

## **APPLICATION INFORMATION**

# **Demoboard W-CDMA for the BGA2003**

**Application Note**

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**1 SUMMARY****• Description of products**

Monolithic Microwave Integrated Circuit (MMIC): RF transistor with internal bias circuit. The benefit is lower component count, low production spread and enabling function by  $I_{ctrl}$  with high isolation when shutoff.

**• Application Area**

Low noise amplifier for systems like GSM, DECT, DCS with low component count.

**• Presented Application**

The application presents a low noise amplifier for W-CDMA at 3400 MHz with matching components.

**• Main results**

An amplifier has been designed and tested for application in W-CDMA with minimum component count:

- Frequency is 3400 MHz;  $I_{supply} = 4.7$  mA;  
Gain = 9.4 dB; IIP3 = 2.1 dBm; Noise Figure (NF) = 2.7 dB;  
 $VSWR_{in} = 1.4$ ;  $VSWR_{out} = 1.6$
- Frequency is 3400 MHz;  $I_{supply} = 10$  mA;  
Gain = 10.3 dB; IIP3 = 9.2 dBm; Noise Figure = 3.1 dB;  
 $VSWR_{in} = 1.2$ ;  $VSWR_{out} = 1.6$ .

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**2 THE INTERNAL BGA2003 CIRCUIT**

For understanding of the behaviour of the BGA2003 MMIC circuit the internal circuit diagram is given in Fig.1.

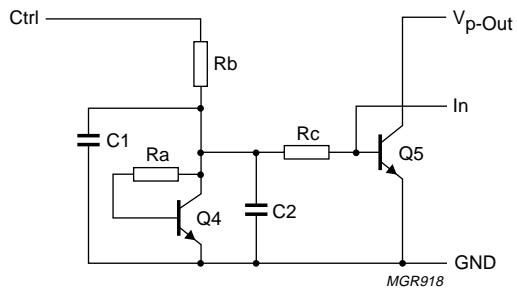


Fig.1 Internal circuit diagram.

Q5 is the main RF transistor. Q4 forms a current mirror with Q5. The input current of this current mirror is determined by the current into pin Ctrl. Rb limits the current when a control voltage is applied directly to the Ctrl input. Rc, C1, and C2 decouple the bias circuit from the RF input signal.

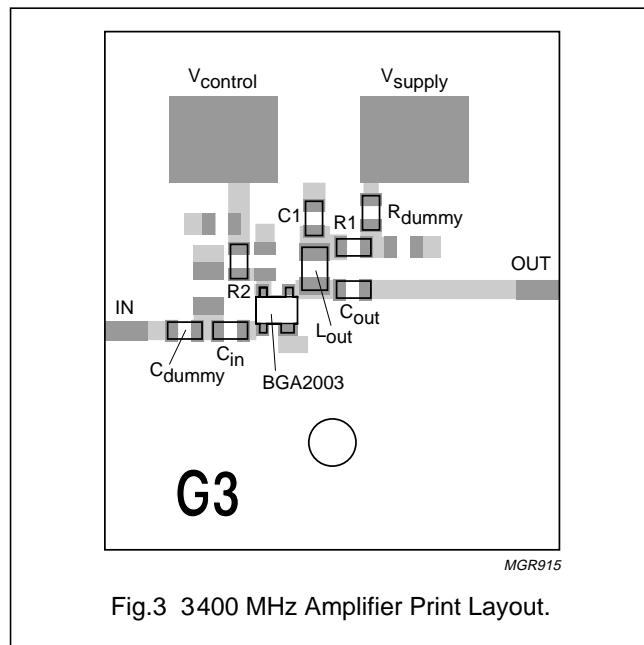
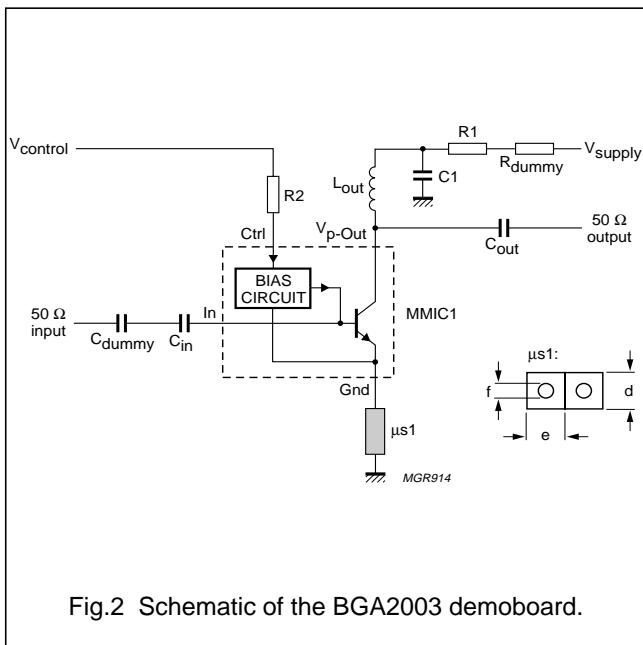
**3 SIMULATION OF THE BGA2003 DEMOBOARD**

S-parameters of the BGA2003 MMIC were measured at  $V_{p\text{-Out}} = 2.5$  V,  $I_{\text{supply}} = 4$  mA up to 3 GHz. HP-MDS simulation was used to extrapolate to 3.4 GHz and optimize component values for gain, noise and matching. These component values have been used as a starting point for finding the used practical component values (see Table 1).

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## 4 APPLICATION CIRCUIT

**Table 1** Used components for the BGA2003 demoboard

COMPONENT	VALUE	UNIT	SIZE - MANUFACTURER	PURPOSE; COMMENT
C <sub>dummy</sub>	150	pF	0603 Philips	connecting dummy (NP0); see Chapter 5
C <sub>in</sub>	47	pF	0603 Philips	DC-decoupling; input match
C <sub>out</sub>	0.82	pF	0603 Philips	output match
L <sub>out</sub>	2.2	nH	0603 AVX type 1200	output match
C1	2.2	pF	0603 Philips	RF-short to ground
R <sub>dummy</sub>	0	Ω	0603 Philips	connecting dummy, short; see Chapter 5
R1	120	Ω	0603 Philips	DC-bias; RF decoupling
R2	4.7	kΩ	0603 Philips	DC-bias; bias setting
μs1	—	—	PCB via	d = e = 1 mm; f = 0.4 mm
MMIC1	BGA2003	—	Philips SOT343R1	
PCB	—	—	FR4	$\epsilon_R \sim 4.6$ ; H = 0.5 mm

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**Table 2** Measured values

$V_{\text{supply}} = 3.0 \text{ V}$ ;  $V_{\text{control}} = 3.0 \text{ V}$ ;  $I_{\text{supply}} = 4.66 \text{ mA}$ ;  $f = 3400 \text{ MHz}$ ; see note 1.

S-PARAMETERS	CONDITION	TYP.	UNIT	VSWR
$S_{11}$		-16.4	dB	1.4
$S_{21}$		+9.4	dB	—
$S_{12}$		-15.2	dB	—
$S_{22}$		-13.1	dB	1.6
NF		+2.65	dB	—
Input IP3	at -30 dBm in; note 2	+2.1	dBm	—

**Notes**

1. S-parameters measured at -30 dBm input level.
2. IP3 -30 dBm in, f1 and f2 100 kHz separated.

**Table 3** Measured values

$V_{\text{supply}} = 3.7 \text{ V}$ ;  $V_{\text{control}} = 6.0 \text{ V}$ ;  $I_{\text{supply}} = 10 \text{ mA}$ ;  $f = 3400 \text{ MHz}$ ; note 1.

S-PARAMETERS	TYP.	UNIT	VSWR
<b>Spars with <math>I_{\text{ctrl}} = 0</math></b>			
$S_{11}$	-3.85	dB	4.6
$S_{21}$	-19.1	dB	—
$S_{12}$	-19.3	dB	—
$S_{22}$	-5.27	dB	3.4

**Note**

1. Switch off isolation.

**5 COMMENTS ON THE PRINTED CIRCUIT BOARD**

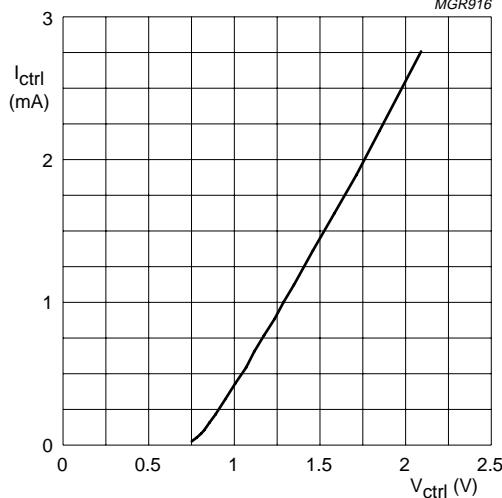
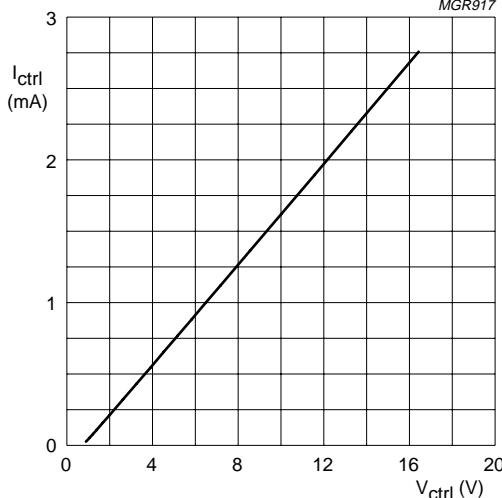
This Printed Circuit Board (PCB) is developed for a LNA with the BGA2003, with component positions for extra decoupling and matching. Although this application was designed for minimal component count, two extra components  $R_{\text{dummy}}$  and  $C_{\text{dummy}}$  were needed as interconnect on this PCB. With a new PCB these components can be left out.  $C_{\text{in}}$  is for DC-decoupling the input to the circuit and matching to  $50 \Omega$ .  $L_{\text{out}}$  and  $C_{\text{out}}$  match the circuit to the  $50 \Omega$  output. Decoupling the supply for high frequencies is done by R1 and C1. The value of R1 determines the voltage on  $V_{\text{p-out}}$ , which was designed to be 2.5 V with a supply current of 4 mA. The value of R2 and the value of  $V_{\text{control}}$  determine the control current and thereby the collector current. With  $4.7 \text{ k}\Omega$  for R2 and  $V_{\text{ctrl}} 3.0 \text{ V}$  a supply current of 4.66 mA was set (see Figs 4 and 5).

$$I_{\text{supply}} \text{ can also be estimated by calculation with formula: } I_{\text{supply}} = \frac{10 \times (V_{\text{control}} - 0.83)}{(R2 + 152)}$$

Coil  $L_{\text{out}}$  can be replaced by a stripline made on the PCB itself.  $C_{\text{in}}$  can be omitted in some applications when the input signal is not DC coupled.

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Fig.4 I<sub>ctrl</sub> as function of V<sub>control</sub>.Fig.5 I<sub>ctrl</sub> as function of control V<sub>control</sub> with R2 = 5.1 kΩ.

For higher IIP3 a supply current of 10 mA was set by applying larger V<sub>ctrl</sub> (6 V). V<sub>supply</sub> was raised to 3.7 V to compensate for the extra voltage drop across R1 to keep voltage on pin V<sub>p-Out</sub> to 2.5 V. To get the same supply current of 10 mA at 3 V supply, and keep voltage on pin V<sub>p-Out</sub> to 2.5 V, R1 should be changed from 120 Ω into 47 Ω.

**Table 4** Measured values on the BGA2003 demoboard

V<sub>supply</sub> = 3.7 V; V<sub>control</sub> = 6.06 V; I<sub>supply</sub> = 10.0 mA; 3400 MHz; see note 1

S-PARAMETERS	CONDITION	TYP.	UNIT	VSWR
S <sub>11</sub>		-20.4	dB	1.2
S <sub>21</sub>		+10.3	dB	-
S <sub>12</sub>		-14.8	dB	-
S <sub>22</sub>		-12.9	dB	1.6
NF		+3.10	dB	-
Input IP3	at -20 dBm in; note 2	+9.2	dBm	-

**Notes**

1. S-parameters measured at -30 dBm input level.
2. IP3: 2x -20 dBm in; f1 and f2 100 kHz separated.

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Printed in The Netherlands

125006/3100/01/pp8

Date of release: 1999 Feb 16

Document order number: 9397 nnn nnnnn

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