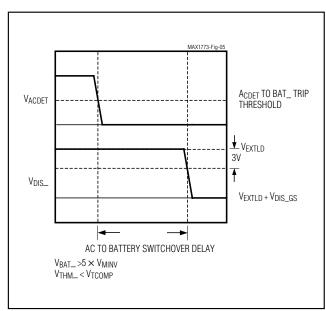


Figure 5. AC to Battery Switchover Delay

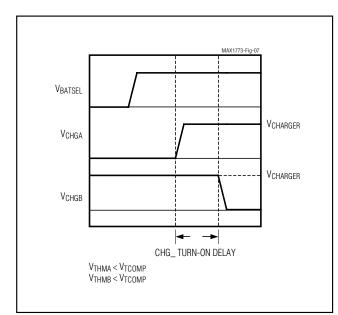


Figure 7. Charge Turn-On Delay (Battery A to Battery B)

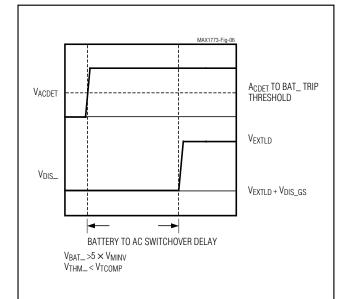


Figure 6. Battery to AC Switchover Delay

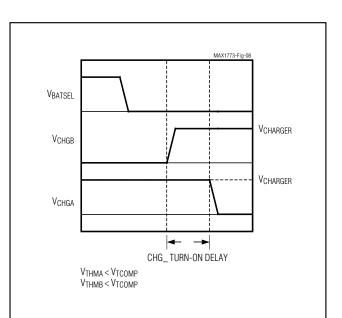


Figure 8. Charge Turn-On Delay (Battery B to Battery A)

Table 1. AC Adapter States

BATSEL	BATTERY A	BATTERY B	BATSTAT	CONNECTION STATE
0	Present	Х	0	AC adapter is connected to load. Battery A's charge path connected.
0	Absent	Х	1	AC adapter is connected to load.
1	Х	Present	1	AC adapter is connected to load. Battery B's charge path connected.
1	Х	Absent	0	AC adapter is connected to load.

X = Don't care, Present: VTHM_ < VTCOMP, Absent: VTHM_ > VTCOMP, ACPRES = 0

BATSEL BATTERY A **BATTERY B** VBATA VBATB BATSTAT CONNECTION STATE 0 Present $>5 \times V_{MINV}$ Х Х 0 Battery A is connected to the load. Х Present $>5 \times V_{MINV}$ Absent Х 0 Battery A is connected to the load. Х Present $>5 \times V_{MINV}$ Х $< 5 \times V_{MINV}$ 0 Battery A is connected to the load. Х Х 1 $<5 \times V_{MINV}$ Present $> 5 \times V_{MINV}$ Battery B is connected to the load. Х Х Present 1 Absent $> 5 \times V_{MINV}$ Battery B is connected to the load. 1 Х 1 Х Present $> 5 \times V_{MINV}$ Battery B is connected to the load.

Table 2. Simplified Standard Battery States (without latches)

X = Don't care, Present: V_{THM} < V_{TCOMP}, Absent: V_{THM} > V_{TCOMP}

Detailed Description

The MAX1773 provides the functions necessary to allow an external controller to manage the power connections needed for two battery packs, an AC adapter input, a battery charger, and the system load. The MAX1773 uses seven PMOS FETs to provide all the switching necessary in systems using a step-down charger powered by the AC adapter (Figures 9 and 10). The MAX1773 automatically adapts to many transient conditions—such as AC plug-in, battery hot swapping, and battery switchover—to provide constant power to the system without requiring real-time support from an external controller. The MAX1773 draws its power from the highest voltage supply present (Figure 11).

Battery Detection

The MAX1773 monitors the battery's thermistor voltage to determine the presence of the battery. The device compares the battery's thermistor voltage (VTHM_) to the thermistor trip point (VTCOMP). If VTHM_ < VTCOMP, then the MAX1773 assumes that the battery is present. However, if VTHM_ > VTCOMP, the MAX1773 assumes that the battery is absent and does not charge or discharge the battery.

Modes of Operation

The MAX1773 provides three modes of operation. Startup States mode provides functionality when the MAX1773 is initially powered by a battery when no AC adapter is present. AC adapter States mode provides functionality when an AC Adapter is present. Standard Battery States mode provides functionality when one or both batteries are present, the AC adapter is not present, and EXTLD is above 2.2V. The Standard Battery States mode requires an external supply with an output voltage between 2.2V and 4.5V for ACDET, as shown in Figure 10. The external power supply must be powered from EXTLD.

AC Adapter States

The MAX1773 checks for the presence of an AC adapter by sensing the voltage at ACDET. When VACDET exceeds the batteries' voltage and 4.75V, then the MAX1773 uses the AC adapter to power the load. In addition, if the selected battery is present, the MAX1773 connects the selected battery's charge path. See Table 1 for a detailed listing of the MAX1773 states for operation with an AC adapter detected.

Standard Battery States

When the AC adapter power supply is not present, the MAX1773 uses the batteries to supply the load. BAT-SEL allows an external controller to select a battery. Table 2 shows the simplified standard battery states that normally control operation. However, the Battery Switchover Latch, the Low-Battery Latch, and the Discharged Battery Latch are able to suspend the state table and provide additional functionality.



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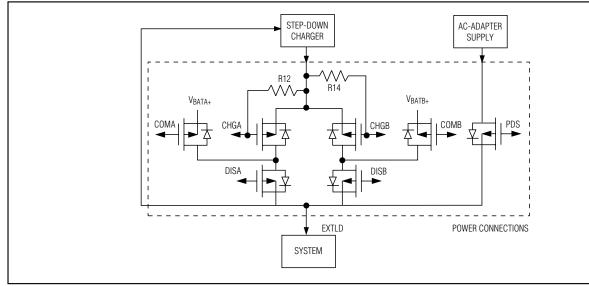


Figure 9. 7-MOSFET Topology

VBATA	VBATB	BATTERY A	BATTERY B	CONNECTION STATE
$>5 \times V_{MINV}$	Х	Present	Х	Battery A is connected to the load.
$< 5 \times V_{MINV}$	$>5 \times V_{MINV}$	Present	Present	Battery B is connected to the load.
Х	$>5 \times V_{MINV}$	Absent	Present	Battery B is connected to the load.
Х	Х	Absent	Absent	No connections.
$< 5 \times V_{MINV}$	$<5 \times V_{MINV}$	Х	Х	No connections.
$< 5 \times V_{MINV}$	Х	Х	Absent	No connections.
Х	$<5 \times V_{MINV}$	Absent	Х	No connections.

Table 3. Startup States

X = Don't care, Present: V_{THM} < V_{TCOMP}, Absent: V_{THM} > V_{TCOMP}

The Battery Switchover Latch stops the MAX1773 from oscillating when the device switches from the selected battery and then the selected battery's voltage recovers. According to the state table, the MAX1773 would switch back to the selected battery as soon as the battery's voltage recovered. The Battery Switchover Latch suspends the state table as soon as the MAX1773 switches over to the nonselected battery. This causes the MAX1773 to continue to power from the nonselected battery unless the latch is cleared. The Battery Switchover Latch is cleared when BATSEL is toggled (to select the other battery), when in the Startup States mode, in the AC Adapter States mode, and when the selected battery is removed (VTHM_ > VTCOMP).

To prevent the MAX1773 from switching to a discharged battery, the Low-Battery Latch suspends the state table when the unconnected battery's voltage is below $5 \times V_{MINV}$ and the discharging battery's voltage drops below $5 \times V_{MINV}$. Instead of switching to the unconnected battery, the MAX1773 continues to power from the discharging battery. This latch is cleared when the unconnected battery is removed (V_{THM_} > V_{TCOMP}), when in the Startup States mode, when in the AC Adapter States mode, and if the unconnected battery's voltage rises above $5 \times V_{MINV}$.

The Discharged Battery Latch sets whenever the MAX1773 is in the Standard Battery States mode, both batteries are present (V_{THM} < V_{TCOMP}), one of the batteries is low (V_{BAT} < 5 × V_{MINV}), and the other battery's voltage is below V_{ACDET} . While the Discharged Battery Latch is set, the state table is suspended, the MAX1773 is not allowed to switch batteries, and the

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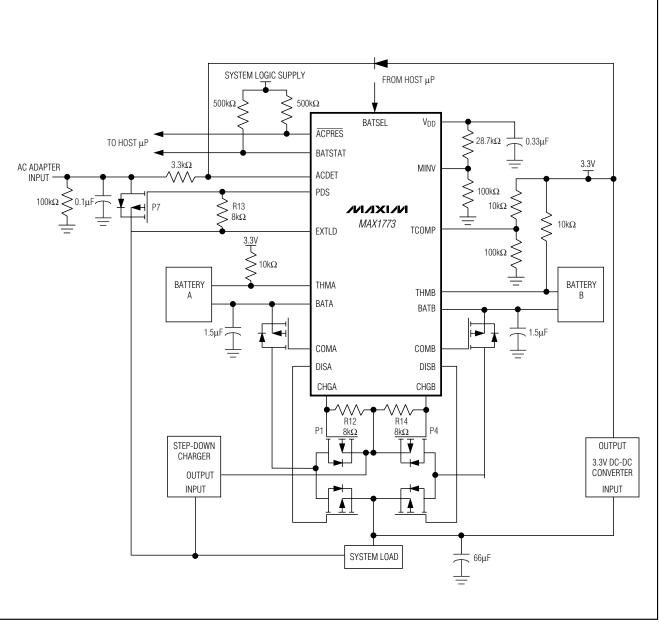


Figure 10. Standard Application Circuit

Low Battery Latch is cleared. The Discharged Battery Latch is cleared when both batteries are above V_{ACDET}, in the AC Adapter States mode, and in the Startup States mode.

Startup States

When VACDET rises at startup, the MAX1773 uses Startup States. See Table 3 for a detailed listing of the MAX1773 states in this mode. Note that once ACDET rises above 2.2V, the MAX1773 is no longer in the Startup States mode and enters either the Standard Battery States mode or the AC Adapter States mode.



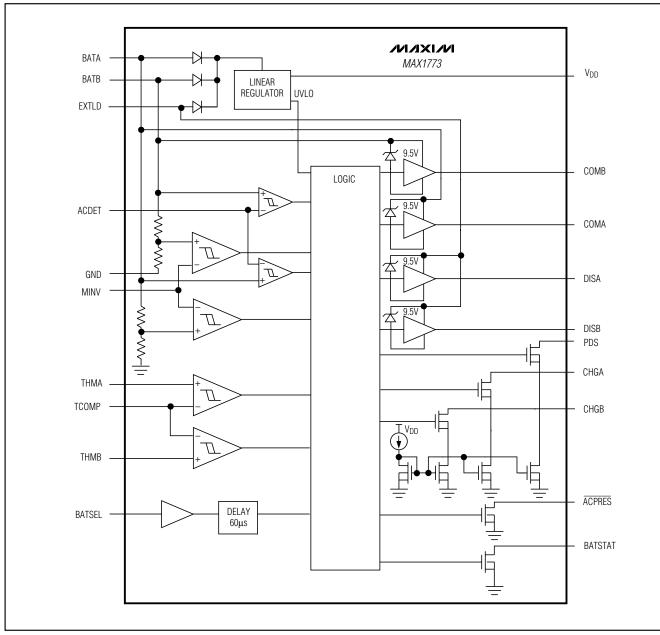


Figure 11. Functional Diagram

Status and Configuration

BATSTAT and ACPRES provide information to an external controller. Table 4 shows the different states of BATSTAT and ACPRES.

In the AC Adapter States mode, the BATSEL Action Delay (see *Electrical Characteristics*) allows the external controller to tell if both batteries are absent. When

both batteries are absent in the AC Adapter States mode and BATSEL changes states, BATSTAT is immediately updated. However, changes to the connection states are delayed (see Table 1 for connection states). If BATSEL is returned to its original state within the BATSEL Action Delay, then changes to the connection states are never made. Note that in the Standard



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Table 4. Status Bits

MODE	STATUS	BATSTAT	ACPRES
All	V _{DD} Undervoltage Lockout	1	1
Startup States		1	1
Standard Battery States	Selected Battery Discharge Path Connected	BATSEL	1
Standard Battery States	Other Battery Discharge Path Connected	BATSEL	1
AC Adapter States	Selected Battery Charge Path Connected	BATSEL	0
AC Adapter States	Selected Battery Absent	BATSEL	0

Battery States mode and in the AC Adapter States mode when one or both batteries are present, both BATSTAT and the connection states are delayed during the BATSEL Update Delay.

MOSFET Drivers

To minimize the time when no supply is connected to the external load during switchover transients, the MAX1773 uses active pullup drivers for the discharge paths (DIS_) and the common paths (COM_). When the MAX1773 initially begins to pull up one of these pins, it uses a large current (Initial COM_ Source Current and Initial DIS_ Source Current; see *Electrical Characteristics*). Once the COM_ voltage rises to within 2V of VBAT_ or the DIS_ voltage rises to within 2V of VEXTLD, then a weaker driver is used to hold up the voltage (Final COM_ Source Current and Final DIS_ Source Current; see *Electrical Characteristics*).

The MAX1773 is designed to prevent shoot-through from one battery to the other when transitioning from discharging one battery to discharging the other battery. To accomplish this, the MAX1773 does not connect the second battery to EXTLD until it senses that the first battery is disconnected from EXTLD. See Notes 4 and 5 of *Electrical Characteristics*.

To allow flexibility when choosing the higher voltage PDS PMOS FET (P7, Figure 10), the MAX1773 does not limit the gate-to-source voltage applied to the PDS PMOSFET. The minimum VGS is set by the MAX1773 PDS sink current (see *Electrical Characteristics*) and the external resistor from PDS to EXTLD (R13):

 $V_{GS(MIN)} = -I_{PDS(SINK)} \times R_{PDS}$

where $V_{GS(MIN)}$ is the minimum P7 gate-to-source voltage, $I_{PDS(SINK)}$ is the PDS sink current, and R_{PDS} is R13.

The MAX1773 uses open-collector drivers to open the charge paths. Minimize the value of the pullup resistors on the charge paths (R12 and R14) to allow the MAX1773 to quickly turn on the PMOS FETs; however,

keep the value large enough to prevent a lower V_{GS} than specified by the PMOS FET. The minimum V_{GS} is:

$V_{GS(MIN)} = -I_{CHG}(SINK) \times R_{CHG}$

where $V_{GS(MIN)}$ is the minimum P1 or P4 gate-to-source voltage, $I_{CHG_{SINK}}$ is the CHG_ sink current (see *Electrical Characteristics*), and $R_{CHG_{is}}$ is R12 or R14.

VDD Regulator

The MAX1773 features an internal linear regulator to provide power for itself and external circuitry. The linear regulator's output is available at V_{DD} and is nominally 3.3V. When the linear regulator is not used to power external circuitry, bypass it with a 0.33μ F ceramic capacitor. To supply external loads up to 1mA, bypass the linear regulator with a 3.3μ F tantalum capacitor.

Applications Information

Load Switchover Transients

When power switches from one power source to another, a transient is created on the load. This transient (ΔV_{EXTLD}) is minimized by the capacitance on the load (C_{EXTLD}). The voltage transient can be approximated as:

$$\Delta V_{EXTLD} = \frac{i_{EXLTLD} \times t_{SWITCHOVER}}{C_{EXTLD}}$$

where $\ensuremath{\mathsf{t}}\xspace{\mathsf{SWITCHOVER}}$ is the time where no supply is connected to the EXTLD.

In applications where the battery voltage always falls away slowly, tSWITCHOVER is primarily composed of the Battery Switchover Delay. However, in applications where the battery voltage can suddenly fall away, tSWITCHOVER is substantially increased because it is primarily composed of the Battery Action Delay (Figures 1 and 2).

Ideally, when a battery is removed from the system, the thermistor connection is broken before the battery's power path is broken. In this case, tSWITCHOVER is typi-



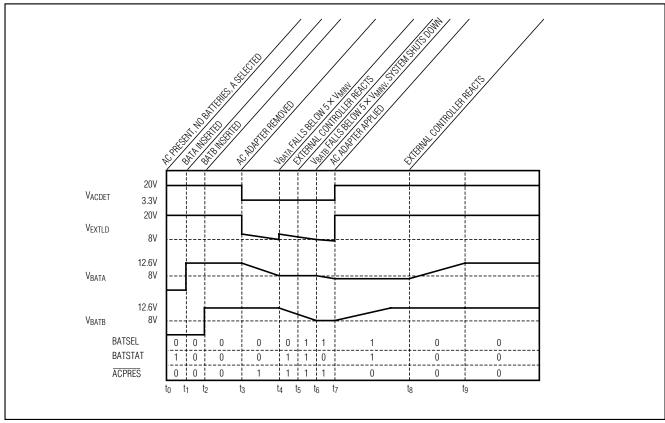


Figure 12. Charge/Discharge Example

cally bound by the Thermistor Action Delay (Figures 3 and 4). However, if the battery's power path is broken first, then t_{SWITCHOVER} primarily consists of the shorter of the following times: time until the thermistor connection is broken plus the Thermistor Action Delay, or the Battery Action Delay.

Source Switchover Transients

When the MAX1773 suddenly switches a power supply to the load, it creates a current transient from the source to charge up the capacitance on the load. The peak current drawn is approximated by:

$$I_{PK} = \frac{\Delta V_{EXTLOAD}}{R_{SOURCE} + R_{SWITCH} + R_{ESR}}$$

where $\Delta V_{EXTLOAD}$ is the voltage difference between the supply switched off and the supply switched on, RSOURCE is the source resistance of the power supply switched on, RSWITCH is the RDS(ON) of the PMOS FETs in the path, and RESR is the equivalent series resistance of the output capacitance.

The duration of the current transient is determined by RSOURCE, RSWITCH, RESR, and the output capacitance. Smaller resistances and less output capacitance reduce the transient duration.

Typical Operation

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Figure 12 shows a typical discharge and charge cycle for a system utilizing the MAX1773, two 3-cell lithium-ion (Li+) batteries, and a 20V AC adapter power supply. The diagram starts with the AC adapter applied, no batteries present, and battery A selected (see AC Adapter States). BATSTAT = BATSEL = 1 indicates that battery A is not present and battery A's charge path is not connected. If the external controller polled the MAX1773 as described in <u>Status and Configuration</u>, then BATSTAT would return BATSEL (0) to indicate that battery B is not present.

At t_1 , battery A is inserted and the MAX1773 connects battery A's charge path. Note that BATSTAT changes to BATSEL (0) to indicate that battery A is present.

At t₂, battery B is inserted. BATSTAT does not change and still indicates that battery A is present.



SUPPLIER	PHONE	FAX
Fairchild	408-822-2000	408-822-2102
IR	310-322-3331	310-322-3332
Siliconix	408-988-8000	408-970-3950

Table 5. Recommended Manufacturers

At t₃, the AC adapter is removed and the MAX1773 automatically disconnects battery A's charge path and connects battery A's discharge path (see *Standard Battery States*). ACPRES changes to 1 to indicate that the AC adapter source is no longer present. BATSTAT = BATSEL (0) to indicate that battery A is present and supplying the load. Between t₃ and t₄, battery A discharges as it supplies the load.

At t4, battery A's voltage falls below $5 \times V_{MIN}$, and the MAX1773 automatically disconnects battery A's discharge path and <u>connects</u> battery B's discharge path. BATSTAT goes to BATSEL (1) to indicate that battery A is no longer supplying the load.

Shortly after BATSTAT goes high, the external controller should catch up to the MAX1773 and change BATSEL. This is shown at t₅. BATSTAT remains at 1, indicating that battery B is present and supplying the load.

At t6, battery B falls below $5 \times V_{MIN}$, and the MAX1773 automatically disconnects battery B's discharge path and connects battery A's discharge path. BATSTAT changes to BATSEL (0) to indicate that battery B is no longer supplying the load. At this point, the external controller orders a controlled shutdown of the system and drastically reduces the supply current.

At t7, the AC adapter supply is reconnected to the system. The MAX1773 automatically disconnects battery A's discharge path, connects the AC adapter's load path (PDS switch), and connects battery B's charge path. BATSTAT goes to BATSEL (1) to indicate that battery B is present. ACPRES goes to 0 to indicate that the AC adapter source is present.

At ta, the external controller recognizes that battery B is charged and changes BATSEL to battery A. BATSTAT goes to BATSEL (0) to indicate that battery A is present.

After t9, the batteries are fully charged and the system is ready for another cycle.

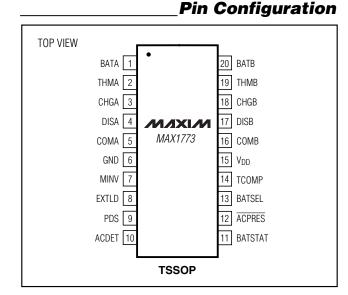
Power MOSFET Selection

The MAX1773 does not place stringent requirements on the external PMOS FETs. Use PMOS FETs with low VGS thresholds (logic level FETs). Low $R_{DS(ON)}$ PMOS FETs are desirable since the PMOS FET's resistance directly contributes to power losses. Also, ensure that

the PMOS FET's V_{DS} and V_{GS} ratings exceed the specific circuit requirements. See Table 5 for a list of recommended manufacturers.

Layout Guidelines

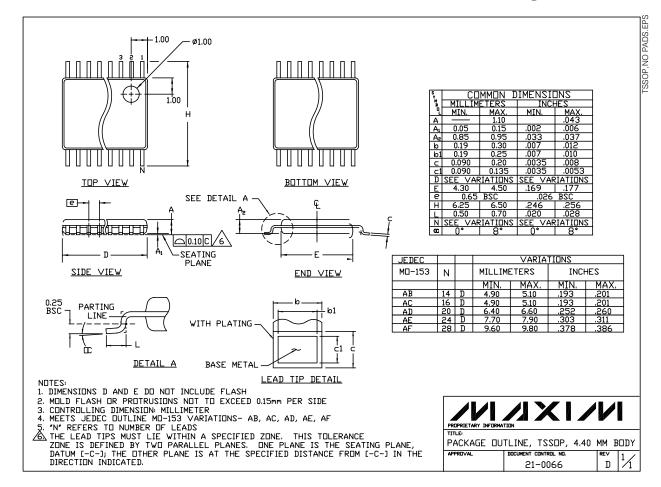
The MAX1773 does not use fast switching times or high frequencies. Therefore, the layout requirements are minimal. Keep the gate connections to the external PMOS FETs short to minimize capacitive coupling, reduce parasitic inductance, and ensure stability. In addition, minimize the power path length when possible to reduce the path's resistance. See the MAX1773 evaluation kit for a layout example.



Chip Information

TRANSISTOR COUNT: 5245 PROCESS: BICMOS

Package Information



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