# Transmit Gain Adjustments For The MC34014 Speech Network

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## INTRODUCTION

The MC34014 telephone speech network provides for direct connection to an electret microphone and to Tip and Ring. In between, the circuit provides gain, drive capability, and determination of the ac impedance for compatability with the telephone lines. Since different microphones have different sensitivity levels, different gain levels are required from the microphone to the Tip and Ring lines. This application note will discuss how to change the gain level to suit a particular microphone while not affecting the other circuit parameters.

#### CIRCUIT DESCRIPTION

Refer to Figure 1. The microphone is assumed to be an electret type, characterized by a high dynamic impedance. It is therefore considered to be an ac current source rather than a voltage source. If the microphone used has a dynamic impedance which is not high (compared to Rg), then the microphone must be modeled as a current source paralleled by its dynamic impedance. That impedance value must then be considered to be in parallel with Rg in the following equations. The  $T_X$  amplifier has a fixed gain of -20, and the EQ amplifier gain varies from 0.25 to 0.75, depending on the loop current.  $Z_L$  is the line impedance. The transmit gain is defined as  $V+I_{\mbox{mic}}$  and is equal to:

$$\frac{V+}{I_{mic}} = \frac{R_6 \times Z_L \times A_{TX}}{(1 + R_6/R_A)R_9 + (A_{TX}) (A_{EQ}) (Z_L)}$$

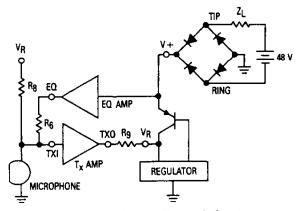


Figure 1. MC34014 Transmit Section

where  $A_{TX}$  = gain of the transmit amplifier (20 V/V)  $A_{EQ}$  = gain of the equalization amp. (0.25 to 0.75 V/V)  $R_A$  =  $R_B$ //10  $k\Omega$  (10  $k\Omega$  = input impedance of  $T_X$  amp.)

The ac impedance of the circuit is defined as:

$$Zac = \frac{Rg (1 + R6/RA)}{(ATX) (AEQ)}$$

The receive gain (see data sheet for the equivalent circuit) is defined as:

$$Grx = \frac{R_4}{R_1} + \frac{(X_C//R_2) (A_{EQ}) (A_{TXO}) (A_{STA}) \times R_4}{((X_C//R_2) + R_3) (1 + R_6/R_A) \times R_2}$$

As can be seen from the above equations, changing  $R_6$  while maintaining the  $R_6/R_A$  ratio constant will result in a transmit gain change (proportional to  $R_6$ ) but will not affect the other parameters. For example, increasing  $R_8$  and  $R_6$  by a factor of 3 will increase the transmit gain by  $\approx 10$  dB.

Using the above procedure to increase the transmit gain results in increasing Rg, which supplies the bias current to the microphone. If the higher value of Rg results in insufficient bias voltage at the microphone, then the alternate biasing scheme of Figure 2 should be used.

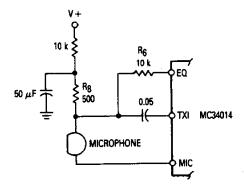


Figure 2. Alternate Biasing Scheme for Higher Voltage Microphones



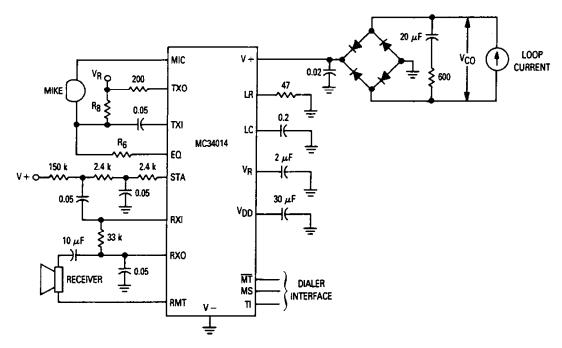
## **TEST RESULTS**

Tests were conducted with a Primo EM-95A microphone, having a sensitivity of  $-53 \text{ dB} \pm 3 \text{ dB}$  (0 dB = 1 V/μbar), and a Hosiden KUC2123 microphone which has a sensitivity of  $-60 \text{ dB} \pm 3 \text{ dB}$ . The test circuit is shown in Figure 3. The tests consisted of applying a constant sound level to the microphones, and measuring the output at VCO, while simulating line lengths of 0-21 Kfeet. The outputs of the two circuits were nearly identical at all line lengths.

### CONCLUSION

Although the designs of the various parameters (transmit gain, receive gain, ac impedance, etc.) of the MC34014 speech network are not mutually exclusive due to the commonality of various components, it is possible to adjust the transmit gain independently to suit a particular microphone.

For further information on the MC34014 speech network, refer to the data sheet.



For Primo EM-95A microphone Rg = 500  $\Omega$ , R<sub>6</sub> = 10 k For Hosiden KUC2123 microphone Rg = 1.5 k, R6 = 30 k

Figure 3. Microphone Gain Test Circuit

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