# SEMICONDUCTOR DIODES AND TRANSISTORS

## PROGRAMED INSTRUCTION



MANUFACTURERS OF CATHODE-RAY OSCILLOSCOPES

VOLUME 5 CIRCUITS 2

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## SEMICONDUCTOR DIODES AND TRANSISTORS

VOLUME 5

## CIRCUITS 2

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## STOP. PLEASE READ.

In Volume 5 we will discuss high frequency and temperature considerations in linear transistor circuits. We also include a review of the characteristics of transistor switching circuits.

The prerequisites for taking this volume are Volumes 1-4 of Semiconductor Diodes and Transistors, or the equivalent.

The objectives for each set on the following page can also be used as a table of contents. That is, objective 1 will indicate the material in set 1, etc.

#### OBJECTIVES

- 1. Recall the component parts of a high frequency equivalent circuit.
- 2. Recall the two primary limitations of high frequency performance of a transistor common emitter circuit.
- 3. Recall the methods of minimizing the high frequency limitations on a common emitter circuit.
- 4. Recall the high frequency limitations on a common emitter circuit and methods of minimizing these limitations.
- 5. Recall the high frequency advantage of a cascoded amplifier stage and be able to determine the approximate gain.
- 6. Recall the high frequency limitations on a common collector circuit and methods of minimizing these limitations.
- 7. Recall the characteristics of current mode and saturated mode switching.
- 8. Recall the effects of temperature change in the base emitter junction of a transistor.
- 9. Recall the method of stabilizing a transistor circuit against changes in ambient temperature.
- 10. Recall the output distortion from a push-pull circuit due to changes in power dissipated by the transistors.
- 11. Recall the point at which a transistor operates to be thermally balanced.
- 12. Recall the method of adding components to a push-pull circuit to obtain thermal balance.





#### Answer to Frame 1.0



We have adapted the transistor equivalent circuit used in Volume 4 to a high frequency equivalent circuit. (Both are common emitter circuits.)



Low Frequency Equivalent

The transistor high frequency equivalent circuit has three changes from the low frequency equivalent circuit.

High Frequency Equivalent

#### The changes are:

- 1. Add C<sub>F</sub>; C<sub>F</sub> represents the capacitance across the emitter base junction.
- 2. Add C<sub>C</sub> and omit  $r_c$ ; C<sub>C</sub> represents the capacitance across the collector base junction. The reverse biased collector base resistance ( $r_c$ ) has been omitted because  $X_{c_c}$  at high frequencies is much less than  $r_c$ .
- 3.  $\alpha_{i_{r_{e}}}$ , the current generator amplitude has been changed from  $\beta_{i_{b}}$ . In the low frequency equivalent circuit we assumed that all the emitter current was flowing through  $r_{e}$ . Under these circumstances we could consider the amplitude of the collector current generator to be  $\beta_{i_{b}}$  or  $\alpha_{i_{e}}$  ( $\beta_{i_{b}}$  and  $\alpha_{i_{e}}$  are equal). However, no part of the emitter current flowing through  $C_{E}$ , the emitter capacitance, is conducted through the collector current generator. Current through  $C_{E}$  constitutes moving charges in and out of the base. No electrons actually cross the emitter base junction. Therefore we must stipulate that only  $\alpha$  times the emitter current through  $r_{e}$  will be conducted in the collector current generator. As the signal frequency is increased, a larger percentage of  $i_{e}$  will flow through  $C_{E}$ . Therefore as signal frequency is increased, for a constant emitter amplitude, the collector current amplitude will decrease.



capacitance

1.2 There is capacitance across the \_\_\_\_\_ base junction and the \_\_\_\_\_ base junction.

emitter collector

1.3 Because it is forward biased, the depletion region is narrower and the capacitance is larger across the \_\_\_\_\_ base junction.

emitter

At higher frequencies the capacitive reactance of  $\mathsf{C}_{\mathsf{C}}$  becomes low enough that we may ignore the resistance of \_\_\_\_\_

r<sub>c</sub> (collector resistance)

The portion of the base current that flows through the emitter capacitance  $\mathsf{C}_{\mathsf{E}}$  , 1.5 \_ multiplied by the current generator . is/is not

is not

1.6

The current generator, then, will multiply only the portion of the base current that flows through \_\_\_\_\_

r<sub>e</sub> (emitter resistance)

1.4

The amplitude of the current generator output is then  $\alpha$  times only the portion of emitter current through \_\_\_\_\_\_.

 $r_e$  (emitter resistance)

1.8 Label all the parts of the high frequency equivalent circuit below.





#### 1.7

- 0 The two primary limitations that determine the high frequency response of a transistor in a common emitter configuration are:
  - The high frequency at which the collector signal current is .707 of the collector low frequency signal current. This frequency is the frequency at which X<sub>C<sub>F</sub></sub> is equal to \_\_\_\_\_\_.



βr<sub>e</sub> C<sub>C</sub> R<sub>g</sub> r<sub>b</sub> R<sub>L</sub>

The two primary limitations that determine the high frequency response of a transistor in the common emitter configuration are:

1. The frequency at which the capacitive reactance of  $C_E(X_{C_E})$  is equal to  $\beta$  times  $r_e$ . The key to understanding this is to remember we are driving the base of the transistor. From the base  $r_e$  looks  $\beta$  times as large as it is because only  $1/\beta$  of the current through  $r_e$  flows to the base. However, all the current through  $C_E$  flows to the base so it will be seen from the base as its actual value.



At the frequency where  $X_{C_E}$  equals  $\beta r_e$  only .707 of the total emitter current will be flowing through  $r_e$  to the collector. The voltage gain of the stage will be 30% down due to this consideration alone.

2. The other limitation in the common emitter configuration is the time constant of  $C_{\rm C}$  times the voltage gain of the stage (A<sub>V</sub> + 1) (Miller effect) and the series resistance of R<sub>g</sub>, r<sub>b</sub>', and R<sub>L</sub>.



At the frequency where  $X_{C_E}$  is equal to  $\beta r_e$ , .707 of the base current will flow through

 $\rm r_e$  or  $\rm C_E$ 

2.2

At this frequency the collector signal current will be only .707 of the \_\_\_\_\_\_ frequency collector signal current.

low

2.3 If the collector signal current is down to .707 of the low frequency signal current the voltage gain of the stage must be down to \_\_\_\_\_\_ of the low frequency voltage gain.  $(A_V + 1)$ 

2.5	This capacitance	$\left[ (A_V + 1) C_C \right]$	will have to charge through the three resiste	ors
		/	, and	



2.6

The fastest change available at the collector of the transistor is, then, limited by R<sub>g</sub>, r<sub>b</sub>', R<sub>L</sub> and collector \_\_\_\_\_.

capacitance

The high frequency performance of a transistor in the common emitter configuration is then limited by:

The frequency at which the reactance of the emitter junction \_\_\_\_\_\_\_.
is equal to the emitter \_\_\_\_\_\_\_ x \_\_\_\_\_\_.

2. The time constant including the \_\_\_\_\_ capacitance and the resistances \_\_\_\_\_ and \_\_\_\_.



C<sub>E</sub> resistance or r<sub>e</sub> β Collector or Miller R<sub>g</sub> r<sub>b</sub>' R<sub>L</sub> To increase the frequency at which  $X_{C_E}$  is equal to  $m{ heta}_{r_e}$  we can increase emitter

To reduce the time constant of (A<sub>V</sub> + 1) C<sub>C</sub> × (R<sub>g</sub> + r<sub>b</sub>' + R<sub>L</sub>) we can:

- Increase \_\_\_\_\_\_\_\_to base voltage to reduce the value of C<sub>C</sub>.
- Decrease the value of \_\_\_\_\_\_ which will also reduce voltage gain.
- Select a transistor that will operate at the desired frequency with a low value of \_\_\_\_\_.

4. Drive the transistor from a \_\_\_\_\_ resistance source.



Answer to Frame 3.0:

current collector <sup>R</sup>L r<sub>b</sub> low

In attaining high frequency performance from a transistor in the common emitter configuration there are a number of tradeoffs that must be made.

The first is in the selection of the transistor. One of the methods of attaining high frequency operation from a transistor is to make the base thinner. When the base is made thinner  $r_b'$  will increase. The first tradeoff, then, is in the selection of a transistor. It must operate at the desired frequency yet  $r_b'$  must be kept small to decrease the time constant involving  $C_C$ ,  $r_b'$ ,  $R_a$  and  $R_L$ .

The next tradeoff is in the selection of  $R_L$ . As we decrease  $R_L$  to decrease the time constant of  $C_C$ ,  $r_b'$ ,  $R_a$  and  $R_L$ , we decrease the voltage gain of the stage.

Another tradeoff is the operating transistor  $V_{cb}$ . The larger  $V_{cb}$  the smaller the collector capacitance  $C_{c}$ , but the more power dissipated by the collector.

The value of  $R_g$  should also be kept to a minimum. This may be at the expense of voltage gain in the previous stage or require an additional emitter follower stage.

These are four tradeoffs we can make to increase high frequency performance by reducing the time constant of  $C_C$ ,  $r_b$ ',  $R_a$  and  $R_L$ .

The other high frequency limitation is the frequency at which  $X_{C_E} = \beta r_e$ . By increasing emitter current we reduce  $r_e (r_e \approx \frac{26}{I_E (mA)})$ . A higher frequency will be required to bring  $X_{C_E}$  down to the lower value. By increasing emitter current we also increase the power dissipated by the transistor, another tradeoff.

3.1 In selecting a transistor for a high frequency circuit it is desirable to have the base resistance r<sub>b</sub>' as \_\_\_\_\_ as possible.

small

 $^{\sf R}$ L

> collector capacitance (C<sub>C</sub>) power

3.3 We sacrifice voltage gain to improve the high frequency performance of a common emitter transistor circuit by reducing \_\_\_\_\_.

3.4 For high frequency performance it is desirable to drive a transistor in the common emitter configuration from a \_\_\_\_\_\_ resistance source.

low

re

3.6

3.5 We can improve high frequency performance by increasing I<sub>E</sub>, which will reduce

For high frequency performance, we operate a transistor with a  $_{large/small}$  V<sub>cb</sub> and a  $_{large/small}$  I<sub>E</sub> which will increase the \_\_\_\_\_\_ dissipated by the transistor.

To further enhance the performance of a transistor in the common emitter configuration, we select a transistor with a \_\_\_\_\_\_ value  $r_b'$ , reduce the value of  $R_L$  at the expense of \_\_\_\_\_\_ gain and drive the transistor from a \_\_\_\_\_\_ resistance source.

large large power low voltage low The two primary limitations on the high frequency performance of a transistor in the common base configuration are:

> The frequency at which X<sub>C<sub>F</sub></sub> is equal to \_\_\_\_\_. 1.

The time constant of \_\_\_\_\_ and \_ 2.

To increase the high frequency performance of a transistor in the common base configuration we operate the transistor with a  $\_$  Iarge/small  $V_{cb}$  and a Iarge/small IE. We select a transistor with a satisfactory ft and a Iarge/small

 $r_{\rm b}$  '. We also select a \_\_\_\_\_ value  $R_{\rm L}$  which will sacrifice some

\_\_\_\_\_gain.



Answer to Gating Frame 4.0

re RL Cc rb large large small low voltage

The two primary high frequency limitations of a transistor in the common base configuration are essentially the same as in the common emitter configuration. There is the frequency at which the signal current through  $r_e$  is only 70% of the emitter signal current. However, in the common base configuration we are diriving the emitter therefore  $r_e$  is not multiplied by  $\beta$ . The frequency at which  $I_{r_e}$  is 70% of  $I_e$  is the frequency at which  $X_{c_e}$  is equal to  $r_e$ . The other limitation is the

time constant involving  $C_c$  and  $r_b'$  in the transistor and the collector load  $R_L$ .



The common base configuration is able to operate at a higher frequency than the common emitter configuration for two reasons:

- 1. The generator resistance has been removed from the time constant of C\_C,  $r_{\rm b}',$  and  $R_{\rm L}$  .
- 2.  $r_e$  is not amplified  $\beta$  times therefore the frequency must be much higher before  $X_{c_e}$  is equal to  $r_e$ .

The means of improving high frequency performance of a transistor in the common base configuration are similar to those used in the common emitter configuration. A transistor is selected with an acceptable  $f_t$  and a low  $r_b$ '. The transistor is operated at a high  $V_{cb}$  to reduce  $C_C$  and a high  $I_E$  to reduce  $r_s$ .

The collector load is again kept small to improve high frequency, but again at the expense of voltage gain.

4.1	One high frequency limitation on a transistor in the common base configuration is the frequency at which X <sub>CE</sub> is equal to				
	r <sub>e</sub>				
4.2	Another high frequency limitation on a transistor in the common base configuration is the time constant involving,, and				
	C <sub>C</sub> r <sub>b</sub>				
	R <sub>L</sub>				
4.3	A transistor that is selected for a high frequency common base circuit should have an acceptable f <sub>t</sub> and a small				
	rb				

4.4 Assuming all other factors equal, a transistor in the common base configuration with 10 mA of quiescent current would have a \_\_\_\_\_\_ frequency response lower/higher than one conducting 1 mA of quiescent current.

#### higher

4.5 Assuming all other factors equal, a common base transistor with 2 volts quiescent V<sub>CB</sub> would have a \_\_\_\_\_\_ frequency response than one with 5 volts quiescent V<sub>CB</sub>.

#### lower

4.6 Assuming all other factors equal, a common base transistor with an  $R_L$  of 1 k $\Omega$  would have a \_\_\_\_\_\_\_ frequency response than one with an  $R_L$  of 100 $\Omega$ .

lower

In a transistor in the common base configuration, the collector signal current will be 70% of its low frequency value when the signal frequency is high enough so that  $X_{c_e}$  is equal to \_\_\_\_\_\_. Another limitation on the common base configuration is the time constant involving \_\_\_\_\_, and

A transistor with an acceptable  $f_t$  with a low value \_\_\_\_\_\_ should be selected for a high frequency common base circuit. To improve the high frequency response the common base transistor should be operated with a \_\_\_\_\_\_  $V_{CB}$  and a \_\_\_\_\_\_\_  $I_E$ . The collector load resistor ( $R_L$ ) should be kept \_\_\_\_\_\_ small/large.

r<sub>e</sub> C r<sub>b</sub> R L r<sub>b</sub> high high small

### 0 Determine the approximate A<sub>v</sub> in the circuit below.



The advantage of a cascoded amplifier stage from a high frequency standpoint is that \_\_\_\_\_\_ is almost eliminated in the common emitter section.

Answer to Frame 5.0:

 $A_{v} \approx 4$ Miller capacitance

The approximate voltage gain of a cascoded amplifier stage is determined in the same way as the voltage gain in a push-pull circuit. If we assume a high  $\beta$  in all four transistors, we can assume approximately the same current in the collectors of the common base transistor as in the emitters of the common emitter transistors. With this assumption voltage gain is the ratio of emitter resistance ( $r_{e_1} + R_E + r_{e_2}$ ) to collector resistance ( $R_{L_1} + R_{L_2}$ ). The voltage gain in the circuit on the facing page is:

$$A_{v} \approx \frac{R_{L_{1}} + R_{L_{2}}}{r_{e_{1}} + R_{E} + r_{e_{2}}} = \frac{200\Omega + 200\Omega}{2.6\Omega + 95\Omega + 2.6\Omega} \approx 4$$

The advantage of this circuit from a high frequency standpoint is that the Miller capacitance is essentially removed from the common emitter section. The collectors of the common emitter section are driving the emitters of the common base section. They will, therefore, only move a few millivolts.



5.1 When an input signal is applied to the circuit on the facing page, the collectors of  $Q_1$  and  $Q_2$  will have a signal amplitude of a few  $\mu V/mV/volts$ .

millivolts

5.2 By keeping the collectors of Q<sub>1</sub> and Q<sub>2</sub> nearly constant we have nearly eliminated the \_\_\_\_\_\_ capacitance effect.

Miller

5.3 The value of  $r_e$  in  $Q_1$  and  $Q_2$  is \_\_\_\_\_  $\Omega$  each.

$$r_{e} = \frac{26}{I_{E} (mA)} = \frac{26}{10} = 2.6\Omega$$

5.4 The total emitter resistance in the emitter circuit of  $Q_1$  and  $Q_2$  is \_\_\_\_\_\_\_.

 $2.6\Omega + 70\Omega + 2.6\Omega = 75.2\Omega^{-1}$ 



300Ω

5.6 The approximate voltage gain of the circuit on the facing page is \_\_\_\_\_

 $A_v \approx \frac{300\Omega}{75\Omega} = 4$


The high frequency advantage of a cascoded stage is that

is effectively removed from the common emitter section. The voltage gain of the cascoded amplifier on the facing page is \_\_\_\_\_.

Miller capacitance 6 6.0

The two primary limitations on a common collector transistor circuit are:

The frequency at which X<sub>CE</sub> is equal to \_\_\_\_\_\_.

The frequency at which X<sub>C</sub> is equal to \_\_\_\_\_ and \_\_\_\_\_.

To minimize these limitations a transistor with an	acceptable f <sub>+</sub> and a low
is selected. The transistor is operated at a low/h	V <sub>CB</sub> and a Lev / Lev
The impedance of the signal source is kept at a _	
n	ninimum/maximum



βr<sub>e</sub> r<sub>b</sub>' Rg r<sub>b</sub>' high high minimum

The high frequency limitations of the common collector configurations are attributed to primarily the same factors that limited the common emitter and common base configurations.

1. The frequency at which  $X_{C_E}$  is equal to  ${}^{\beta}r_e$  the emitter signal current will be down to 70% of the low frequency signal current. As in the common emitter configuration  $r_e$  looks  $\beta$  times its value when driven from the base.

2. At the frequency where  $X_{C_c}$  is equal to  $r_b' + R_g$ , the signal amplitude at  $r_e$  is attenuated to 70% its actual value by the voltage divider action of  $r_b' + R_g$  to  $C_c$ .

To reduce the effects of these limitations, the same techniques as were used in the common emitter and common base circuits are used. A transistor is selected for an acceptable  $f_t$  and a low  $r_b'$ . The transistor is operated at a high  $V_{CB}$  to reduce the value of  $C_c$  and at a high  $I_E$  to reduce the value of  $r_e$ . The signal source impedance ( $R_a$ ) is kept to a low value. 6.1 At the frequency where  $X_{C_E}$  is equal to  $\beta r_e$  in a common collector circuit, the emitter signal current will be \_\_\_\_\_% of its low frequency signal current.

70%

6.2 As the input frequency to a transistor in the common collector configuration is increased, the signal to r<sub>e</sub> will be attenuated by the voltage divider action of \_\_\_\_\_\_\_ + \_\_\_\_\_\_ and \_\_\_\_\_\_.



rb'

6.3 A transistor to be used in a high frequency common collector circuit is selected for an acceptable f<sub>t</sub> and a low value \_\_\_\_\_.

6.4 All other factors being equal, a transistor in the common collector configuration that is conducting 1 mA quiescently will have a \_\_\_\_\_\_ frequency response than one conducting 20 mA.

lower

6.5

All other factors being equal, circuit \_\_\_\_\_ below will have the higher frequency response.





В

higher

6.7

Two high frequency limitations on a common collector circuit are:

- 1. The frequency at which  $X_{C_E}$  is \_\_\_\_\_\_ times as large as  $r_e$ .
- 2. The frequency at which  $R_g + r_b'$  is equal to \_\_\_\_\_.

We would choose transistor \_\_\_\_\_\_ for use in a 50 MHz common collector circuit.

Transistor A -  $f_t = 200 \text{ MHz}$   $r_b' = 50\Omega$ Transistor B -  $f_t = 250 \text{ MHz}$   $r_b' = 100\Omega$ 

Select the circuit in each pair that would have the best high frequency response. Circuit \_\_\_\_\_\_ will have the best high frequency response.













7.0 Circuit A is an example of \_\_\_\_\_ mode switching. Circuit B is an example of \_\_\_\_\_ mode switching.

With the same square wave in, the transistor in circuit \_\_\_\_\_\_ will dissipate the most power. The circuit that will respond to the highest repetition rate input is circuit \_\_\_\_\_\_. When in the "on" mode, the collector voltage of circuit \_\_\_\_\_\_ will be closest to ground potential. The collector voltage at this time is labeled \_\_\_\_\_.





В

## Answer to Frame 7.0:

saturated current B B A V CE (sat)

<u>Circuit A</u> is an example of <u>saturated</u> mode switching. The transistor is allowed to go into saturation. A transistor is in saturation when the collector base junction is forward biased. This circuit is used in programing where the transistor, in its on state, must simulate a closed switch. For this reason the saturated voltage  $V_{CE}$  (sat) is an important transistor switching characteristic. The transistor in circuit A will dissipate very little power because it will operate in either cutoff or saturation. By allowing the transistor to saturate, storage time becomes significant, especially at high repetition rates. Storage time is a limiting factor on how high a repetition rate this circuit can operate.

<u>Circuit B</u> is an example of <u>current</u> mode switching. When the transistor is off, the diode will clamp the transistor emitter to  $\approx$ -.7V. When the transistor is turned on, the current is switched from the diode to the transistor. The size of the emitter resistor and collector resistor are selected so the transistor is not allowed to go into saturation. This effectively removes storage time from the switching time so this circuit is able to operate at a higher repetition rate than the saturated mode circuit (A).

The transistor in circuit B will dissipate more power than in circuit A because the transistor does not simulate a closed switch in the "on" cycle so this circuit isn't usually used in programming. It is used primarily where a high repetition rate is desired.

7.1	More power is dissipated by a transistor in a	mode	switching
	circuit.		

current

7.2 The highest repetition rate is available in a \_\_\_\_\_ mode switching circuit because \_\_\_\_\_\_ time is effectively removed from the switching time.

current storage

7.3 In a circuit that demands performance that very closely approximates a switch, \_\_\_\_\_\_mode switching would be used.

saturated

How closely a transistor approximates a closed switch is the transistor characteristic

 $V_{\mathsf{CE}}$  (sat)

A limiting factor of switching repetition rate in a saturated mode circuit is \_\_\_\_\_\_\_time.

storage

The transistor characteristic V<sub>CE</sub> (sat)<sup>is</sup> important when the transistor is to be used in a \_\_\_\_\_\_ mode switching circuit.

The transistor in a current mode switching circuit will dissipate \_\_\_\_\_\_power (less/more) than one in a saturated mode switching circuit. The switching rate in a saturated mode circuit is limited by \_\_\_\_\_\_ time. The current mode switching circuit has a \_\_\_\_\_\_ switching rate capability than the saturated mode switching circuit.

saturated more storage higher 8.0 As temperature in a transistor increases, the base to emitter voltage required for a given collector current \_\_\_\_\_\_ approximately \_\_\_\_\_mV/°C.





Answer to Frame 8.0:

decreases  $\approx 2$ 

The junctions in a transistor have a negative temperature coefficient. That is, for an increase in temperature the emitter base voltage required for a given collector current is reduced. For every °C increase in junction temperature, the emitter base voltage required for a given collector current is reduced  $\approx 2 \text{ mV}$ . This is an approximation that applies to both silicon and germanium transistors.

On the facing page is an example to illustrate this point. It takes .62V from base to emitter to maintain 5 mA collector current at a temperature of 20°C. However, at 30°C it only takes a  $V_{EB}$  of .6V to maintain an I<sub>c</sub> of 5 mA. If  $V_{EB}$  is not reduced to .6V, a reduction of 20 mV, then I<sub>c</sub> will increase sharply with the increase in temperature.

As temperature increases in a transistor the V<sub>EB</sub> required for a given collector

current \_\_\_\_\_\_.

decreases

8.2

A transistor, then, is said to have a \_\_\_\_\_\_ temperature coefficient.

## negative

8.3 In the circuit below the collector voltage will \_\_\_\_\_\_ as temperature decrease/increase as temperature 25V

decrease (T increases,  $V_{EB}$  constant,  $o_{o}^{o}$ ,  $I_{c}$  increases causing  $V_{c}$  to decrease)

8.1



increase .65V **(5°C** requires 10 mV change in V<sub>EB</sub>)

Note:

In Set 8 we have introduced a problem in transistor circuits caused by changes in transistor temperature. The change in transistor temperature may be caused by a change in ambient temperature or a change in power dissipated by the transistor. In the following sets we will discuss methods of minimizing these temperature problems.

8.4

Temperature stabilize the transistor in circuit A against changes in ambient temperature by properly adding a diode to the base circuit. Temperature stabilize the transistor in circuit B against changes in ambient temperature by properly adding a diode to the emitter circuit.



Circuit B

## Answer to Frame 9.0:



A forward biased semiconductor diode has approximately the same temperature coefficient as the emitter base junction in a transistor; i.e., for a 1°C increase in temperature, the junction voltage across the diode will decrease by  $\approx 2 \text{ mV}$ .

By connecting the diode in parallel with the emitter base junction, we can compensate for the  $\Delta V_{EB}$  due to temperature change.





In the circuit above we adjust the variable resistor for the desired collector output voltage. As temperature increases or decreases the  $V_{EB}$  required for a given  $I_c$  will decrease or increase.

The diode, having approximately the same temperature coefficient as the transistor, will provide the decreased or increased base voltage. The collector current will remain constant and, as a result, collector voltage will remain constant.

The resistance value of  $R_{\rm B}$  is not critical. Some circuits select  $R_{\rm B}$  to draw  $\approx 1$  mA of current; others select it to draw more.





In the circuit above the variable resistor is again adjusted for the desired collector output voltage. As temperature increases or decreases, the  $V_{EB}$  required for a given  $I_c$  will decrease or increase. The diode will act as a temperature variable resistor and provide the decreased or increased emitter voltage (see circuit below). The collector current will remain constant and as a result, collector voltage will remain constant. The emitter resistor,  $R_E$ , can be connected to an available negative supply, in our example -12V,  $R_e$  is then selected to provide the same amount of current to the diode as is being provided to the transistor. The diode is then operating at the same point on its response curve as the emitter base junction of the transistor. In this way, the diode voltage is able to follow the emitter-base junction voltage better.



The emitter base junction of a transistor and a semiconductor diode have 9.1 temperature coefficient. the same/a different

the same

To temperature stablize a transistor with a semiconductor diode, the diode should be 9.2 \_\_\_\_with the \_\_\_\_\_\_to base junction of the transistor.

> parallel emitter

Correct the circuit below for proper temperature stabilization, if there are any errors. 9.3



answer on next page

The anode and cathode leads of the diode should be reversed.

Correct the circuit below for proper temperature stabilization if there are any errors.



add a resistor of  $\approx\!\!10~k\Omega$  from the base to +10V

9.5 When the diode for temperature stabilization is in the emitter circuit, the diode should be conducting the same amount of current as the \_\_\_\_\_.

transistor

9.4



answer on next page

The value of R<sub>E</sub> is 2.5 kΩ ( $\frac{10V}{4 \text{ mA}}$  = 2.5 kΩ) (2.33k if .7V V<sub>EB</sub> is considered).

Temperature stabilize the circuit below using a diode first in the base circuit and then in the emitter circuit. Include the component sizes selected.





В

answer on next page

9.7

Answer to 9.7:



In the following set we will discuss the distortion on the output waveform of a push-pull circuit caused by a change in power dissipated by the transistors. The following sets will analyze the problem and finally arrive at a method for minimizing distortion due to thermal effects.

The output from the circuit below would present a CRT display like display A, B or C? \_\_\_\_\_.

> NOTE: To obtain the "display" the sweep speed would have to be a few milliseconds/div.



10.0





## Answer to Frame 10.0:

В

Distortion in transistor circuits can be caused by a change in power dissipated by the transistors. The first step in determining how the distortion will affect the output waveform is to determine the quiescent operating point for each transistor.



With the base of each transistor in the circuit above quiescently at 0V, there will be  $\approx 5 \text{ mA I}_{\text{E}}$ in each transistor. With a good  $\beta$ , each transistor I<sub>c</sub> will also be  $\approx 5 \text{ mA}$ . 5 mA through the 400 $\Omega$  collector load resistors will drop 2V. The V<sub>c</sub> of each transistor will therefore be 8V. The transistor will, then, be operating at 8V V<sub>c</sub> and 5 mA I<sub>c</sub> which is point X on the facing page curves.

$$P_{max} = 55 \text{ mW}$$



Constant Power Curve By applying a negative going signal to the base of  $Q_1$  the collector will go positive. From the curves on the facing page we can see that the operating point has moved away from the constant power curve or has decreased transistor power dissipation. If we look at the output from  $Q_1$ , it would look as below.

Original Step

As the transistor dissipates less power the temperature decreases and the  $V_{EB}$  required to maintain a constant  $I_c$  increases (Set 8). However, the  $V_{EB}$  in this case remains constant, therefore,  $I_c$ will decrease. As  $I_c$  decreases  $V_c$  will increase resulting in this waveform.

By applying a positive going signal to the base of  $Q_2$  the collector will go negative. From the curves on the facing page we can see that the operating point has approached the constant power curve or has increased transistor power. If we look at the output from  $Q_2$  it would look as below.

As the transistor dissipates more power the temperature increases and the  $V_{EB}$  required to maintain a constant  $I_c$  decreases. However, the  $V_{EB}$  in this case remains constant, therefore  $I_c$  will increase. As  $I_c$  increases  $V_c$  will decrease resulting in this waveform.

Original Step
If we use the output from this circuit to drive the vertical plates of a CRT, the display would look as below .



Resultant CRT Display



10.1 As power dissipation in a transistor increases the V<sub>EB</sub> required to maintain a constant I<sub>c</sub> will \_\_\_\_\_\_. decrease/increase

decrease

10.2 The operating point for the transistors in the circuit on the facing page is \_\_\_\_\_\_ volts V\_c and \_\_\_\_\_ mA l\_c.

 $V_c \approx 8V$  $I_c \approx 4 \text{ mA}$ 

10.3 The operating point on the set of transistor curves is point \_\_\_\_\_

С



If a step were applied so that the current through Q<sub>1</sub> would decrease by 1 mA and the current through Q<sub>2</sub> would increase by 1 mA, the power dissipated by Q<sub>1</sub> would \_\_\_\_\_\_ and the power dissipated by Q<sub>2</sub> would \_\_\_\_\_\_ increase/decrease

decrease increase

10.5

10.4

Draw the resulting output waveform for each transistor if a negative step is applied to the base of  $Q_1$  and a positive step is applied to the base of  $Q_2$ .

Collector Q1

Collector Q<sub>2</sub>

answer on next page







Determine the quiescent  $V_c$  and  $I_c$  and determine the operating point on the curves on the facing page for the circuit below. Draw the output waveform at each collector.



Collector Q<sub>1</sub>

answer on next page

$V_c \approx 6.2V$		
$I_c \approx 3 \text{ mA}$		
Operating at	Point	С

Collector Q<sub>1</sub>

Collector Q<sub>2</sub>

.0 To obtain thermal balance we operate the transistors in a push-pull circuit at \_\_\_\_\_\_ power, which is when \_\_\_\_\_\_ is equal to 1/2 V<sub>CC</sub>.





Answer to Frame 11.0:

maximum V<sub>CE</sub>

Let's assume that the operating point for the transistors in the circuit below is point Y on the facing page curves rather than point X as we had in Set 10.

Note: In the next set we will determine how we shift the operating point. In this set we want to see why it is desirable to shift the operating point to the maximum power point.



If we apply a negative step to the base of  $Q_1$ , the operating point moves to a higher  $V_{CE}$  and a lower power. The collector waveform will look as below.



As the transistor cools,  $I_c$  will decrease because  $V_{EB}$  is held constant.  $V_c$  will increase and this waveform will result.

At the same time we apply a positive step to the base of  $Q_2$ . The operating point moves to a lower  $V_{CE}$  and again a lower power. The collector output waveform will look as below.



As the transistor cools  $I_c$  will again decrease because  $V_{EB}$  is held constant.  $V_c$  will increase and this waveform will result.

If we take the output from the circuit now the drift due to thermal effects will cancel one another. The circuit is said to be thermally balanced.



For any circuit, that transistor will always be dissipating maximum power for that circuit when the  $^{V}$ CE of the transistor is 1/2 the collector supply voltage,  $V_{CC}$ . To be thermally balanced the transistors in a push-pull circuit must have a  $V_{CE}$  of  $1/2V_{CC}$  when balanced.

11.1 To be thermally balanced, the transistors in a push-pull circuit must be operating at \_\_\_\_\_\_ circuit power.

### maximum

11.2 To operate at maximum power the  $V_{CE}$  of the transistors must be \_\_\_\_\_% of  $V_{CC}$  in a balanced condition.

### 50%

11.3 If the load line below was the load line for transistors in a push-pull circuit and the transistors were thermally balanced, the transistor operating point would be



 $V_{CE} = 4.5V$ 

Assume that the  $V_{CC}$  to the transistors in a push-pull circuit is 14V, to operate the transistors at maximum power, we will operate at a  $V_{CE}$  of \_\_\_\_\_\_ volts. To be thermally balanced we will operate the transistors at a V<sub>CE</sub> of \_\_\_\_\_\_ volts.

7V 7V

Thermally balance the transistors in the circuit below .



12.0



The first step in determining the value of the thermal balance resistor is to determine the  $V_{CC}$  to the circuit. The collector voltage of +10V is easily observed. The emitter voltage is not so obvious. To determine the emitter voltage we must remember that in a push-pull circuit each transistor is driven by the same amplitude signal but 180° out of phase. One end of  $R_E$  (190 $\Omega$ ) will move positive by the same amount; the other end moves negative. The <u>center</u> of the resistor is at an effective AC ground. With this in mind we can redraw the emitter circuit of  $Q_1$  (see next page).



We are concerned with setting  $V_{CE}$  to  $1/2 V_{CC}$  when the push-pull circuit is in a balanced state. In a balanced state there is no DC current through  $R_E$ . Therefore, the effective ground at the center of  $R_E$  will be at the same DC potential as the emitter of  $Q_1$ . If we have silicon transistors this will be -.7V since the base is at 0V.

At this point we can Thevenize the emitter circuit and simplify the circuit for  $Q_1$  as below.



The  $V_{CC}$  of the circuit for  $Q_1$  is then 11V.

The emitter current for  $Q_1$  will remain 5 mA because it is conducting through the relatively large resistance of 5 k $\Omega$  (see facing page).

If the transistor is to drop  $1/2 \vee_{CC} (5.5 \vee)$ , then the series resistance must drop the other 5.5 $\vee$ . From Ohm's Law the series resistance must be:

$$R = \frac{5.5V}{5 \text{ mA}} = 1.1 \text{ k}\Omega$$

 $R_1 = 400\Omega$ ;  $R_E = 94\Omega$ . The thermal resistance must make up the difference.

$$R = 1.1 \text{ k}\Omega$$

$$R_{L} + R_{E} = 494\Omega$$

$$R_{Thermal} = 606\Omega \text{ or } \approx 600\Omega$$

Since the circuit for  $Q_2$  is the same as for  $Q_1$ , we also add a 600 $\Omega$  resistor to the collector circuit of  $Q_2$ . The circuit now looks as below.



The voltage gain of the stage is the same because the output is developed across only the  $400\Omega$  collector resistors. The voltage gain at the collectors of the transistors has more than doubled however. This doesn't affect the low frequency operation of the circuit but the high frequency performance will be impaired because of increased Miller effect.

We therefore supply an AC bypass capacitor (.001  $\mu Fd$ ) around the thermal balance resistor and have the final circuit as below .





12.1 Draw the emitter circuit for  $Q_1$  in the circuit on the facing page, assuming  $Q_1$  is a silicon transistor





 $\approx$  6 volts



10 mA

12.4 To be thermally balanced, Q1 must have a V<sub>CE</sub> of \_\_\_\_\_ volts.

3 volts

 $R_{\text{Total}} = \frac{3V}{10 \text{ mA}} = 300\Omega$ 



 $300\Omega$  –  $200\Omega$  (sum or  $R_{E}$  (50 ) and  $R_{L}$  (150  $)=\underline{100\Omega}$ 

12.7 To thermally balance  $Q_2$  we must add a resistor between the collector and the 150 $\Omega$  R<sub>L</sub> of \_\_\_\_\_\_ ohms.

100 $\Omega$  (it has the same circuit as  $Q_1$ )

12.8 To improve the high frequency performance we place a \_\_\_\_\_\_ in shunt with the thermal balance resistor.

capacitor



2.9 Redraw the circuit on the facing page with the thermal balance components added.

answer on next page

12.9



#### POST TEST

 Change the transistor low frequency equivalent circuit below to a high frequency equivalent circuit and label the parts.



- 2. In the manufacturing of a transistor, improving f will usually result in an increase in \_\_\_\_\_.
- 3. If we assume an  $\alpha$  of .98 in the transistor below, the current in the collector current generator,  $\alpha_{i}$ , is \_\_\_\_\_\_ mA.



4. As the resistance of the signal source to a common emitter transistor circuit is increased, the high frequency performance of that circuit will

# increase/decrease/remain the same

- 5. As the collector load resistor (R<sub>L</sub>) is increased, the gain of a common emitter circuit will \_\_\_\_\_\_\_ and the high increase/decrease/remain the same frequency performance will \_\_\_\_\_\_\_ increase/decrease/remain the same
- 6. To reduce collector capacitance  $(C_c)$ , we would \_\_\_\_\_\_ base to \_\_\_\_\_\_ increase/decrease voltage.
- 7. By increasing emitter current we improve the high frequency performance because \_\_\_\_\_\_\_ is reduced.
- 8. Even though the f<sub>t</sub> of one transistor is higher than that of another, the high frequency performance may be poorer because of a substantially increased
- 9. The common base configuration has \_\_\_\_\_\_ high better/poorer/about the same frequency performance than/as the common emitter configuration.



12. The high frequency performance of the common collector circuit, like the common emitter circuit, is limited by the higher input impedance. From the input the emitter base resistance  $(r_e)$  is seen as \_\_\_\_\_\_ times its actual value.

- 13. In all three transistor configurations, the high frequency performance is improved by operating the transistor at a  $_{large/small} V_{CB}$  and a  $_{large/small} I_{F}$ .
- 14. A minimum amount of power is dissipated by a transistory when operated in a mode switching circuit.
- 15. The maximum switching rate of a switching circuit is increased if the transistors are operated in a \_\_\_\_\_\_ mode switching circuit because \_\_\_\_\_\_ time is removed from the switching time.
- 16. V
  CE (sat)
  mode switching circuit.
- 17. Add components to the circuit below that will stabilize the DC output voltage against ambient temperature changes.



18. To thermally balance a push-pull transistor circuit, the transistor is one-half V<sub>CC</sub>.



19.

# POST TEST ANSWERS



2. r<sub>b</sub>'

1.

- 3. 9.8 mA
- 4. decrease
- 5. increase decrease
- increase
   collector
- 7.  $r_e ( \mathbf{r}_e = \frac{26}{I_E} )$
- 8. r<sub>b</sub>'
- 9. better
- 10. Miller capacitance

- 11. A<sub>v</sub>≈ 5
- 12. β
- 13. large large
- 14. saturated
- 15. current storage
- 16. saturated



18. V<sub>CE</sub>



19.