

Design Idea DI-25

DPA-Switch[®] 30 W DC-DC Converter with Synchronous Rectification



| Application | Device | Power Output | Input Voltage | Output Voltage | Topology |
|-----------------|---------|--------------|---------------|----------------|----------|
| DC-DC Converter | DPA425R | 30 W | 36-75 VDC | 5 V | Forward |

Design Highlights

- Extremely low component count
- High Efficiency - 90% using synchronous rectification
- Accurate UV/OV allows self-driven synchronous rectification
- No current sense resistor or current transformer required
- Output overload, open loop and thermal protection
- 300 kHz switching frequency - optimizes efficiency when simple self-driven synchronous rectification is used

Operation

DPA-Switch greatly simplifies the design compared to a discrete implementation. Resistor R1 programs the input under/over voltages to 33 V and 86 V, respectively, and linearly reduces the maximum duty cycle with input voltage to prevent core saturation during load transients. Tight tolerances of the UV/OV thresholds determine the secondary MOSFETs gate voltage range, allowing low cost, self-driven synchronous rectification. Resistor R3 programs the internal current limit of the DPA425R to 45% of nominal. The larger *DPA-Switch* selection reduces conduction losses, raising efficiency without design or overload penalty.

Capacitor C9, R5 and the gate capacitance of Q1 reset T1 during the *DPA-Switch* off time. Zener VR1 provides a hard voltage clamp to limit DRAIN voltage under output transient and overload conditions. The bias supply for U1 is generated from an auxiliary winding on L2, providing higher efficiency than a winding on T1.

MOSFETs Q1 and Q2 are connected as self-driven synchronous rectifiers. Resistor R15 filters voltage spikes at the gate of Q2, and D3 prevents the body diode of Q1 from conducting. The UV/OV thresholds ensure both minimum and maximum gate voltage specifications are met.

Key Design Points

- For nominal undervoltage set point V_{UV} :
 $R1 = (V_{UV} - 2.35 \text{ V}) / 50 \mu\text{A}$. $V_{OV} = (R1 \times 135 \mu\text{A}) + 2.5 \text{ V}$.
- Select C9 such that the core resets at V_{UV} and the DRAIN voltage $\leq 170 \text{ V}$ at V_{OV} . Note the gate capacitance of Q1 will affect the value of C9.
- Zener VR1 safely limits the DRAIN voltage below BV_{DSS} and guarantees transformer reset.

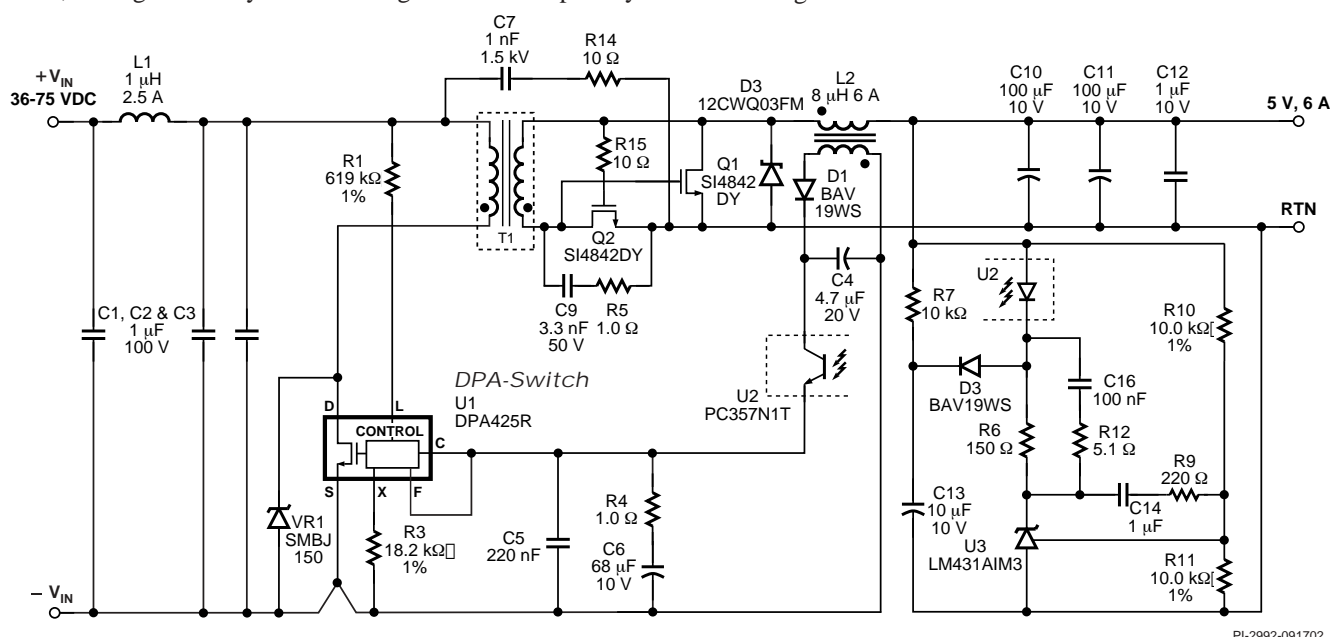


Figure 1. *DPA-Switch* 30 W, 15 V, 6 A DC-DC Converter.

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- Opto U2 should have a CTR range of 100% to 200% for optimum loop stability.
- At zero load, maximum input voltage, the bias voltage across C4 should be ≥ 8 V (12 V to 15 V under nominal conditions).
- Good layout practices should be followed:
 - Locate C5, C6 and R4 close to U1 with grounds returned to the SOURCE pin.
 - Primary return should be connected to the *DPA-Switch* tab, not the SOURCE pin.
 - Minimize the primary and secondary loop areas to reduce parasitic leakage inductance.
- Consult AN-31 for additional design tips and information.

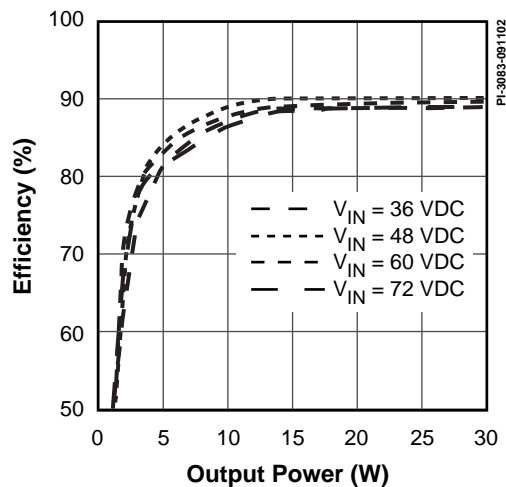


Figure 2. *DPA-Switch 30 W, 5 V Synchronous Rectifier Efficiency vs. Output Power.*

OUTPUT INDUCTOR PARAMETERS

| | |
|-----------------------------|--|
| Core | RM6ILP Ferroxcube 3F3 material Gap for A_{Lg} of 278 nH/T ² |
| Winding Details | Main: 6T, 4x26 AWG Bias: 15T, 32 AWG |
| Bobbin | RM6ILP 8 pin (EPCOS B-65821-A6008-T1 or equivalent) |
| Winding Order (pin numbers) | Bias (1-2), tape, Main Winding (7,8-5,6), tape |
| Inductance | 8 μ H $\pm 10\%$ |

Table 2. *Output Inductor Construction Information.*

TRANSFORMER PARAMETERS

| | |
|-----------------------------|--|
| Core | EFD20 Ungapped Ferroxcube EFD20-3F3 |
| Bobbin | EFD20 10 pin (B&B B-052 or equivalent) |
| Winding Detail | Primary: 8T + 8T, 25 AWG Secondary: 4T, 0.002" Cu Foil |
| Winding Order (pin numbers) | Primary (5-3), tape, Secondary (6,7-9,10), tape, Primary (3-1), tape |
| Inductance | Primary: 307 μ H $\pm 25\%$, Leakage: 1 μ H (max.) |
| Primary Resonant Frequency | 3 MHz (minimum) |

Table 1. *Transformer Construction Information.*

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