# INSTRUCTION MANUAL



Tektronix International A.G. 

070-220

Tektronix, Inc.

# K4XL's 🌮 BAMA

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#### **GENERAL DESCRIPTION**

The Tektronix 160-Series instruments are designed to supply timed pulses of adjustable amplitude and duration. A choice of power supplies is available as well as an indicator unit. The instruments may be mounted in any combination desired, and an adapter frame, the FA 160 is available for mounting in a standard 19-inch relay-rack.

#### **Type 360**

The Tektronix Type 360 Indicator contains a 3WP flat-faced crt, high-voltage supply, dc unblanking, vertical amplifier of 0.05 v/div sensitivity, and a horizontal amplifier with a gain of approximately two. It is designed to be powered by a Type 160, Type 160A, or Type 126 Power Supply and to receive its sweep and unblanking voltages from a Type 162 Waveform Generator; it can, however, be operated from any source of the proper voltages and waveforms. Several Type 360 Indicators can be driven by a single Type 162 and a simple Type 161-Type 162 hookup provides calibrated sweep delay. For low-level applications a Tektronix Type 122 Preamplifier provides increased ac sensitivity to 50-microvolts/div. A single Type 160 or Type 160A Power Supply can furnish the power to operate several combinations of the Type 160 Series instruments and Type 360 Indicators.

# Туре 126

The Tektronix Type 126 Power Supply provides the voltages and currents necessary to power one Type 360 Indicator or any one of the 160-Series Waveform Generators. It mounts beneath the unit to be powered, and includes a cabinet to house both the Type 126 and the unit powered.

#### Type 160 and Type 160A

The Tektronix Type 160 and Type 160A power supplies are designed to furnish current for the instruments composing the 160-Series. Either instrument will mount in the Type FA 160 adapter frame beside a combination of Pulse Generators.

The Type 160A can safely supply six 161's or six 162's. This is due to the internal shunt resistor incorporated in these units which permits 170 ma to be safely drawn from the supply. If you wish to use the Type 160A to supply some other device, however, only 125 ma may safely be drawn from the supply. To exceed this rating you must provide an external shunt resistor for the 225-volt supply.

#### Type 161

The Tektronix Type 161 Pulse Generator is designed to supply calibrated rectangular output pulses of adjustable duration and amplitude and of either polarity when the required trigger voltage is received from an external source. Two types of trigger waveforms can be used to trigger the Type 161, a negative-going sawtooth or a positive pulse. One output pulse is generated for each input pulse or each cycle of the sawtooth.

When a negative sawtooth waveform is used to trigger the generator a rectangular pulse of either polarity and a 50-volt positive gating pulse are generated. The time of occurrence of the pulse and of the gate can be adjusted to any point throughout the duration of the sawtooth. The duration of the generated pulse and the output gate are the same. When a positive pulse is used to trigger the generator, the same output waveforms are available, but there is no delay available in the generation of the pulse.

# Type 162

The Tektronix Type 162 Waveform Generator provides three types of waveforms of adjustable duration and repetition rate: pulse, gate, and sawtooth. Generation of the waveforms can be initiated either by means of an externally derived electrical impulse, or by means of front-panel controls and switches. Pulse and gate waveforms have a minimum risetime of the order of one microsecond and an amplitude of 50 volts. The shortest pulse duration is of the order of 10 microseconds. The sawtooth waveform is a positive voltage decreasing uniformly from positive 150 volts to positive 20 volts.

The device is useful for initiating chains of events electrically, and for controlling the duration of their occurrence and their repetition rate. When generating waveforms recurrently, the instrument provides an unusually stable repetition rate. The Type 162 is specifically designed to operate in conjunction with Tektronix Type 161 Generators.

# Type 163

The Tektronix Type 163 Pulse Generator is designed to supply rectangular output pulses of adjustable duration and amplitude when the required trigger voltage is received from an external source.

Two types of triggering waveforms can trigger the Type 163 Pulse Generator, a negative-going sawtooth or a positive pulse. One output pulse is generated for each input pulse or for each cycle of the input sawtooth.

The gate output pulse is taken from the cathode of a cathode follower and the adjustable pulse is taken from a potentiometer comprising the cathode resistor of this cathode follower. The duration of the adjustable pulse and the gate pulse are therefore the same.

The time of occurrence of the output pulse and gate can be adjusted to any point throughout the duration of the triggering sawtooth.

# **PULSE GENERATOR**

# **Output Waveform**

Type 161

Positive Gate. Positive Pulse. Negative Pulse.

Type 162

Positive Pulse. Positive Gate. Negativegoing Sawtooth.

Type 163

Positive Gate. Positive Pulse.

# **Positive Pulse Characteristics**

Type 161

Amplitude, 0 to 50 volts, continuously variable.

Duration, 10  $\mu \sec$  to 0.1 sec continuously variable.

Risetime, .5  $\mu$ sec or better when load capacitance is 10  $\mu\mu$ f or less.

Overshoot, less than 5%.

Delay, 0 to 100% of duration of input sawtooth.

#### Type 162

Amplitude, 50 volts positive from ground.

Duration, 10  $\mu$ sec. to .05 sec.

Risetime,  $1 \mu sec_approximately$ , minimum.

Repetition rate, 0.1 cps to 10 kc for recurrent operation.

#### Type 163

Amplitude; continuously adjustable between 0 and 25 volts, peak to peak. Other characteristics, same as gate.

#### Negative Pulse Characteristics

Type 161

Similar to positive pulse, except polarity.

#### **Gate Characteristics**

Type 161

Amplitude, 50 volts positive from ground potential, not adjustable.

Type 162

Amplitude, 50 volts positive from ground.

Duration, 100  $\mu$ sec to 10 sec.

Repetition rate, 0.1 cps to 10 kc for recurrent operation.

Type 163

Amplitude, fixed, 25 volts, peak to peak.

Duration, 1  $\mu$ sec to 10,000  $\mu$ sec, continuously adjustable.

Risetime, .2  $\mu$ sec or better when load capacitance is 10  $\mu\mu$ f or less.

Decay Time, 0.2 to 0.5  $\mu$ sec.

Overshoot can be adjusted to zero.

Delay, 0 to 100 per cent of sawtooth duration.

# Sawtooth Characteristics

Type 162

Amplitude decreases uniformly with time from positive 150 volts to positive 20 volts.

Duration, 100  $\mu$ sec to 10 sec.

Repetition rate, 0.1 cps to 10 kc for recurrent operation.

#### Output Impedance

Type 161

Positive pulse, 1800 ohms maximum. Negative pulse, 5000 ohms maximum. Positive gate, 1000 ohms maximum.

Type 162

Approximately 1000 ohms for all outputs.

Type 163

Gate 100 ohms.

Pulse, 500 ohms (varies with pulse-amplitude control setting).

Minimum load resistance 3.5 k.

#### Method of Triggering

Type 161

Positive pulse, or negative-going positive sawtooth.

Type 162

Externally derived electrical pulse or gate. Front-panel pushbutton or switch.

#### Triggering Input Impedance

Type 162

High impedance, consisting of control grid with 1-megohm grid return resistor.

#### **Trigger Sensitivity**

Type 161

Positive pulse, 3-volts peak-to-peak, minimum.

Maximum repetition rate 50 kc.

Type 162

Positive pulse, 15 volts peak or greater with rise time 5 milliseconds or less.

Sine wave, 6 volts rms, frequency between 5 cps and 50 kc. At frequencies below 5 cps, the product of rms voltage times frequency must exceed 10.

#### Type 163

Positive pulse, 2 volts peak-to-peak, minimum.

Negative-going sawtooth. Must include dc bias sufficient to keep voltage positive.

# **Gate Sensitivity**

Type 162

Eight volts.

#### **Power Requirements**

Type 161

225 volts dc positive at 22 ma.170 volts dc negative at 17 ma.6.3 volts ac or dc at 1.65 amps.1.1 amp to S/N 135.

Type 162

225 volts dc positive at 28 ma.150 volts dc positive at 1 ma.170 volts dc negative at 7 ma.6.3 volts ac at 1.7 amps, through male octal socket at rear of instrument.

(TEKTRONIX Type 160A Power Supply is specially designed to furnish the required power for as many as seven of these units.)

Type 163

-170 volts at 26 ma.

+ 225 volts at 35 to 45 ma (minimum to maximum pulse duty cycle).

Five Type 163 units can be operated at once from a Type 160A Power Supply.

#### **POWER SUPPLY**

#### Voltage and Current Outputs

Type 160

+300 volts dc, unregulated, at 170 milli-amps\*.

+ 225 volts, dc, regulated, at 125 milliamps. + 150 volts dc, regulated, at 5 milliamps. -170 volts dc, regulated at 125 milliamps. 6.3 volts ac, unregulated, at 10 amps.

\*current limitation of the winding in absence of any current through + 225-volt regulated circuit.

Type 160A

+300 volts dc, unregulated, at 250 milliamps.\*

+225 volts dc, regulated, at 175 milliamps.\*\*

+150 volts dc, regulated at 15 milliamps. +70 volts dc, unregulated. \*

-170 volts dc, regulated, at 125 milliamps. 6.3 volts ac, unregulated, at 20 amps.

\* Voltage varies with load.

\*\* Will regulate at 225 ma with a 1500-ohm shunt across the 225-volt series tube.

Type 126

+ 300 volts dc, unregulated at 65 milliamps.\* + 225 volts, dc, regulated at 45 milliamps. + 150 volts, dc regulated at 5 milliamps. -170 volts dc, regulated at 30 milliamps. 6.3 volts ac, unregulated at 4 amps.

\* In the absence of any current drawn from the 225-volt supply.

# Regulation

Type 160

Electronic, with Type 5651 gas diode reference element.

#### Type 160A

Electronic regulation compensates for linevoltage variations between 105 and 125 volts, and for current-demand differences of the units connected to the power supply.

Type 126

Electronic regulation compensates for linevoltage variations between 105 and 125

 $AA_1$ 

volts, and for current differences of the units connected to the power supply.

# Ripple

Type 160A

At rated load the ripple is about 40 millivolts at the +225-volt supply, 25 millivolts at the -170-volt supply and 8 millivolts in the +150-volt supply.

#### Type 126

At rated load the ripple is about 40 millivolts on the +225-volt supply, 30 millivolts on the +150-volt supply, and 10 millivolts on the -170-volt supply.

#### INDICATOR

#### Input Impedance

Vertical

Direct, 1 megohm shunted by 40  $\mu\mu f$ . Probe, 10 megohm shunted by 14  $\mu\mu f$ .

#### Frequency Response

#### Type 360

#### Functions of Controls and Connectors

FOCUS Adjustable voltage for the crt focusing grid.

INTENSITY Bias adjustment for crt control grid.

SCALE ILLUM Adjustable resistor to control the voltage across the graticule lights.

VERT GAIN ADJ. Screwdriver front-panel control to calibrate the VOLTS/DIV control.

DC BAL Screwdriver front-panel control to adjust the dc levels so the trace does not shift position vertically when the VARIABLE control is rotated.

SWEEP CAL Screwdriver front-panel control to adjust the sweep to match the ruled graticule.

+GATE INPUT Binding post input to crt unblanking circuit.

Vertical

DC to 500 KC.

Horizontal

DC to 100 kc.

#### Calibrated Sensitivities

Vertical

0.05, 0.5, 5, and 50 volts/division (Continuously variable sensitivity between calibrated steps.)

# Maximum Input Voltage

Vertical

600 v (dc plus peak ac).

#### Waveforms Required

Horizontal

Positive- or negative-going sawtooth, 110 to 150 volts excursion within the limits of -95 volts to +170 volts.

Gate, 45 to 75 volts positive same duration as the sawtooth.

VOLTS/DIV	Switch to select fixed frequency-compensated attenuators which produce the sensitivity indicated when the VARIABLE control is in the CALIBRATED position.
VARIABLE	Variable gain control with about a 10 to 1 range.
POSITIONING VERT (red)	Control to position the trace vertically.
HORIZ (black)	Control to position the trace horizontally.
VERTICAL INPUT	UHF coax connector to vertical amplifier.
AC-DC	Switch to insert or remove coupling capacitor for ac-or dc-coupled operation.
SAWTOOTH INPUT	Binding post input to horizontal amplifier.

# Type 161 Functions of Controls and Connectors

INPUT	Connector to TRIGGER SELECTOR switch for connecting external trigger source. (For example, TEKTRONIX Type 162 Waveform Generator.)
TRIGGER SELECTOR	Two-position toggle switch to accommodate input circuit to POS. PULSE input or NEG. SAWTOOTH input.
OUTPUT PULSE DELAY	Variable potentiometer to adjust comparison voltage in sawtooth comparator circuit. Triggers when the two are equal.
POS. TRIGGER BIAS	Same variable potentiometer as above, adjusts operating bias of pulse amplifier for most satisfactory triggering.
NEG. DELAY LIMIT	Screwdriver-adjustable resistor in series with negative end of OUTPUT PULSE DELAY potentiometer, for adjusting low voltage triggering level of voltage comparator circuit to accommodate scale calibrations to various sawtooth amplitudes.
POS. DELAY LIMIT	Screwdriver-adjustable resistor in series with positive end of OUTPUT PULSE DELAY potentiometer, for adjusting high voltage triggering level of voltage comparator circuit to accommodate scale calibration to various sawtooth amplitudes.
PULSE WIDTH	Four-position switch selects value of coupling capacitor in pulse-generating multivibrator, determines discharge time in conjunction with PULSE WIDTH MULTIPLIER variable resistor, and thereby determines pulse width.
PULSE WIDTH MULTIPLIER	Continuously-variable resistor in coupling circuit of pulse-generating multivibrator, determines discharge time in conjunction with PULSE WIDTH adjustable capacitor, and thereby determines pulse width.

- PULSE WIDTHScrewdriver adjustable voltage-pickoff potentiometer, adjusts positive biasCALIBRATORon pulse-generator multivibrator to accommodate PULSE WIDTH calibrations<br/>to characteristics of multivibrator tube. May require readjustment when<br/>multivibrator tube is replaced.
- PULSEVoltage-pickoff variable potentiometer with contact arm connected toAMPLITUDEPULSE OUT terminal, determines percentage of developed pulse that<br/>is made available to output terminal. Calibrated in volts.
- PULSETwo-position toggle switch, applies output of either positive or negativePOLARITYpulse amplifier across PULSE AMPLITUDE potentiometer.
- PULSE OUT Binding post connected to arm of PULSE AMPLITUDE potentiometer.
- GND Binding post connected to metal chassis of instrument.

GATE OUT Binding post to cathode-follower positive gate amplifier.

# Type 162

# Functions of Controls and Connectors

MANUAL	Pushbutton (SW2) for initiating a pulse or chain of pulses manually.
+GATE IN	Panel connector for connecting an external source of positive gate voltage to the instrument.
+TRIGGER IN	Panel connector for connecting an external source of triggering voltage to the instrument.
OPERATING MODE	Five-Position, three-section rotary switch (SW1A,B,C) for selecting the source and mode of triggering action.
MAN., ONE CYCLE	One phantastron run-down occurs each time MANUAL pushbutton is depressed.
MAN., CONTINUOUS	Phantastron runs recurrently during period MANUAL pushbutton is depress- ed, and completes a rundown if pushbutton is released before a rundown is completed.
RECURRENT	Phantastron runs recurrently as long as OPERATING MODE switch remains in this position.
GATED	Connects +GATE terminal to triggering circuits. Phantastron operates recurrently during period of gate. Completes run-down if gate terminates during a run-down.
TRIGGERED	Connects +TRIGGER terminal to triggering circuits.Phantastron executes one run-down for each positive pulse received.
CAL	Screwdriver adjustable 50-k resistor in voltage divider of phantastron discharge circuit. Correct setting of this control makes WAVEFORM DURATION dial direct reading.
VERNIER	Potentiometer in phantastron discharge circuit for vernier control of wave-

form duration or repetition rate. Must be set on the CALIBRATED POSITION index for WAVEFORM DURATION dial to read correctly.

WAVEFORMEleven-position switch varies phantastron discharge resistance to giveDURATIONa time variation of ten-to-one.oror

PULSE INTERVAL

- MULTIPLIER Five-position switch selects phantastron timing capacitors to give decade series of time multipliers between 0.1 and 1000 times the reading of the WAVEFORM, INTERVAL dial.
- GATE OUT, PULSE OUT Two-position toggle switch selecting dc or ac coupling to shaping amplifier, thereby determining type of output at panel connector located immediately below the switch.

SAWTOOTHPanel connector from cathode of phantastron plate to grid coupling cathode-<br/>follower.

# Type 163 Functions of Controls and Connectors

INPUT	Connector to TRIGGER SELECTOR switch for connecting external trigger source.
TRIGGER SELECTOR	Two-position toggle switch to accommodate input circuit to POS. PULSE input or NEG. SAWTOOTH input.
OUTPUT PULSE DELAY	Variable potentiometer to adjust comparison voltage in voltage-comparator circuit to compare with sawtooth triggering waveform.
POS. TRIGGER BIAS	Same variable potentiometer as above, adjusts operating bias of pulse amplifier for most satisfactory triggering.
NEG. DELAY LIMIT	Screwdriver-adjustable resistor in series with negative end of OUTPUT PULSE DELAY potentiometer, for adjusting low-voltage triggering level of voltage-comparator circuit to accommodate scale calibrations to various sawtooth amplitudes.
POS. DELAY LIMIT	Screwdriver-adjustable resistor in series with positive end of OUTPUT PULSE DELAY potentiometer, for adjusting low-voltage triggering level of voltage-comparator circuit to accommodate scale calibrations to various sawtooth amplitudes.
PULSE WIDTH	Four-position switch selects value of coupling capacitor in pulse-generating multivibrator, determines discharge time in conjunction with PULSE WIDTH MULTIPLIER variable resistor, and thereby determines pulse width.
PULSE WIDTH MULTIPLIER	Continuously-variable resistor in coupling circuit of pulse-forming multi- vibrator, determines discharge time in conjunction with PULSE WIDTH selected capacitor, thereby determines pulse width.

PULSE WIDTH CALIBRATOR	Screwdriver adjustable voltage-pickoff potentiometer, adjusts negative bias on pulse-generator multivibrator to accommodate PULSE WIDTH calibrations to characteristics of multivibrator tube. May require readjust- ment when multivibrator tube is replaced.
PULSE AMPLITUDE CALIBRATOR	Screwdriver-adjustable potentiometer which adjusts the bias on the output cathode follower to accommodate PULSE AMPLITUDE calibrations to characteristics of cathode-follower tube.
PULSE AMPLITUDE	Voltage-pickoff variable potentiometer with contact arm connected to PULSE OUT terminal, determines percentage of developed pulse that is made available to output terminal. Calibrated in volts.
PULSE OUT	Binding post connected to arm of PULSE AMPLITUDE potentiometer.
GND	Binding post connected to metal chassis of instrument.
GATE OUT	Binding post to cathode-follower gate amplifier.

# Lists of Included Accessories

#### 126

1-3 to 2-Wire adapter, 103-013. 1-3-conductor power cord, 161-010. 2-Instruction manuals.

#### 160

2-Inter-unit power cables, 012-016. 1-3 to 2-wire adapter, 103-013. 1-3-conductor power cord, 161-010.

2-Instruction manuals.

# 161, 162, 163

1-Inter-unit power cable, 012-017. 2-Instruction manuals.

#### 360

- 1-P6017 Probe, 010-038.
- 1-Inter-unit power cable, 012-016. 1-Green filter, 378-509. 2-Instruction manuals.



# SECTION 2

# OPERATING INSTRUCTIONS

#### Type 162

#### General

The Tektronix 160-Series instruments, including the Type 360 Indicator and the Type 126 Power Supply, may be operated in any normal indoor location, or in the open if protected from moisture. If an instrument has been exposed to moisture, it should be left in a warm room until it has become thoroughly dry before placing it in operation.

#### **Power Supply Requirements**

Power for the 160-Series instruments can be furnished by the Type 160A Power Supply or any well regulated power supply capable of furnishing the required voltages and current. Specifications and requirements for the instruments are given in the Specifications section of this manual. If a Tektronix Type 160 or Type 160A Power Supply is used, install the interunit octal-plug power cable.

#### Multiple Connection of Type 160-Series Instruments

The 160-Series Pulse Generators and the Type 360 Indicator are equipped with one male octal input power receptacle and one female output socket connected in parallel. Additional units may be connected by means of additional interunit power cables.

The SAWTOOTH OUT waveform of the Type 162 is specially designed to provide the required NEG. SAWTOOTH input waveform for the TEK-TRONIX Type 161 Pulse Generator so as to obtain pulse sequences with precise and adjustable delay between the initiating pulse and the output pulse, and to provide a stable source of repetition rate for the Type 161.

#### Type 360

#### **Preliminary Instructions**

#### Mounting

If the Type 360 is to be rack mounted in the FA 160 Mounting Frame or in a mounting of your own construction do not place the instrument immediately adjacent to the 160 Power Supply as the external magnetic field of the fan motor may affect the crt display. One of the other 160 Series instruments placed between the power supply and the indicator will provide sufficient isolation. Or you can safely place the 360 above or below the 160A.

#### Illuminated Graticule

The brightness of the illuminated graticule can be adjusted to suit ambient light conditions by means of the SCALE ILLUM control. The filter supplied is colored to provide the maximum trace contrast for the P2 phosphor in the presence of room light. Place the filter next to the crt face so it does not block the light from the graticule lines. The scribed face of the graticule should be toward the crt face to reduce parallax.

The graticule is accurately scribed in quarterinch divisions. These scale markings and the calibrated vertical-deflection sensitivities can be used to convert deflection in centimeters into volts of signal amplitude. If a 162 is used to provide the sweep sawtooth for the 360 Indicator a similiar conversion can be made to yield time in seconds so the amplitude and duration of the displayed waveform can be read directly from the scribed graticule. As a general rule, white graticule lines are superior to red for photographic purposes.

Where the volume of photographic work warrants it, you may want to obtain a clear graticule from your Tektronix Field Engineer.

#### Cathode-Ray Tube Controls

At normal INTENSITY settings the crt beam is biased off and a positive 50-volt unblanking gate is required to turn the beam on and produce a visible trace. You can, however, increase the INTENSITY enough to produce a visible trace without the unblanking gate but the retrace will be visible at the faster sweep speeds.

The ASTIGMATISM control is preset for the particular crt and accelerating voltage and normally will not need to be readjusted. The FOCUS and INTENSITY adjustments interact slightly so that the FOCUS may need to be touched up slightly for different INTENSITY settings.

#### FIRST-TIME OPERATION

The following material will assume the Type 360 Indicator will be used with the Tektronix 160 Series. If you are going to use the indicator with other equipment check further in this section of the manual for the required operating conditions.

Plug the power cable into the male plug of the Indicator unit and connect the other end to the power supply or to the power socket of any of the other 160 Series units that you might have already connected to the power supply.

Connect a lead between the +GATE INPUT binding post on the 360 and the GATE OUT, PULSE OUT binding post on the 162. Connect another lead between the SAWTOOTH INPUT binding post on the 360 and the SAWTOOTH OUT binding post on the 162. Set the front-panel controls on the 360 and the 162 as follows:

360 CONTROLS	
FOCUS INTENSITY VOLTS/DIV VARIABLE POSITIONING	center full left 50 full right
VERT HORIZ AC, DC	center center AC
162 CONTROLS	
OPERATING MODE	RECURRENT

	RECORDENT
VERNIER	CALIBRATED
	POSITION
WAVEFORM DURATION	1.0
MULTIPLIER	1.0
GATE OUT, PULSE OUT	GATE OUT

Switch the power supply on and wait about 30 seconds for the tube heaters to reach operating temperature. Advance the indicator INTENSITY control until the trace is visible and adjust the FOCUS control if necessary to make the trace as fine as possible.

#### Sweep Timing

The accuracy with which you can read time directly from the ruled graticule will depend on the calibration of both instruments. The Type 162 generates a sawtooth of known duration. With the controls set as suggested for "First-Time Operation" the sawtooth duration is 10 milliseconds. If the indicator's horizontal amplifier is adjusted so this 10-millisecond sawtooth will produce a trace that is exactly 10 divisions long then time can be read directly from the graticule lines. In this case the sweep speed is 1 millisecond per division. Always make sure the duration of the sawtooth as indicated by the 162 WAVEFORM DURATION control is correct and then adjust the 360 SWEEP CAL control so the displayed sweep is 10 divisions long. For a more accurate method of timing the sweep see the MAIN-TENANCE section.

#### **Vertical Amplifier**

Input to the vertical amplifier is made via the UHF connector labeled VERTICAL INPUT. The VOLTS/DIV control establishes the sensitivity of the vertical amplifier. There are four fixed calibrated sensitivities of 0.05, 0.5, 5 and 50 volts/div and the VARIABLE control has a range of a little over 10 to 1 so the sensitivity is continuously variable between calibrated steps. The probe furnished with the indicator will provide an additional 10times attenuation and reduce the loading on the circuit under test.

#### **Operation With Other Equipment**

There are several requirements for operation of the 360 that are taken care of automatically when the Indicator is used with the 160 Series Power Supply and Waveform Generator. The first requirement is power to operate the indicator. The +225-volt and the -170-volt supplies should be within about 5% of these values and should be well regulated as they determine the operating potentials of the amplifiers and serve as reference potentials for the regulated high-voltage supply. The unregulated 300-volt supply which furnishes power to the high-voltage oscillator can be as low as 250 volts or as high as 350 volts or you can use a regulated supply for this but there is very little to be gained as the high-voltage supply has its own regulation. The heater supply should be within + or - 10% of 6.3 volts at full load as recommended by tube manufacturers.

The horizontal amplifier will accommodate either a positive-going or negative-going sawtooth and the total sawtooth excursion and dc level can vary within limits. The minimum practical sawtooth excursion is about 110 volts and the excursion must be within the limits of about -95 volts to +170 volts. The maximum practical excursion is about 150 volts and should be within the limits of -90 volts to +160 volts as the horizontal positioning range is less at this operating condition.

The general procedure for adapting the 360 for a sawtooth that falls within the above specifications is as follows:

1. Remove the cabinet so the internal controls are accessible and switch the SAWTOOTH

POLARITY switch to either POSITIVE SAW-TOOTH or 162SAWTOOTH depending on whether you will use a positive or negative-going sawtooth. Make all power and front-panel connections to the 360 and turn the equipment on. Center the SWEEP CAL control (screwdriver slot straight up and down) so you will have a fine adjustment in both directions after you make the coarse adjustment.

2. Change the crt accelerating voltage by means of the H. V. ADJ control so the displayed trace is about 10 divisions long. The H. V. ADJ control can be reached with a screwdriver through a slot in the shield at the lower right rear of the instrument. Make any final adjustment with the SWEEP CAL control.

#### NOTE

When you change the crt accelerating voltage you change the vertical sensitivity as well as the horizontal sensitivity so it will be necessary to recalibrate the VOLTS/DIV switch.

The unblanking signal should be a flat-topped positive square wave of about 45 to 75 volts amplitude. If the rise time of the unblanking waveform is too long the first part of the trace will not be visible and as the unblanking waveform is dc coupled to the crt grid any tilt to the top of the square wave will cause a variation of trace intensity.

#### Type 161

#### General

The TEKTRONIX Type 161 Pulse Generator will operate in any normal indoor location, or in the open if it is protected from moisture. If the instrument has been exposed to moisture, leave it in a warm dry room until it is thoroughly dry before placing it in operation.

Operate the instrument in such a way that good ventilation can take place, so that high internal temperatures will not occur. All components are well supported and the instrument is quite rugged, but it should not be roughly handled.

#### FIRST-TIME OPERATION

Power for the Type 161 Pulse Generator can be furnished by the TEKTRONIX Type 160, Type 160A Power Supply, or by any wellregulated supply capable of furnishing the required voltages and currents.

If the TEKTRONIX Type 160 or 160A Power Supply is used, install the interunit octal-plug power cable. No particular precautions are required before power is applied to the unit.

The Type 161 must be triggered from an external source with a trigger waveform of the proper characteristics. The TEKTRONIX Type 162 Waveform Generator will furnish both the required pulse and sawtooth waveforms. The following is a list of convenient settings of controls for observing the operation:

TRIGGER SELECTOR	POS. PULSE
POS. TRIGGER BIAS	.3
PULSE WIDTH	1
PULSE WIDTH	
MULTIPLIER	1
PULSE AMPLITUDE	20
PULSE POLARITY	POS.

Connect a step voltage to the INPUT terminal which has a peak of at least six volts, and observe the output of the PULSE OUT terminal on an oscilloscope, such as TEKTRONIX Type 532. Set the sweep time of the oscilloscope at approximately 1 millisecond per centimeter, and a pulse will appear approximately 1 centimeter long.

# Method of Triggering the Type 161 Pulse Generator

Two triggering waveforms may be used: a positive pulse or a negative-going positive sawtooth. The positive pulse requirements are not strict. Any positive peak value above 2 volts will consistently trigger a pulse. The maximum peak voltage should not exceed about 250 volts. Fig. 2-1 shows a simple battery connection for triggering the Type 161.



The negative-going sawtooth must have a dc component such that it does not go below about 20 volts positive at any part of the cycle. The maximum positive excursion of the sawtooth should not exceed about 200 volts. The Type 162 Waveform Generator will furnish a suitable sawtooth triggering waveform.



Fig. 2-2. The Sawtooth Out waveform from the Type 162 Waveform Generator is used to trigger the Type 161. Note that the output pulse from the Type 161 may be delayed with respect to the triggering waveform.

# Type 162

#### First Time Operation

No particular precautions are required before power is applied to the unit. The following is a convenient setting of controls for observing the operation: Set the OPERATING MODE switch to RECURRENT, the VERNIER control to CALIBRATED POSITION, the WAVEFORM DURATION switch to 1.6, and the MULTIPLIER switch to 10. With these settings, a sawtooth wave of about 60-cycle frequency should be observable at the SAWTOOTH OUT terminal using an oscilloscope such as the TEKTRONIX Type 532. Similarly, a pulse or gate should be observable at the PULSE OUT, GATE OUT terminal, depending upon the position of the toggle switch, located immediately above the terminal, which determines whether gate or pulse output is produced.

# Method of Triggering and Gating the Type 162

A basic method of triggering the Type 162 is the use of a radio B battery connected

between one of the two input terminals and the ground terminal of the instrument, through a pushbutton or momentary switch. Although the instrument will trigger on eight or ten volts, a 22 1/2 -volt or 45-volt B battery provides a very dependable trigger source.



If the battery is connected as shown in Fig. 2-3, with the negative terminal of the battery connected to the +TRIGGER IN, triggering will not take place when the switch is depressed, but when it is released, as shown in Fig. 2-3. The instrument will not be operated at all if the battery is connected in this manner to the +GATE IN.



A more usual method of connecting a battery triggering source is shown in Fig. 2-4, where the positive terminal of the battery is connected to the instrument input terminal, in this case to the + TRIGGER IN terminal, and the OPERATING MODE switch is turned to the extreme right to the TRIGGERED position. As shown in Fig. 2-4 the output wave commences at the same time as the input pulse.



Fig. 2-5. The Type 162 connected for gated operation. Note the relationship between the waveforms.

Fig. 2-5 shows input and output waveforms when the input signal is connected to the +GATE IN terminal, and the OPERATING MODE switch is turned to the GATED position. Output commences when the input gating signal begins, and continues until the input signal returns to zero. If a sawtooth has begun before the termination of the gating signal, it will be completed even though the gating signal has already returned to zero. At the PULSE OUT terminal, a series of pulses will be available, the first pulse occurring simultaneously with the start of the gating signal, and subsequent pulses occurring at the start of subsequent sawtooth waves.



Fig. 2-6. The Type 162 operated in the Manual, One-Cycle, Operating Mode.

Fig. 2-6 shows the output waveform with relation to the position of the MANUAL pushbutton control when the OPERATING MODE switch is in the MANUAL, ONE CYCLE position. A single sawtooth and a single pulse are produced regardless of the length of time the pushbutton remains depressed.



Fig. 2-7. The Type 162 operated in the Manual, Recurrent, Operating Mode.

Figure 2-7 shows the output waveform with relation to the position of the MANUAL pushbutton control when the OPERATING MODE switch is in the MANUAL, CONT. position. A recurrent sawtooth and a series of pulses are produced as long as the button remains depressed. A sawtooth which is started just before the release of the pushbutton will continue until an entire sawtooth waveform is completed.

#### Type 163

#### Methods of Triggering the Type 163 Pulse Generator

The Type 163 must be triggered from an external source with a trigger waveform of the proper characteristics. The TEKTRONIX Type 162 Waveform Generator will furnish both the required pulse and sawtooth waveforms. The following is a list of convenient settings of controls for observing the operation. Set TRIGGER SELECTOR switch to POS. PULSE position. POS. TRIGGER BIAS to 0.6. PULSE WIDTH to 1000 microseconds. PULSE WIDTH MULTIPLIER to 1. PULSE AMPLITUDE to 20. Connect a step voltage which has a peak of at least six volts to the INPUT terminal and observe the output at the PULSE OUT terminal using an oscilloscope such as TEKTRONIX Type 532. Set the sweep time of the oscilloscope at approximately 1 millisecond per centimeter, and a pulse will appear approximately 1 centimeter long with the foregoing settings.

Two triggering waveforms may be used: a positive pulse or a negative-going positive sawtooth. The positive pulse requirements are not strict. Any positive peak value above 2 volts will consistently trigger a pulse. The maximum peak voltage should not exceed about 250 volts.

Triggering is similiar to that used with the Type 161. Refer to Figures 2-1 and 2-2 for suitable hookups.

The negative-going sawtooth must have a dc component such that it does not go below about 20 volts positive at any part of the cycle. The maximum positive excursion of the sawtooth should not exceed about 200 volts. The Type 162 Waveform Generator will furnish a suitable sawtooth triggering waveform. See "Maintenance" for instructions for calibrating the OUTPUT PULSE DELAY dial.

# Applications

Many combinations of Tektronix 160-Series instruments are possible. The following material illustrates a few of these combinations. While these applications have been prepared with a slant toward biological research fields. they are intended to acquaint you with some of the possible uses of the Type 160-Series Units.

#### **Explanatory Note**

In examining these waveforms on an oscilloscope the waveform to be examined may be used as an initiating pulse to trigger the oscilloscope sweep, due attention being paid to the polarity of the waveform. This is accomplished by connecting the output to be examined with the External Trigger binding post on the oscilloscope, and making the proper adjustments of TRIGGER MODE, STABILITY and TRIGGERING LEVEL. It should be borne in mind that the sweep transit time must be equal to or longer than the duration of the waveform to be examined if the entire waveform is to be seen on the sweep. If the sweep transit time is less than the waveform duration. only a portion of the waveform will be seen. The waveform to be examined is impressed on the vertical deflection plates by connecting the vertical amplifier probe with the output terminal under examination.

#### Initiating Pulses

A. For 161

 $1. \ \mbox{Negative-going sawtooth from Tektronix scope.}$ 

2. Negative-going sawtooth from 162.

3. Positive-going pulse from delayed trigger output of scope.

4. Positive-going pulse from 162.

5. Positive-going pulse from external source.

6. Negative-going pulse derived from fly back of conventional oscilloscope sweep generator.

#### B. For 162

1. Any positive-going pulse may be used for triggered operation.

2. Any positive-going waveform may be used for gated operation, the 162 recycling for the duration of the waveform.

#### 1a.Initiating pulse derived from Tektronix Type 162



Fig. 2-8. Free running Type 162 determines rate of 161 pulse formation. Position of pulse on sweep determined by delay setting of 161. Parameters of pulse determined by amplitude and duration controls on 161.

# 1b. Initiating pulse derived from Tektronix 532 Oscilloscope



Fig. 2-9. Free running oscilloscope sweep determines rate of 161 pulse formation. Position of pulse on sweep determined by delayed trigger control on panel of oscilloscope. Parameters of pulse determined by amplitude and duration controls on 161.



Fig. 2-10. Free running oscilloscope sweep determines rate of 162 sawtooth formation. Position of beginning of sawtooth pulse determined by setting of delayed trigger control on panel of oscilloscope. Duration of sawtooth determined by setting of waveform duration controls on panel of 162. A positive-going gate of the same duration as the sawtooth may be obtained simultaneously from the other output connection.



Fig. 2-11. Free running oscilloscope sweep determines rate of 162 pulse formation. Position of pulse with relation to sweep determined by delayed trigger control on panel of oscilloscope. Interval between pulses out of 162 determined by pulse interval controls on panel of 162. If this interval is longer than the oscilloscope sweep interval, the 162 will not pulse with each sweep. If this interval is equal to the oscilloscope sweep interval, the 162 will pulse once with each sweep. If this interval is shorter than the oscilloscope sweep interval, the 162 will pulse as many times as it can during the period of positivity of the delayed trigger output. A negative-going sawtooth is available at the other output terminal starting simultaneously with each pulse.

# II. Initiating pulse derived from external source other than oscilloscope

This requires only some means of controlling a source of voltage in excess of 8-10 volts. A manually operated switch or a mechanically operated switch in a circuit containing the required source of voltage will supply the

necessary pulse each time the switch contacts close or open. Since both the 161 and 162 respond to positive-going pulses, the following conditions establish the characteristics of operation:



Fig. 2-12. Since the initiating pulses are positive-going waveforms, more predictable and less confusing operation will probably be obtained if the control pulse is habitually obtained from the positive terminal of the source.

A. 162 Triggered.





B. 162 Gated. Duration of switch closure 1 sec.



Fig. 2-14. The output gate and sawtooth durations are identical and are determined by the panel control settings. If these durations are set at 1 sec. or more, the operation will occur once each time the switch is closed. If these durations are less than 1 second, the operation will recycle for the entire 1 second of switch closure. The number of cycles will be given by the quotient of duration of switch closure divided by the waveform duration.





Fig. 2-15. The pulse formation starts at the instant of switch closure. The dimensions of the pulse are determined by the panel control settings.

# III. Operation independent of external initiating pulse

A. The 161 pulse generator will not operate in this way. It requires an initiating pulse.

B. 162 on Recurrent operation.



Fig. 2-16. Two outputs are available. Positive-going pulses occur at intervals determined by the controls on the panel. Negative-going sawtooths occur at the same intervals. The rundown of the sawtooth starts at the time of each pulse and continues throughout the interval between pulses. This operation continues as long as the selector is on Recurrent and the proper voltages are supplied.

C. 162 on Manual-Recurrent.

Operation similar to Recurrent (IIIB) occurs whenever the pushbutton switch is depressed and continues as long as the switch is held down.

D. 162 on Manual-One Cycle.



Fig. 2-17. Two outputs are available. A positive-going gate occurs once each time the switch is depressed. It starts at the time the contacts close and endures for an interval which is determined by the settings on the panel controls. A negative-going sawtooth occurs once each time the switch is depressed. It starts at the time the contacts close and endures for an interval determined by the settings on the panel controls. The operation will not recur until the push-button switch is released and depressed once again.

#### IV. Combined unit operations

A. 1) Double pulse formation. Basic interval supplied by oscilloscope sweep.



Fig. 2-18. The timing of each pulse with reference to the sweep is controlled by the delay setting on the 161 panel. The dimensions of each pulse are determined by the pulse duration and amplitude controls.

A. 2) Double pulse formation. Basic interval supplied by 162.



Fig. 2-19. The interval at which all operations recycle is determined by the interval settings on the controls of the 162 operating recurrently. The timing of each pulse with reference to the sweep is determined by the delay settings on the dials of the 161's. The dimensions of each pulse are determined by the pulse duration and amplitude controls on the 161's.





Fig. 2-20. All operations recycle at interval determined by control pulse. Delays and dimensions of output pulses determined by control settings of 161's.

B.1) Multiple pulse formation. Basic interval supplied by external pulse. Repetitive pulse formation required during a fraction of sweep transit time.



Fig. 2-21. All operations recycle at interval determined by control pulse. This initiates sweep of oscilloscope and sawtooth input to 161A. At a given time, determined by the delay setting of 161A, a positivegoing gating pulse is initiated. The duration of the gate is determined by the duration settings of 161A. The 162 operates recurrently during a period determined by the gate from 161A. The frequency of operation of 162 is determined by the interval setting on the control panel of 162. The recurrent pulse output from 162 thus consists of a train of pulses of controlled time of initiation, controlled train duration and controlled repetition rate. The 161B produces a pulse output for each individual pulse in from the 162. The duration and amplitude controls the 161B permit control of the individual pulse dimensions in the train. B.2) Multiple pulse formation. Basic interval supplied by external pulse. Repetitive pulse formation required during a fraction of sweep transit time. Single pulse required at variable position with reference to sweep.



Fig. 2-22. 161A, 162 and 161B operate as described in Paragraph B2. 161 forms a single pulse at a time determined by its delay control setting having dimensions determined by its duration and intensity controls.



#### Туре 126

#### General

Rectifiers V118 and V120 are conventional full-wave rectifiers. Electrolytic capacitors C118 and C120 are used as filters.

#### -170-Volt Regulated Supply

The negative 170-volt supply is regulated by comparing the voltage of the reference tube, V105, with the voltage from a voltage divider connected between ground and the -170volt bus. The error signal is amplified in V110 and applied to the grid of V115. This amplified error signal changes the series resistance of V115 in the proper direction to correct the output voltage. A screwdriver adjustment, labeled -170 ADJUST, permits the voltage to be set correctly. The remaining two regulated supplies are referenced to the -170-volt bus.

#### +225-Volt Regulated Supply

The positive 225-volt supply is regulated by comparing with ground potential the voltage from a voltage divider connected between the +225-volt bus and the -170-volt bus. The error signal is amplified in V130B and applied to the grid of V125, the series regulator tube.

#### + 150-Volt Regulated Supply

A divider from the +225-volt supply to ground applies the proper voltage to the grid of V130A to obtain +150 volts at the cathode. Since very little current is required from this supply, no further regulation is used. SECTION 3

# CIRCUIT

#### **300-Volt Unregulated Supply**

The 300-volt output is obtained from the unregulated side of the 225-volt supply. This supply is used to supplement the 225-volt supply to provide the required current for the 160-Series instruments.

#### 6.3-Volt AC Unregulated Supply

This voltage is supplied from a 6.3-volt winding on the power transformer. Current from this winding should not exceed 4 amps.

#### Type 160

The Type 160 Power Supply has been replaced by the Type 160A, an improved design. Circuit information on the Type 160 is included here, however, for the benefit of customers having these instruments.

Rectifier tubes V1 and V2 are conventional 5V4 full wave rectifers. Electrolytic capacitor filters are used, consisting of C1, C2, C5 and C6.

#### -170-Voit Regulated Supply

The basic reference element is V5, a gas diode. The negative 170-volt supply is regulated by comparing the voltage of the reference tube, V5, with the voltage of a voltage divider connected between ground and the -170-volt bus. The error signal is amplified in V4, and applied to the grid of V3B, a series regulator triode. Current available is limited to 125 ma. A screwdriver adjustment R15A, labeled SET TO -170 V, in the voltage divider element, R15, A, B, and C, permits the voltage to be set accurately. The remaining two regulated supplies are referred to the -170-volt bus.

#### + 225-Volt Regulated Supply

The reference element is the -170-volt bus. The positive 225-volt supply is regulated by comparing to ground potential the voltage of a voltage divider connected between the +225volt bus and the -170-volt bus. The error signal is amplified in V6, and applied to the grid of V3A, a series regulator triode. Current available is limited to 125 ma. A screwdriver adjustment, R5A, labeled SET TO +225V, in the voltage divider network, R5A, B, and C, permits the voltage to be set correctly.

# 150-Volt Regulated Supply

The reference element is the -170-volt bus. The positive 150-volt supply is regulated by comparing to ground potential the voltage of a voltage divider connected between the -170-volt bus and the +150-volt bus. The error signal is amplified in V7A, and applied to the grid of V7B, the other half of the same dual triode, which acts as a series regulator tube. Output from this bus is limited by the current limitation of V7B, and the existing load on the +225-volt supply, because this current is supplied from the +225-volt regulator.

#### **300-Volt Unregulated Supply**

This output comes from the unregulated side of the series-regulator tube, V3A, and is used to supplement the 225-volt supply to provide the required current for six Type 161 or Type 162 generators. The use of the +300-volt source is not recommended for other purposes because of ac ripple. Current limitation is determined by the transformer secondary winding and the existing current through the +225volt supply. The total current in the plate lead of V3A should not exceed 175 ma.

# 6.3-Volt AC Unregulated Supply

This voltage is supplied from a 6.3-volt ungrounded winding on the power transformer. Filaments of all tubes in the three regulators are also supplied by this winding. Current available external to the supply is limited to 10 amps.

#### Type 160A

#### General

Rectifier tubes, V1, V30 and V31, are conventional fullwave rectifiers. Electrolytic capacitors, C1 and C30, are used as filters.

#### -170-Volt Regulated Supply

The negative 170-volt supply is regulated by comparing the voltage of the reference tube, V6, with the voltage from a voltage divider connected between ground and the -170-volt bus. The error signal is amplified in V7A, and is applied to the grids of V16 and V17 via the cathode follower, V7B. A screwdriver adjustment, R10, labeled ADJ. -170 v, permits the voltage to be set correctly. The remaining two regulated supplies are referred to the -170volt bus.

# + 225-Volt Regulated Supply

The positive 225-volt supply is regulated by comparing with ground potential the voltage from a voltage divider connected between the + 225volt bus and the -170-volt bus. The error signal is amplified in V33 and applied to the grids of V35, the series-regulator tube. Current available is limited to about 175 ma by the limitation of the series tube, but this tube can be shunted with a 1500-ohm resistor to increase the current capability to 225 ma. A screwdriver adjustment labeled ADJ. + 225 v permits the voltage to be set correctly.

#### +150-Volt Regulated Supply

The reference element is the -170-volt bus. The positive 150-volt supply is regulated by comparing to ground potential the voltage of a voltage divider connected between the -170-volt bus and the +150-volt bus. The error signal is amplified in V47A, and applied to the grid of V47B, the series-regulator tube. Output from this bus is limited by the current limitation of the series tube and the existing load on the +225-volt supply, because this current is supplied from the +225-volt regulator.

#### +300 Volt Unregulated Supply

This output comes from the unregulated side of the series-regulator tube, V35 and is used to supplement the 225-volt supply to provide the required current for the 160-Series instruments. The use of the +300-volt source is not recommended for other purposes because of ac ripple. Current limitation is determined by the transformer secondary winding and the existing current through the +225-volt supply. The total current from the plus-supply rectifiers should not exceed 250 ma.

# 6.3 Volt AC Unregulated Supply

This voltage is supplied from a 6.3-volt winding on the power transformer. Filaments of all tubes in the three regulators are also supplied by this winding. Current available external to the supply is limited to 20 amps.

# Туре 360

#### VERTICAL AMPLIFIER

#### Input Connection

Input is made to the vertical amplifier by way of the UHF connector labeled VERTICAL INPUT. Blocking capacitor C10 is shorted out in the DC position of SW9 and labeled AC-DC.

#### **Input Attenuators**

Frequency-compensated rc attenuators are switched into the amplifier input circuit by the VOLTS/DIV switch. Two attenuators are used singly or cascaded to produce four calibrated sensitivities.

#### **Phase Inversion Stage**

V30 and V32 comprise a cathode-coupled phase-inverter amplifier. Gain of the amplifier is adjustable by means of R34 which determines the amount of coupling between the cathodes. The front-panel screwdriver control labeled DC BAL adjusts the dc grid voltage of V32 so its cathode is at the same dc potential as the cathode of V30. When this control is properly set no change in vertical positioning will occur when the VARIABLE control is varied.

#### **Vertical** Positioning

Vertical positioning is produced by a dual potentiometer connected to the plates of the phase-inverting amplifier so the current through one plate load is increased when the potentiometer is adjusted to reduce the current through the other plate load.

#### Output Stage

V50 and V52 provide the additional gain required to bring the signal to the proper level for application to the crt vertical-deflection plates. The front-panel screwdriver adjust, R56, introduces variable degeneration between the cathodes permitting the gain to be set so the VOLTS/DIV setting will agree with the trace deflection when the VARIABLE gain control, R34, is turned full right to the CALIBRATED position.

#### Voltage-Setting CF

V72A provides a low-impedance source for the reduced plate and screen voltage required for the phase-inversion stage tubes, V30 and V32.

#### HORIZONTAL AMPLIFIER

#### Gain Set Stage

The sawtooth waveform is applied to the grid of V72B and taken from the plate for application to the horizontal-deflection plate. DC coupled inverse feedback from plate to grid reduces the gain of this stage to approximately unity. R77, the SWEEP CAL control, permits the feedback to be varied over a small range so the overall gain of the horizontal amplifier can be set so the sawtooth waveform will sweep the crt spot the proper distance.

#### Horizontal Positioning

The HORIZ. POSITIONING control, R71, allows the dc level of the input grid of V72B to be varied thus changing the average dc

level of the plates of V72B and V80 which positions the trace to the left or right.

#### Phase-Inversion Stage

V80 is a pentode amplifier with sufficient degenerative feedback from plate to grid to make the gain about equal to the gain of the first stage. The signal at the plate of V80 is out of phase with the signal at the grid and consequently out of phase with the signal applied to the crt pin-6 deflection plate so the single-ended input sawtooth is converted to a push-pull signal at the crt deflection plates.

#### HIGH-VOLTAGE SUPPLY

Accelerating voltages for the crt are obtained by rectifying a 60-kc high ac voltage produced by a vacuum-tube oscillator. V104 is the oscillator tube connected as a Hartley oscillator with the primary of transformer T100 as the tapped inductor, and C107 as the capacitor.

A half-wave rectifier, V116, supplies about 1500 volts negative to provide the focus and accelerating voltages to operate the crt.

#### High-Voltage Regulator

A portion of the rectified high voltage is tapped off at adjustable R132 and compared with the regulated -170 volt supply at V100A. Any error signal will be amplified and applied to the grid of V100B. The plate voltage of V100B determines the screen voltage of V104 and consequently the oscillator output. The feedback loop phasing is such that any change in the rectified high voltage will cause the oscillator output to change in the opposite direction thus cancelling variations in the high-voltage supply.

#### Unblanking

The crt control-grid voltage is supplied by a separate secondary winding and rectifier. The positive end of this supply is connected to the +GATE INPUT binding post and a signal at this binding post will drive the whole gridvoltage supply with it so the same signal appears at the crt control grid about 1600 volts below. Since this is a dc connection, the unblanking pulse can have any duration with no change in grid voltage. C116 transmits the leading edge of the unblanking pulse to reduce the unblanking time for fast sweeps.

# Type 161

The basic waveform generator of the TEK-TRONIX Type 161 Pulse Generator is a plateto-grid coupled monostable multivibrator, or "one-kick" multivibrator, coupled to the output terminals through suitable amplifiers, and triggered by means of a sharp negative pulse from a bistable multivibrator, or regenerative trigger amplifier.

#### **Block Diagram Description**

In the Block diagram, V1 is a double triode whose two sections operate as a pulse amplifier when the instrument is being triggered by pulses, and as a voltage comparator when the instrument is being triggered by a sawtooth voltage. The voltage comparator circuit compares the amplified sawtooth with an adjustable comparison voltage and initiates a pulse when the two are equal. This arrangement provides an adjustable delay between the start of the sawtooth and the start of the pulse. The input switch, SW1, labeled POS. PULSE, NEG. SAW-TOOTH, connects the input connector to the pulse amplifier in the POS. PULSE positions and rearranges the circuit into a voltage comparator in the NEG. SAWTOOTH positions.

The regenerative trigger amplifier, V2, produces a step of the same magnitude regardless of the size of the triggering pulse. The output step voltage of the trigger amplifier operates the monostable multivibrator consisting of V3B and V4A. The disconnect diode, V3A, couples the multivibrator to the trigger amplifier in the forward direction but prevents reaction of the multivibrator from affecting the trigger circuit.

Switch SW2, labeled PULSE WIDTH, selects any of four capacitors to vary pulse width.

The positive pulse amplifier, V4B, a cathode follower, provides positive output at the GATE OUT terminal and to the PULSE POLARITY switch SW3.

The negative pulse amplifier, V5 supplies negative output to the PULSE POLARITY switch SW3.

The PULSE AMPLITUDE potentiometer provides a continuous adjustment of the output pulse amplitude between 50 volts and zero.

# **Pulse Amplifier**

When the TRIGGER SELECTOR switch, SW1, is in the POS. PULSE position, the INPUT terminal is connected to the grid of V1B. Assuming that R9A, labeled POS TRIGGER BIAS, is set near 0.3 to give a bias voltage on V1B of about 80 volts, V1B will act as an amplifier to a positive pulse applied at the INPUT terminal, and a negative pulse will appear at its plate which is coupled to the grid of trigger amplifier, V2A. A 20-volt positive pulse into the INPUT terminals will produce a negative plate pulse of about 60 volts, which is transmitted through frequencycompensated divider, R10, R11, to the input grid of B section of V2.

# **Regenerative Trigger Amplifier**

The trigger amplifier is a bistable multivibrator which can be changed from complete cutoff of section A and full conduction of section B to the opposite condition of cutoff of section B and conduction of section A by a small input voltage variation of the order of 5 volts or less. The transition between one state and the other occurs very rapidly.

The circuit operation of the trigger circuit is briefly as follows: In the quiescent state, bias voltage at the grid of V2B is about 25 volts, slightly below cathode, so that some grid current flows and about 7 milliamperes of plate current flows. Bias voltage at the grid of A section of V2 is set well below cutoff by the voltage divider, R15, R16 connected between -170 volts and the plate of B section, which rests at about 75 volts because of plate current through R12.

When the B- section grid receives the negative spike of voltage from V1, its voltage begins to drop, and the plate voltage rises toward 225 volts. The plate of B section is connected to the grid of A section through a frequencycompensated voltage divider, R15, R16, so that the A-section grid has a corresponding rise. Simultaneously, the common cathode voltage drops, and the grid and cathode of A section approach each other, so that plate current begins to flow in A section.

The grid of section A continues rapidly in the positive direction until sufficient cathode current flows through R13 to cause the cathode to rise above the grid of section B, and plate current from section B is then cut off, but section A conducts. The corresponding drop in plate voltage of section A causes a negative pulse of voltage to appear, which is differentiated through C5 and R17 to form a suitable negative spike to trigger the one-kick multivibrator.

After the input pulse into V1 has terminated and the grid voltage of this tube has dropped below about 75 volts, the plate of V1 then rises toward + 225 volts carrying the grid of V2B with it, and the trigger circuit then returns to its quiescent state with the B section of V2 conducting while the grid of A section is biased well below cutoff. A positive pulse is generated at the plate of V2A at the instant of the transfer.

The negative spike out of the trigger tube, V2, is applied to the cathode of diode-connected V3A. In the quiescent state, V3B is cut off and the cathode and plate of V3A are therefore at the same voltage. A negative pulse at the cathode will thus be passed while a positive pulse will not. The unwanted positive pulse generated when the circuit returns to its quiescent state is therefore not applied to the onekick multivibrator.

When the TRIGGER SELECTOR switch, SW1, is set to the NEG. SAWTOOTH position, the Type 161 will respond to a negative sawtooth waveform of sufficient amplitude. For this type of operation, V1 operates in a voltagecomparator circuit with the two cathodes connected to a common resistor. The cathode voltage required for conduction of section B is determined by a voltage-divider potentiometer, R9A, labeled OUTPUT PULSE DELAY, connected between ground and positive 225 volts, which sets the grid bias of V1B. The sawtooth signal input into section A of this tube must be dc connected to permit the instrument to operate at the low-frequency limit given in the specifications, and must include an average dc component of about 80 volts.

At the start of the sawtooth input, V1A is conducting, and the cathode voltage follows within a few volts of the grid of V1A. When the cathode drops to a point within a few volts of the grid of section B, conduction begins in section B, causing a sudden drop in voltage at its plate and the resulting negative step triggers V2.

The calibration of potentiometer R9A is in terms of the fraction of the sawtooth waveform time duration at which triggering will result. The calibration is correctly set at the factory only for a negative-going sawtooth waveform, 130 volts peak to peak, between the limits of positive 150 volts and 20 volts. For waveforms not conforming to the foregoing, screwdriver adjustments R9B and R9C, labeled POS. DELAY LIMIT and NEG. DELAY LIMIT, must be readjusted to make the calibrations read correctly.

#### Monostable Multivibrator

The one-kick multivibrator consists of section B of V3 and section A of V4. A one-kick multivibrator can be changed from conduction in one tube and cutoff at the other tube to the opposite condition upon application of a triggering pulse. Thereafter it returns to the original state by itself after a period of time determined by the sizes of circuit parameters.

In the quiescent state before receipt of the triggering pulse from the previously-described trigger circuit, plate current flows in V4A, and V3B is cut off. The grid of V4A is connected to a positive voltage near 150 volts through R24 which is of the order of 1 megohm. Grid current flowing through this resistor prevents the grid from going far positive. Grid current of the order of magnitude of 0.1 milliamp holds the grid voltage about half a volt positive, with a resulting plate current of about 8 milliamps, and the plate voltage rests at about 50 volts.

The grid voltage of V3B is determined at about -60 volts by the voltage divider R19, R22, connected between -170 volts and the plate voltage of V4A, about 50 volts, so that plate current of V3B is cut off. A negative spike from the trigger circuit, coupled via one of the four timing capacitors, C6 to C9, depresses the grid of V4A to cutoff, resulting in a positive pulse of about 175 volts at the plate of V4A. The positive pulse is impressed on the grid of V3B through voltagedivider network R19, R22, causing plate current to flow momentarily until the timing capacitor charge is discharged through R24 and R25, and the grid of V4A rises sufficiently high to permit plate current to flow in V4A.

At the moment that plate current begins to flow in V4A, a negative step is generated at its plate which depresses the grid of V3B below cutoff and the multivibrator returns to its quiescent state. The length of the positive pulse out of V4B is determined by the size of the timing capacitor, the value of R24 plus R25, and the voltage into which the timing capacitor discharges, as determined by the setting of R26. The four timing capacitor values. C6 to C9, are in decade ratio to provide decade ratios of pulse widths, selectable by means of switch SW2, labeled PULSE WIDTH. R24, labeled PULSE WIDTH MULT., is variable and is fitted with an indicator dial calibrated from one to ten.

The resulting positive pulse from the plate of V4A is applied to the grid of output cathodefollower amplifier V4B by means of a frequencycompensated voltage divider, R30, R32, connected between the plate of V4A and minus 170 volts. During the quiescent state, V4B is biased well below cutoff at about 50 or 60 volts negative. The positive amplitude of the pulse applied to the grid of V4B is determined by the setting of R30, a screwdriver-adjustable potentiometer in the voltage-divider circuit, R30, R32. This level is adjusted at the factory so that the peak voltage at the GATE OUT terminal is 50 volts.

# Negative Pulse Amplifier

The positive pulse out of V4A is also applied to the grid of V5B through a frequency-compensated voltage divider consisting of R28 and R34. V5 is a dual triode with a common cathode resistor, R29, for both triode sections. In addition to receiving a positive signal on the grid of section B, V5 also receives a negative signal on the grid of section A, from the plate of V3B of the one-kick multivibrator. In the quiescent state, the grid of V5B is about 18 volts below the grid of V5A, and V5B therefore has no plate current flowing. The common cathode potential is therefore determined by the current flowing through section A at a level a fraction of a volt below the grid of section A. When a negative pulse is impressed on the grid of section A, plate current in section A drops, thereby dropping the cathode potential.

When a positive pulse simultaneously impressed on the grid of section B raises its voltage within about nine volts of the cathode potential, plate current flows in section B. Because of the plate current flowing in section B, the cathode potential fails to fall as fast as the grid potential of section A and soon section A ceases to conduct while section B conducts heavily. A negative pulse is therefore developed at the plate of section B. The amplitude of the negative pulse into the output of the potentiometer is determined by the setting of R29, the variable cathode resistor. The PULSE POLARITY switch, SW3, inserts R31, a potentiometer, as the cathode-load resistor of V4B for positive-pulse output, or inserts it as the plate-load resistor for V5B for negative-pulse output. In the negative-pulse output position, a second section of SW3 inserts R33, as a cathode-load resistor in V4B to retain the positive gate output when SW3 is in the negative-pulse position.

# Type 162

The TEKTRONIX Type 162 Waveform Generator was designed primarily as an interval timer and repetition rate generator. The basic circuit element is a phantastron run-down circuit with timing capacitance and resistance values variable by means of front-panel selector switches, and provided with associated triggering circuits and wave shaping and output amplifiers.

# Block Diagram Description

The OPERATING MODE switch shown at the left of the diagram is in three sections. The section shown is the input section SW1C which, in the two top positions, completes the circuit from either the +GATE IN or the +TRIGGER IN panel connectors to the regenerative trigger tube, V1. In the remaining three positions, SW1C grounds the grid of V1B, the input section of the regenerative trigger, so that its trigger action is not involved except in the top two positions of SW1C, labeled +GATE IN and +TRIGGER IN.

The regenerative trigger circuit, consisting of the two halves of V1, is a circuit which produces a large (80 volt) positive square-top voltage wave output for a small (8 volt) voltage change at its input. Upon receipt of a short voltage pulse, the trigger circuit produces a short output pulse. Upon receipt of a gating voltage, the output waveform remains positive until the input wave is removed.

The trigger amplifier, V2A, controls the operation of a multivibrator, V2B and V3A. Its grid and cathode circuits are switched by SW1A and SW1B switch sections in such a way as to cause it to produce either a short output pulse upon receipt of a grid signal, or to produce a gating signal for the duration of a signal input, depending upon the switch setting.

The multivibrator section, V2B and V3A, is triggered by a positive triggering voltage at the grid of V2A. The positive triggering voltage arises either by operation of the regenerative trigger, or by the grounding of the negative grid-bias source of V2A, depending upon the setting of the OPERATING MODE switch, SW1. The V3A half of the multivibrator gates the phantastron and permits it to run during the period of a positive pulse at V3A plate.

The phantastron section consists of V4, the pentode portion, V5B, a cathode-follower timingcapacitor recharged and V6B a diode-connected plate catcher, or plate-voltage limiter. The gating section of the multivibrator, V3A, during its period of plate-current conduction, holds the phantastron suppressor below the level that permits plate current conduction in the phantastron. During the period of the multivibrator cycle when V3A is not conducting, its plate voltage rises and carries the phantastron screen positive and the suppressor up to ground potential so as to initiate a phantastron rundown, and permit the phantastron to recycle continuously as long as this condition persists.

The length of time required for the phantastron to execute one rundown is determined by the discharging time of a timing capacitor and timing resistor. Switches SW3, labeled MULTI-PLIER, and SW5, labeled WAVEFORM DUR-ATION, select various values of timing capacitors and resistors to permit selection of the rundown time.

The panel connection labeled SAWTOOTH OUT, connects directly to cathode-follower V5B cathode to provide approximately a 1000-ohm output impedance. V5B thus serves the dual purpose of output tube and timing capacitor recharger.

Pulse and gate shaper, V3B, receives its input signal from the gating section of the multivibrator, V3A, which remains positive during the phantastron rundown. Toggle switch SW4, labeled PULSE OUT, GATE OUT, inserts either frequency-compensated dc coupling or differentiated ac coupling between the shaping amplifier and the output amplifier. In the GATE OUT position of SW4, dc coupling results.

In the output amplifier and cathode follower section, consisting of V5A, and V6A, the gate or pulse signal is amplified and limited, and the signal is produced across the cathode resistor of V6A at an impedance of about 1000 ohms. Cathode follower V6A is biased below cutoff before receiving a signal so that the output signal begins at ground potential and increases in the positive direction.

#### Phantastron

In the quiescent state, the suppressor of V4 is held below plate-current cutoff at -40 volts by voltage divider R14, R15, connected between +40 volts at the plate of V3A and -170 volts. and V4 plate rests at +150 volts. The grid of V4 is connected to a positive voltage source through the variable timing resistance, R20, a high resistance of several megohms, so that grid current flowing in this resistor prevents the grid voltage from going more than a fraction of a volt positive. One end of timing capacitor C3 is connected to the grid of V4 and the potential of this end is therefore held at approximately ground voltage. The other end of timing capacitor C3 is connected to the cathode of cathode follower V5B whose grid is connected to the plate of V4, at +150 volts. The cathode

of a cathode follower adjusts its voltage by means of cathode resistor current to follow very close to the grid voltage. The cathode is therefore at positive 150 volts, and timing capacitor C3 is thus charged to 150 volts.

When a positive gating pulse is applied to the screen of V4 the suppressor rises to ground potential from -40 volts, plate current begins to flow in V4, and its plate voltage drops, carrying with it the grid and cathode of V5B. The grid voltage of V4 therefore drops momentarily because the low potential end of C3 is 150 volts below the cathode of V5B at the first instant, and C3 begins to discharge through R20. The rate of the discharge through R20 determines the voltage of the grid of V4, which in turn determines the plate voltage of V4. The sum of the cathode voltage of V5B and the voltage of the charge remaining on C3 must always be near but slightly lower than ground potential because the grid of V4 must be above plate current cutoff but below grid-current conduction. If, for example, the voltage at the cathode of V5B were momentarily to become too high with respect to charge voltage remaining on C3, the grid voltage of V4 would also rise. thus lowering V4 plate voltage and thereby the cathode voltage of V5B.

The discharge current from C3, flowing through R20, determines the grid voltage of V4. A change in voltage drop through R20. resulting from a change in discharge current from C3, will therefore be followed by a change in voltage at the cathode of V5B in the correct direction to oppose such a change in grid voltage of V4. For example, if C3 were simply to discharge through a resistor, the discharge current would fall off exponentially. However, the falling off of discharge current results in a decreasing drop in R20 and causes the grid of V4 to rise. Its plate then falls, dropping the voltage of the right end of C3 the required amount to increase the discharge current. and thus tends to maintain it at a constant value. With a constant discharge current flowing from timing capacitor C3, the voltage across C3 falls off linearly. Since the sum of the cathode voltage plus the voltage across C3 must remain near zero, it follows that the cathode voltage must also fall linearly.

When C3 is nearly discharged and the plate of V4 nears cathode potential, the cathode current, which has been flowing largely through the plate, suddenly transfers to the screen, the screen voltage drops, carrying the suppressor with it, and thereby completely cuts off plate current from V4.

When plate current of V4 is cut off, the plate voltage of V4 rises immediately to plus 150 volts, carrying the grid, and eventually the cathode, of V5B with it. The grid of V4 is again held near ground potential by grid current and C3 charges rapidly to 150 volts through the low plate-to-cathode impedance of V5B. During the recharge period, the screen voltage drops as the result of screen current, carrying the suppressor with it by means of R14, so that plate current is further held off.

As the timing capacitor charges, the plate voltage of V4 increases until eventually it reaches a value such that the reduced suppressor voltage no longer prevents plate current from flowing. At this instant, cathode current begins to transfer from the screen to the plate. and the screen voltage rises carrying the suppressor with it, which further increases the plate current. The plate voltage then drops. C3 begins to discharge, and the rundown action starts again. However, if V3A is conducting, the suppressor of V4 is held below cutoff when the plate of V4 reaches full 150-volt plate voltage and the phantastron therefore returns to its quiescent state at the finish of one rundown.

#### **Gating Multivibrator**

The gating function is performed by V3A. which, with V2B, forms an Eccles-Jordan multivibrator connected so that in the quiescent state V3A is conducting and the screen and suppressor voltages of the phantastron tube V4 are reduced below the point of plate current cutoff. To permit V4 to start its rundown action, the multivibrator must be in the opposite state with V3A not conducting and V2B conducting. In the quiescent state, voltage at the grid of V3A is limited to a fraction of a volt positive and V3A conducts. A negative pulse at the plate of V2B will momentarily drive the grid of V3A negative below cutoff through R17 and the plate of V3A will rise rapidly. carrying the screen and suppressor of phantastron V4 with it, thereby initiating the phantastron rundown action.

At the termination of the rundown period, a sudden drop in screen voltage of phantastron, V4, drives the grid of V2B down, a positive step results at the plate of V2B which raises the grid of V3A into the conducting region again, and the screen and suppressor voltages of V4 are lowered below the point of plate current conduction so that the quiescent state is resumed.

# Trigger Amplifier

The grid of trigger amplifier V2A is connected to the arm of OPERATING MODE switch section SW1A. In the GATED or TRIGGERED positions of this switch, the instrument is prepared to receive external trigger pulses. In the quiescent state before receipt of a pulse, the grid of V2A is held below plate current cutoff at -20 volts, by low plate voltage of V1A, and V2B grid is held below cutoff by low plate voltage at V3A.

Upon receipt of a large positive step of voltage at its grid, V2A begins to conduct and a negative step appears at its plate.

In the GATED position, the cathode of V2A is grounded, its grid is limited to a fraction of a volt positive by grid current through R10, and the plate of V2A drops about 200 volts because of plate current of about 4 milliamperes, and carries the grid of V3A well below plate current cutoff. The plate of V3A therefore rises and permits the phantastron action to commence.

When the OPERATING MODE switch, SW1, is in the TRIGGERED position, the cathode of V2A is returned to ground through R30 and C6, a parallel differentiating network with a time constant sufficiently short that V3A is held off from conduction only long enough to start one phantastron rundown for each positive impulse received.

When the OPERATING MODE switch, SW1, is in the RECURRENT position, the grid of V1B is grounded and the grid and cathode of V2A are grounded so that V3A is held off from conduction as long as the switch remains in this position. The phantastron will operate recurrently, therefore. When the OPERATING MODE switch, SW1, is in the MAN CONT position, the grid of V1B and cathode of V2A are grounded. The grid of V2A is held below plate current cutoff by voltage divider R9, R10, and R11. Pushbutton SW2, labeled MANUAL, when depressed, raises the grid-to-ground potential and causes plate current to flow, thereby raising the plate of V3A. The phantastron therefore runs recurrently as long as the pushbutton remains depressed.

When the OPERATING MODE switch, SW1, is in the MAN, ONE CYCLE position, V1B grid is grounded and the cathode of V2A is returned to ground through parallel differentiating network, R32, C6, whose time constant is shorter than the rundown time of the phantastron. The phantastron therefore executes only a single rundown each time the pushbutton is depressed.

# **Regenerative Trigger**

When the OPERATING MODE switch, SW1, is in either the GATED or TRIGGERED positions, the grid of V1B is connected to receive external voltage pulses through the appropriate panel connectors, labeled + GATE IN and + TRIGGER IN.

In the quiescent state the grid of V1A rests at about 17 volts. Under these conditions about 6 milliamps of plate current flows in V1A, resulting in a cathode voltage of about 20.5 volts, and a plate voltage of about 135 volts. The center point of voltage divider R10, R11 connected between V1A plate and -170 volts is therefore about -20 volts in the quiescent state.

The cathode of V1A and V1B are tied together so that V1B also has a cathode bias of  $\pm 20.5$ volts. The grid of V1B is returned to ground through R4 and plate current flowing in V1B is about one-tenth milliampere.

A positive step of voltage arriving at the grid of V1B causes V1B plate to drop, carrying the grid of V1A with it through network, C10, R6, thereby reducing the cathode current of V1A. This causes the common cathode voltage of V1A and V1B to drop, further increasing the grid-to-cathode voltage of V1B so that the action is regenerative. The plate of V1A rises rapidly toward + 225 volts with a positive

step at this point of 80 volts or so, as the plate current in this section reduces almost to zero.

The center point of voltage divider R10, R11, which has been about 20 volts negative, is therefore driven positive about 40 volts to +20 volts, carrying with it the grid of V2A, the trigger amplifier tube.

When the OPERATING MODE switch is in the GATED position, the +GATE input terminal is directly connected to the grid of V1B so that a positive gate signal applied to the terminal raises the grid voltage and holds it during the time the gate signal persists. When the OPERATING MODE switch is in the TRIGGERED position, however, a step voltage applied to the +TRIGGER terminal is ac coupled through C2 and R4, so that V1B grid will return to ground potential after C2 is charged, and the regenerative trigger circuit will return to its quiescent state.

# Pulse and Gate Shaper and Output Amplifier

The gate and pulse waveform shaper, V3B, is followed by a two-stage amplifier and cathodefollower combination, consisting of V3B, V5A, and V6A. The grid of V3B is connected via R14, R15, to the plate of V3A, the gating section of the multivibrator, and hence is driven from -40 volts to zero bias each time rundown occurs. This results in a negative squarewave of output from the plate of V3B. When the toggle switch, SW4, is in the GATE OUT position, an over-compensated negative pulse appears at the grid of V5A. This results in cut off of V5A during the phantastron rundown, and a positive squarewave is therefore produced at its plate. The plate of V5A is directly coupled to the grid of cathode follower. V6A. which, in its quiescent state, is cut off, so that a positive gate results, starting at ground potential and going positive approximately 50 or 60 volts. When the toggle switch, SW4, is in the PULSE OUT position, the coupling capacitor, C3A-F, acts as a differentiating capacitor. This produces a negative spike on the grid of V5A and results in a rather narrow positive pulse at the plate of V5A. The amplitude of the pulse is the same as that of the gate but the pulse is considerably narrower. The differentiating capacitor C3A-F. is switched with the sweep-timing capacitor.
C3B-G, so that the pulse width is a function of the pulse interval. This provision helps to keep the pulses more readily visible at the lower repetition rates when they are displayed on an oscilloscope.

#### Type 163

The basic waveform generator of the TEK-TRONIX Type 163 Pulse Generator is a monostable, or "one kick" multivibrator, triggered by sharp pulses from a regenerative trigger amplifier. A voltage-comparator circuit permits triggers to be generated at any point on an input sawtooth voltage to provide adjustable delay. An output cathode follower provides low output impedance.

#### **Block Diagram**

The Block Diagram shows the INPUT switch in the position to accept sawtooth triggering pulses.

The sawtooth-comparator circuit compares the input sawtooth with an adjustable comparison voltage, and initiates a voltage step when the two are equal.

The output step voltage from the comparator is formed into a sharp trigger of the desired amplitude regardless of the size or slope of the triggering pulse by means of the regenerative trigger amplifier. The regenerated negative pulse is coupled through the disconnect diode to the plate of the multivibrator.

The negative pulse into the multivibrator causes it to flop from its stable state to its unstable state. The period of time the multivibrator remains in its unstable state determines the width of the output pulse. This period depends on the size of the switched capacitor and the size of variable resistors through which the capacitor discharges.

The charging diode speeds the transition period of the multivibrator back to the stable state at the conclusion of the unstable period.

The cathode follower reduces the output impedance to reduce effects of the external load characteristics on the pulse shape. When the INPUT selector switch is in the POSITIVE PULSE position, the operation is the same in all circuits except the input tube, which in this switch position becomes a simple amplifier.

#### Input Selector Switch

The input selector switch, SW10, connects the grid of V10B to the INPUT terminal in NEG. SAWTOOTH position, and in the POS. PULSE position connects the grid of V10A to the INPUT terminal through a capacitor, while connecting the unused grid of V10B to a positive voltage on voltage divider R10, R11, connected between +225 volts and -170 volts.

#### Sawtooth Comparator

The grid voltage of V10A is determined by the setting of R21, which is part of a voltage divider consisting of R20, R21, and R22. When the required sawtooth voltage at the grid of V10B is above this voltage, the common cathode voltage closely follows V10B grid as it drops and is more positive than V10A grid, so that V10A is cut off. When the common cathode voltage approaches V10A grid, current suddenly begins to flow in V10A and a negative voltage step appears at V10A plate. Between its two voltage limits, potentiometer R21 can change the bias by more than 100 volts, and can therefore cause the voltage step to occur at any point of the sawtooth within this range.

## **Regenerative Trigger Amplifier**

The negative step is transmitted to the grid of V11B through frequency-compensated voltage divider C23, R23, to the grid of V11B. C23 is the compensating capacitor which transmits the higher frequency components of the negative step voltage.

V11 is a bistable regenerative trigger amplifier. In the quiescent state before receipt of the negative step voltage V11B is conducting and V11A is cut off because the common cathode connection is at a higher voltage than the grid of V11A. When the negative step arrives at the grid of V11B the common cathode voltage drops while V11B plate rises, and the grid of V11A, which rises with the plate of V11B, approaches the falling cathode until conduction occurs in V11A. As soon as conduction does occur in V11A a rapid transition takes place, with the current transferring from the B section to the A section, and the attendant rise of B-section plate drives the A-section grid farther positive.

A second stable state is reached when V11B no longer conducts at all and the A-section plate remains down. This new stable state continues as long as the plate of V10A is down low enough to hold off plate current from V11B, regardless of how much farther it falls below this point. The change in plate voltage of V11A is thus determined only by the circuit constants of V11A, and a uniform negative step voltage is obtained regardless of the size or speed of the triggering voltage.

#### **Multivibrator**

V13 and V14 comprise a monostable multivibrator. In the stable state V14 is conducting with its grid at ground voltage and its cathode slightly above ground. The grid of V13 is held somewhat negative by the setting of potentiometer R42.

The negative pulse from regenerative pulse amplifier V11 coupled through disconnect diode V12A to the plate of the multivibrator forces the plate of V13 and grid of V14 in the negative directions. As the grid of V14 drops, the common-cathode voltage drops below the grid voltage of V13, thereby causing plate current to flow and further reducing V13 plate. Since the reduction of current in V14 and increase in current in V13 is regenerative, the transition takes place very rapidly.

In the quiescent state, one end of C54 is at ground potential since there is no current flowing through R50 and R51. The other end of C54 is at +225 volts since there is no current flowing in R40, and there is thus a 225-volt charge on C54.

When the multivibrator is triggered, the plate of V13 drops so that the end of C54 formerly grounded is driven negative. This carries the grid of V14 with it past cutoff to well below ground, and C54 begins to discharge through R50 and R51. The length of time required for this end of C54 to rise to ground potential depends on the size of R50 and R51, through which the discharge current flows, and on the size of C54. R51 is adjustable by means of a front-panel control labeled PULSE WIDTH MUL-TIPLIER, and C54 is one of four switched capacitors, C50-C51, C52, C53 and C54, so that the discharge time can be adjusted over a 10,000-to-1 range by selecting capacitors and adjusting the resistor.

As soon as the selected capacitor has discharged until the grid of V14 is again near its cathode, current again flows in V14, the cathode rises because of increased cathode current, the plate of V13 rises carrying V14 grid with it and further increasing current through V14 until the original stable state is resumed with V13 cut off.

In the stable state while V14 is conducting its plate rests in the vicinity of +140 volts because of plate current flowing through R48. During the period while V14 is cut off its plate rises to +225 volts and therefore a squaretopped positive pulse of about 85 volts peakto-peak amplitude is produced.

#### **Output Cathode Follower**

The positive pulse is dc coupled to the grid of output cathode-follower V15 through compensated voltage-divider R62, R63 which is returned to an adjustable negative voltage. This divider places the grid of V15 below cutoff during the stable period of multivibrator V14, and raises it into conduction when V14 plate rises during cutoff to +225 volts. The amount of voltage division is designed by selection of R62 and R63 to place the grid of V15 near 25 volts positive when V14 plate is cut off. The voltage to which the negative end of the voltage divider is returned can be adjusted by means of R61. labeled PULSE AMP CAL so that the peak of the output pulse at the cathode of V15 is 25 volts positive. The output impedance at the gate terminal is approximately 100 ohms and the output impedance at the pulse terminal varies between about 500 ohms and zero, depending on the PULSE AMPLITUDE potentiometer setting. The maximum impedance occurs at about the 13-volt setting.

#### Disconnect Diode

V12A, the disconnect diode between the regenerative trigger amplifier and the multivibrator is provided to disconnect the multivibrator from the trigger amplifier after the multivibrator has been triggered to its unstable state, so that subsequent trigger signals will not affect the multivibrator until it has again reverted to its stable state. In the stable state when the plate of both V11A and V13 are cut off and rest at +225 volts, a negative pulse at the cathode of the disconnect diode will tend to pull the plate down with it, and thus transmit the pulse to the multivibrator. After the multivibrator is triggered the plate of V13 drops well below the plate of V11A and trigger-size variations of V12A cathode have no effect on V12A plate.

#### Charging Diode

Charging diode V12B from the grid of multi-

vibrator V14 to ground provides a low-resistance charging path to ground for C53, so that V13 plate can rise more rapidly when the multivibrator returns to its stable state.

#### Power Connector

The octal plug and socket shown on the upper left of the circuit diagram consist of male and female chassis-mounted connectors to fit the interunit cables supplied with the instrument to connect the Type 163 to a Type 160A Power Supply. The female connector permits additional Type 161, Type 162 or Type 163 units to be operated from the same Type 160 Power Supply. R6 in the wiring between power connectors connects the unregulated 300 volts to the regulated 225-volt bus to increase the available current for the Type 163.

# SECTION 4



# MAINTENANCE

#### Standard Components

Tektronix will supply replacement components at current net prices. However, since most of the components are standard electronic and radio parts you can probably obtain them locally faster than they can be shipped from the Tektronix factory at Beaverton, Oregon. Before ordering replacement parts be sure to consult the instruction manual to see what tolerances are required.

#### Selected Components

We specially select some of the components whose values must fall within prescribed limits, by sorting through our regular stocks. The components so selected will have standard RETMA color coding showing the value and tolerance of the stock they were selected from, but they will not in general be replaceable from dealer's stocks.

#### **Checked Tubes**

To obtain maximum reliability and performance we check some of the vacuum tubes in our instruments for such characteristics as microphonics, balance, transconductance, etc. We age other tubes to stabilize their characteristics. Since there are no well defined standards of tube performance we have established our own arbitrary standards and have developed equipment to do this checking. These checked tubes can be purchased through our local Field Engineering Offices or directly from the factory in Beaverton, Oregon.

#### HOW TO ORDER PARTS

Replacement parts may be purchased at current net prices from your local Tektronix Field Office or from the factory. Most of the parts can be obtained locally. All of the structural parts, and those parts noted in the parts list "Manufactured by Tektronix", should be ordered from Tektronix.

When ordering from Tektronix include a complete description of the part, and its 6-digit part number. Give the type, serial number, and modification number (if any) of the instrument for which it is ordered.

Structural parts are not listed in the parts list. Their part numbers are usually stamped directly on the metal. If not, a complete physical description of the part will suffice.

If the part which you have ordered has been replaced by a new or improved part, the new part will be shipped instead. Tektronix Field Engineers are informed of such changes. Where necessary replacement information comes with new parts.

#### NOTE

Always include the instrument TYPE and SERIAL NUMBER in any correspondence concerning this instrument.

#### GENERAL INFORMATION

#### **Color Coding**

We use color-coded wires in the instruments to help identify the various circuits. These wires will be either a solid color or will be a solid color (including black and white) with one or more colored stripes. The colored stripes are "read" in the same manner as the RETMA resistor color code. In the case of multiple stripes the wide stripe is read first.

Wires carrying positive regulated-powersupply voltages are white and the stripes indicate the supply voltage. For example, the +225-volt supply bus will be coded red-redbrown (2-2-1) giving two significant figures and the decimal multiplier.

The negative-supply bus wires are black and the stripes indicate the supply voltage. For example, the negative-supply voltage is -170-volt and is carried by a black wire coded brown-violet-brown (1-7-1).

The main-voltage leads to the power transformer are yellow and coded brown-brown-brown (1-1-1).

The tube heater leads are white and coded 6-1, 6-2, 6-3, etc., not to indicate that the voltages are different but to differentiate between circuits.

In other respects the color coding will vary from instrument to instrument. In general all signal-carrying leads are white and coded with a single colored stripe. In a few places where the number of leads exceeded the capabilities of single-stripe coding we have used solid-color leads.

## SOLDERING AND CERAMIC STRIPS

Many of the components in your Tektronix instrument are mounted on ceramic terminal strips. The notches in these strips are lined with a silver alloy. Repeated use of excessive heat, or use of ordinary tin-lead solder will break down the silver-to-ceramic bond. Occaasional use of tin-lead solder will not break the bond if excessive heat is not applied.

If you are responsible for the maintenance of a large number of Tektronix instruments, or if you contemplate frequent parts changes, we recommend that you keep on hand a stock of solder containing about 3% silver. This type of solder is used frequently in printed circuitry and should be readily available from radio-supply houses. If you prefer, you can order the solder directly from Tektronix in one-pound rolls. Order by Tektronix part number 251-514.



Fig. 4-1. Soldering iron tip correctly shaped and tinned.

Because of the shape of the terminals on the ceramic strips it is advisable to use a wedge-shaped tip on your soldering iron when you are installing or removing parts from the strips. Fig. 4-1 will show you the correct shape for the tip of the soldering iron. Be sure and file smooth all surfaces of the iron which will be tinned. This prevents solder from building up on rough spots where it will quickly oxidize.

When removing or replacing components mounted on the ceramic strips you will find that satisfactory results are obtained if you proceed in the manner outlined below.

1. Use a soldering iron of about 75-watt rating.

2. Prepare the tip of the iron as shown in Fig. 4-1.

3. Tin only the first 1/16 to 1/8 inch of the tip. For soldering to ceramic terminal strips, tin the iron with solder containing about 3% silver.



Fig. 4-2. Method of applying heat to ceramic strip.

4. Apply one corner of the tip to the notch where you wish to solder (see Fig. 4-2).

5. Apply only enough heat to make the solder flow freely.



Fig. 4-3. Note the slight fillet formed on a correctly soldered joint.

6. Do not attempt to fill the notch on the strip with solder; instead, apply only enough solder to cover the wires adequately, and to form a slight fillet on the wire as shown in Fig. 4-3.



Fig. 4-4. Soldering to a metal pin.

In soldering to metal terminals (for example, pins on a tube socket) a slightly different technique should be employed. Prepare the iron as outlined above, but tin with ordinary tin-lead solder. Apply the iron to the part to be soldered as shown in Fig. 4-4. Use only enough heat to allow the solder to flow freely along the wire so that a slight fillet will be formed as shown in Fig. 4-3.

#### **General Soldering Considerations**

When replacing wires in terminal slots clip the ends neatly as close to the solder joint as possible. In clipping the ends of wires take care the end removed does not fly across the room as it is clipped.



Fig. 4-5. A wooden dowel shaped for use as a soldering aid.

Occasionally you will wish to hold a bare wire in place as it is being soldered. A handy device for this purpose is a short length of wooden dowel, with one end shaped as shown in Fig. 4-5. In soldering to terminal pins mounted in plastic rods it is necessary to use some form of "heat sink" to avoid melting the plastic. A pair of long-nosed pliers (see Fig. 4-6) makes a convenient tool for this purpose.



Fig. 4-6. Long-nosed pliers used as a heat sink.

#### **Ceramic Strips**

Two distinct types of ceramic strips have been used in Tektronix instruments. The earlier type mounted on the chassis by means of #4-40 bolts and nuts. The later type is mounted with snap-in, plastic fittings. Both styles are shown in Fig. 4-7.

To replace ceramic strips which bolt to the chassis, screw a 2-56 nut onto each mounting bolt, positioning the nut so that the distance between the bottom of the nut and the bottom



Fig. 4-7. Old and new styles of ceramic strips. The newer ceramic strips mount in nylon collars.

of the ceramic strip equals the height at which you wish to mount the strip above the chassis. Secure the nuts to the bolts with a drop of red glyptal. Insert the bolts through the holes in the chassis where the original strip was mounted, placing a 2 star lockwasher between each nut and the chassis. Place a second set of 2 flat washers on the protruding ends of the bolts, and fasten them firmly with another set of 2-56 nuts. Place a drop of red glyptal over each of the second set of nuts after fastening.

#### **Mounting Later Ceramic Strips**

To replace ceramic strips which mount with snap-in plastic fittings, first remove the original fittings from the chassis. Assemble the mounting post on the ceramic strip. Insert the nylon collar into the mounting holes in the chassis. Carefully force the mounting posts into the nylon collars. Snip off the portion of the mounting post which protrudes below the nylon collar on the reverse side of the chassis.

#### NOTE

Considerable force may be necessary to push the mounting rods into the nylon collars. Be sure that you apply this force to that area of the ceramic strip directly above the mounting rods.

#### TROUBLESHOOTING

The 160-Series instruments are relatively troublefree. You should not experience much need for extensive troubleshooting. In troubleshooting, however, you should remember that these are complex electronic instruments, and there is no easy way to locate trouble. A thorough understanding of circuit operation is the best aid in troubleshooting.

The first step in troubleshooting the 160-Series instruments should be to deterine whether the input voltages at the octal power socket are correct. Refer to the schematic diagram for the instrument to determine the connections. If the voltages are incorrect remove the plug from the power socket to determine whether the trouble is in the power supply or in the Pulse Generator unit. If the trouble appears to be in the Pulse Generator look for evidence of overheated components. If no burned or blackened parts are in evidence try replacing all the tubes at once with new tubes. If replacement of all the tubes cures the trouble, you can then return the original tubes to their sockets one at a time until the defective tube is located.

Failure of the instrument to operate correctly will probably be due to tube deterioration than from component failure. The pulse generator circuits are relatively insensitive to minor tube variations, but relatively more sensitive to power-supply voltages.

#### CALIBRATION EQUIPMENT

In calibrating the 160-Series instruments two auxiliary generators are required: a Type 105 Square-Wave Generator and a Type 180A or Type 181 Time-Mark Generator. The pertinent specifications for these two instruments are listed below.

Type 105:

Risetime: Less than 0.02  $\mu$ sec into a terminated 93-ohm cable.

Frequency Range: 25 cycles to 1 mc, continuously variable. Maximum Output: 15 v, approximately into a terminated 93-ohm cable.

Type 180A: or Type 181:

Time-Marks: 1, 10, 100, 1000, and 10,000 microseconds.

Marker Amplitude: minimum 2 volts.

#### **Trouble Shooting**

#### Type 126

Tube failure will be the principal cause of trouble involving high or low voltage, lack of regulation or absence of any voltage. Low emission in the rectifiers or series tubes may cause the supplies to dropout of regulation. Since the other supplies are referenced to the -170-volt bus, check this supply first. Remove or measure all external loads to determine whether the trouble lies elsewhere.

If there is no voltage at any terminal, check the source of power and check the fuse. If a replacement fuse should blow look for shorted tubes. Try replacing the rectifiers and the series regulators. If this clears the trouble, the offending tube can be found by replacing the old tubes one at a time. If tube replacement does not clear the trouble, lift the leads of the electrolytics, C118 and C120. If this clears the trouble, the shorted capacitor can be found by replacing the leads one at a time.



Fig. 4-8. Bottom view of the Type 126 power supply.

#### Adjustment

The only adjustment necessary in the power supply is the adjustment of the -170-volt supply. R117, labeled -170 ADJ, accessible from the

left side of the instrument near the back adjusts this supply. No other adjustments are provided. If the other regulated voltages are incorrect after the negative supply is set, check for weak tubes or defective resistors in the voltage dividers.



Fig. 4-9. Type 126, Top view.

#### Type 160

#### Maintenance

The following may help in determining the cause of equipment trouble. All components are conservatively loaded and the minimum of trouble should be expected. Tube failure will be the principal cause of trouble involving high or low voltage, or absence of any voltage. Low emission in either V2 or V3B may reduce the voltage below ground at the -170-volt bus. This will increase the voltage of both the  $\pm 225$ -volt and  $\pm 150$ -volt supplies. Low emission of V1 or V3A may lower both these voltages. Remove all external loads from the power supply to determine whether the trouble lies elsewhere.

In case of absence of voltage at all terminals, check whether the power cord is firmly seated and check the 3-amp fuse mounted on the lower part of the front panel. A simple method of checking the fuse is to replace it with a good one. If a replacement fuse should blow look for shorted tubes by replacing them all. If this procedure clears the trouble, the offending tube can be found by replacing the old tubes one at a time. If tube replacement does not clear the trouble, lift the ungrounded lead of each of the four capacitors, C1, C2, C5 and C6. If this clears the trouble, the offending capacitor can be determined by replacing the leads one at a time.

#### Adjustment

If readjustment of the regulated voltages is required, the negative 170-volt supply should be checked and adjusted first because this bus is used as the reference for both the +225- and +150-volt supplies. R15A, labeled ADJ TO -170V, located on the top of the chassis to the rear, a screwdriver adjustment. controls the -170-volt bus. R5A, labeled ADJ. TO +225V, also located on the top of the chassis to the rear, controls the +225-volt bus. No adjustment for the 150-volt bus is provided. If this voltage departs far from 150 volts because of deterioration of circuit elements and other voltages are normal, it may be necessary to replace the resistors in the voltagedetermining network to return the voltage to normal. Voltage divider R9, R10 which determines the bias voltage of V7A is the voltagedetermining network.



Fig. 4-10. Bottom view of the Type 160 showing the location of the adjustment points.

#### **Type 360**

Before going thru the calibration procedure be sure the other instruments used with the indicator are operating normally--especially the power supply. A quick check of the powersupply voltages to see that they are within specifications might save much time as these voltages affect the calibration of the entire instrument. Remove the case from the instrument and plug it and the Type 162 into the power supply. Turn the instruments on and allow them to operate for about five minutes until the initial warm-up drift has ceased.

#### General

The following outline is based on the procedure used in our test department here at the factory.

Some of the adjustments require the use of a square-wave generator and a time-mark generator. Almost any accurate frequency generator can be used in place of a time-mark generator, however, the use of the square-wave generator is almost mandatory. If you do not have a square-wave or pulse generator with a rise-time of 1 microsecond or less do not attempt to adjust the vertical attenuators. This adjustment is quite stable and should not vary appreciably from its original adjustment.

#### Sweep Timing

There are two adjustments that will affect the sweep timing. Varying the crt accelerating voltage will change the deflection plate sensitivities and have a large effect on the length of the horizontal display. The SWEEP CAL. control on the front panel changes the gain of the horizontal amplifier and has a lesser effect on the horizontal display. Change the crt high voltage to make a coarse adjustment and use the SWEEP CAL. control for a final fine adjustment.

1. Set the 162 for a 1-msec sawtooth which is 100  $\mu$ sec per division on the 360 graticule. Connect the 100- $\mu$ sec output of a Type 180A or 181 Time-Mark Generator to the 360 VER-TICAL INPUT and trigger the 162 from the 180A trigger output or the 181 1000- $\mu$ sec output.

2. Center the 360 SWEEP CAL control and adjust the high voltage so the timing marks very nearly coincide with the graticule lines over the center 8 divisions of the graticule. The HV ADJ control can be reached with a screwdriver through a cutout in the shield at the lower left side and to the rear of the instrument.



Fig. 4-11. Side view of the Type 360 Indicator Unit.

AA<sub>1</sub>

3. Use the SWEEP CAL control to make any final fine adjustment to achieve the best coincidence between the graticule lines and the timing marks.

#### VERTICAL AMPLIFIER

There are three adjustments to be made to the vertical amplifier. First, to standardize the gain so that volts of vertical deflection can be read directly from the ruled graticule. Second, the input stage variable attenuator should be balanced for dc so the trace does not shift position vertically as attenuation is increased or decreased. And, third, the step attenuators should be compensated so that the attenuation is constant for any frequency within the passband of the instrument.

#### Vertical Gain Adjust

You will need a signal of known amplitude to calibrate the gain of the vertical amplifier. The calibrator signal from any Tektronix oscilloscope or from other voltage calibrators is a possible source of such a signal. Or, since the amplifier is dc coupled, you can use an accurately known dc voltage or a dc voltage and an accurate voltmeter.

1. Depending on the method used set the VOLTS/DIV switch to the position that will result in a close-to-full-scale deflection when the calibrating signal is applied. Check to see that the VARIABLE control is turned full right to the CALIBRATED position and if a dc voltage will be used for calibration the AC-DC switch must be in the DC position.

2. Apply the calibrating signal and adjust the VERT GAIN ADJ control so the deflection read from the ruled graticule agrees with the known amplitude of the calibrating signal.

#### DC Balance

4 - 8

The vertical amplifier VARIABLE gain control is located between the cathodes of the first stage and any difference in dc level between these two cathodes will cause the trace to shift vertically as the VARIABLE control is rotated. The DC BAL control permits the dc level of one of the cathodes to be adjusted to match the other. 1. Center the trace horizontally on the screen and rotate the VARIABLE control. Adjust the DC BAL control until the trace does not move as the VARIABLE control is rotated.



Fig. 4-12. Type 360, Front view.

#### **Vertical Attenuators**

There are two types of adjustment to be made. One is to compensate the various attenuators so the ac attenuation is equal to the dc attenuation. This involves a moderately short time constant and can be recognized by a slight rounding or overshoot at the leading corner of a 1-kc square wave. The other type of adjustment is to set the input capacitance equal in all positions of the attenuator so the 10 to 1 probe can be compensated for the instrument. This latter adjustment can be recognized by a downward or upward slope of about the first half of the top or bottom of a 1-kc square wave.

1. Attach the probe to the 360 VERTICAL INPUT and set the VOLTS/DIV switch to .05.

Connect the probe to a source of square waves such as the calibrator signal from a Tektronix oscilloscope or a Tektronix Type 105 Square-Wave Generator. Display about four or five cycles of a 1-kc square wave and adjust the probe trimmer to make the top of the square wave as flat as possible.

2. Turn the VOLTS/DIV switch to .5 and adjust C1 for a flat top and C2 for a square corner on the square wave.

3. Turn the VOLTS/DIV switch to 5 and adjust C4 for a flat top and C5 for a square corner on the square wave.

4. As a check, switch to 50 VOLTS/DIV and examine the square wave. In this position the two attenuators are cascaded and any slight misadjustment may add and become more noticeable. If there is any evidence of misadjustment repeat steps 2 and 3 until the shape of the square wave is acceptable in all three positions of the attenuator switch (50, 5, and .5).

#### Type 161

At the factory, a pulse width series of three capacitors is chosen arbitrarily from the six possible series shown on Fig. 4-19, page 4-13.

#### Adjustment

#### Pos. Pulse Delay

The Type 161 Pulse Generator is adjusted at the factory so that the OUTPUT PULSE DELAY dial will read correctly with an input sawtooth wave beginning at +150 volts and decreasing to +20 volts. If a negative going sawtooth with other dimensions is used the dial calibrations can be accommodated to the new dimensions by means of screwdriver limit controls accessible from the front panel. Turn the OUTPUT PULSE DELAY control full counterclockwise to zero. Trigger both an oscilloscope sweep and the Type 161 with the sawtooth and display one sawtooth on the oscilloscope. The TEKTRONIX Type 532 oscilloscope can be used for this purpose. Turn the OUTPUT PULSE DELAY CCW to .1. Adjust the POS. DELAY limit pot so the leading (left) edge of the pulse is at the 1 CM graticule division on the test scope. Set the OUTPUT PULSE dial to 1.0 and adjust NEG. DELAY so the pulse just drops off the right end of the sawtooth on the test scope. It may be necessary to go over these adjustments again to get proper

calibration as there is some interaction between them.

To check linearity, set OUTPUT PULSE DELAY to .5. The leading edge of the pulse should appear between the 4 and 6 CM mark on the test scope graticule.

#### Pulse Width Cal.

Observe the output pulse on an oscilloscope with a calibrated time base. Set the PULSE WIDTH switch to 0.1 MILLISECONDS and the PULSE WIDTH MULTIPLIER dial full clockwise to 1.0. Adjust PULSE WIDTH CAL. screwdriver adjustment, if necessary, until pulse width measures 0.1 millisecond on the calibrated oscilloscope.

#### **0.01 Millisecond Pulse Width**

Turn PULSE WIDTH switch full counterclockwise to 0.01 MILLISECONDS, and if necessary, adjust C6, a variable ceramic capacitor



Fig. 4-13. Right side view of the Type 161 showing location of the adjustment points.

mounted on the PULSE WIDTH switch, SW2, until the pulse width measures 0.01 milliseconds on the calibrated oscilloscope.

#### Pos. Pulse Ampl. Adj.

Observe the pulse output on a voltage-calibrated oscilloscope. Set the PULSE POLARITY switch to POS. and the PULSE AMPLITUDE dial full clockwise to 50. If necessary adjust the POS. PULSE AMPL. ADJ. screwdriver adjustable 2-megohm variable resistor, R30, until the pulse amplitude measures 50 volts on the calibrated oscilloscope.

#### Neg. Pulse Ampl. Adj.

Observe the pulse output on a voltage-calibrated oscilloscope. Set the PULSE POLARITY switch to NEG. and the PULSE AMPLITUDE switch full clockwise to 50. If necessary adjust R29, labeled NEG. PULSE AMPL. ADJ., a



Fig. 4-14. Left side view, Type 161.

5-k screwdriver-adjustable variable resistor until the pulse amplitude measures 50 volts on the calibrated oscilloscope.

#### **Pulse Compensation Capacitors**

Three screwdriver adjustable ceramic capacitors, C10, C11 and C12, are located inside the case on the left side of the subchassis. These capacitors compensate the voltage divider networks from grid-to-ground capacitance and should not need readjustment. Readjustment might occasionally be necessary after tube replacement, however. The uppermost of the three capacitors, C10, 3-12  $\mu\mu f$ , compensates the trailing edge of the pulse. The bottom capacitor, C11, 1.5-7  $\mu\mu f$ , compensates the leading edge of the negative pulse, which is observable with the PULSE POLARITY switch set to the NEG, position. The center capacitor. C12. 1.5-7  $\mu\mu f$ , compensates the leading edge of the positive pulse, observable with the PULSE POLARITY switch set to the POS. position. Observe the pulses on a wide-band oscilloscope capable of presenting the pulses accurately and adjust the compensating capacitors until the pulses are most nearly square.

#### Type 162

#### Adjustment

The Type 162 Waveform Generator has three screwdriver adjustments. One adjustment, R21B, is on the upper right of the front panel, marked CAL. This adjustment permits the pulse interval to be accommodated to the calibrations of the PULSE INTERVAL dial when the VERNIER dial is turned counterclockwise to the CALIBRATED POSITION index mark. Observe the interval between pulses, with the MULTIPLIER switch set to 1 times or 10 times, using an oscilloscope with a calibrated time base, such as the TEKTRONIX Type 532, and if necessary adjust the CAL control until the dial calibrations correspond to the pulse interval.

The second adjustment is C3B, the variable ceramic capacitor mounted on the MULTIPLIER switch in the 0.1-times position. Do not change this adjustment until you have determined that the CAL screwdriver adjustment is correct for the 1-times and 10-times positions of the MULTIPLIER switch. Be sure the VERNIER



Fig. 4-15. Right side view of the Type 162 showing location of the adjustment points.

control is set to the CALIBRATED POSITION index mark. Then turn the MULTIPLIER switch to the 0.1-times position and if necessary adjust C3B until the pulse interval is 0.1 milliseconds as measured on the calibrated oscilloscope.

The third adjustment is C9, located on the left side of the chassis between the tube sockets of V5 and V6. Adjust C9 for optimum flat top on the pulse waveform by observation of the oscilloscope display.

#### **Pulse Width Capacitors**

#### Type 163

If it should become necessary to replace one of the pulse-width determining capacitors C52, C53, or C54, we recommend that you order a complete set of three from the factory and replace the whole group. Be sure to state that the replacements are to be used in a Type



Fig. 4-16. Left side view, Type 162.

163 Pulse Generator and include the instrument serial number.

At the factory, a pulse-width series of three capacitors is chosen arbitrarily from the six possible series shown on Fig. 4-20, page 4-13.

#### Pos. Pulse Delay

The Type 163 Pulse Generator is adjusted at the factory so that the OUTPUT PULSE DELAY dial will read correctly with an input sawtooth wave beginning at +150 volts and decreasing to +20 volts. If a negative going sawtooth with other dimensions is used the dial calibrations can be accommodated to the new dimensions by means of screwdriver limit controls accessible from the front panel. Turn the OUTPUT PULSE DELAY control full counterclockwise to zero. Trigger both an oscilloscope sweep and the Type 163 with the sawtooth and display at least two pulses on the oscilloscope. The TEKTRONIX Type 532 oscilloscope can be used for this purpose. Adjust the POS. DELAY LIMIT screwdriver adjustment until the pulse is generated at the start of the sweep. Then turn the OUTPUT PULSE DELAY control full clockwise to 1.0 and adjust the NEG. DELAY LIMIT screwdriver adjustment until the pulse is generated at the completion of the sawtooth. Then repeat the adjustment procedure because the two controls are slightly interacting.

#### Pulse Width Calibrator

Observe the output pulse on an oscilloscope with a calibrated time base. Set the PULSE WIDTH switch to 100 microseconds and the PULSE WIDTH MULTIPLIER dial clockwise to 1.0. Adjust R42, labeled, PULSE WIDTH CAL., a front-panel screwdriver adjustment, if necessary, until the pulse width measures 100  $\mu$ seconds on the calibrated oscilloscope.

#### 1 Microsecond Pulse Width

Turn PULSE WIDTH switch full counter-



Fig. 4-17. Right side view of the Type 163 showing location of the adjustment points.

clockwise to 1 microsecond, and if necessary, adjust C50, a variable ceramic capacitor mounted on the PULSE WIDTH switch, SW20, until the pulse width measures 1 microsecond on the calibrated oscilloscope.

#### **Pulse Amplitude Calibrator**

Observe the pulse output on a voltage-calibrated oscilloscope. Set the PULSE AMPLI-TUDE dial full clockwise to 25. If necessary adjust the PULSE AMPLITUDE CALIBRATOR screwdriver adjustable variable resistor until the pulse amplitude measures 25 volts on the calibrated oscilloscope.

#### **Pulse Compensation Capacitors**

A screwdriver adjustable ceramic capacitor, C63, is located inside the case on the left side of the subchassis. This capacitor compensates the voltage divider network for grid-



Fig. 4-18. Left side view, Type 163.

to-ground capacitance and should not need readjustment. Readjustment might occasionally be necessary after tube replacement, however. C63 compensates the leading edge of the pulse. Observe the pulses on an oscilloscope capable of presenting the pulses accurately, such as TEKTRONIX Type 532, and adjust the compensating capacitor until the pulses are most nearly square.

	Series 4-L	Series 4-M	Series 4-N	Series 4-P	Series 4-Q	Series 4-R
C7,μμf	970	980	990	1000	1010	1020
C8, µf	.0097	.0098	.0099	.01	.0101	.0102
C9, µf	.097	.098	.099	.1	.101	.102

Fig. 4-19. Type 161 Pulse Width Capacitor Selections.

The values shown are minimum with tolerances -0% to +1%.

	Series 4-L	Series 4-M	Series 4-N	Series 4-P	Series 4-Q	Series 4-R
C52, μμf	950	960	970	980	990	1000
C53, μf	.0097	.0098	.0099	.01	.0101	.0102
C54, µf	.097	.098	.099	.1	.101	.102

Fig. 4-20. Type 163 Pulse Width Capacitor Selections.

The values shown are minimum with tolerances -0% to +1%.

PARTS LIST and

DIAGRAMS





## MANUFACTURERS OF CATHODE-RAY OSCILLOSCOPES

#### **HOW TO ORDER PARTS**

Replacement parts are available through your local Tektronix Field Office.

Improvements in Tektronix instruments are incorporated as soon as available. Therefore, when ordering a replacement part it is important to supply the part number including any suffix, instrument type, serial number, plus a modification number where applicable.

If the part you have ordered has been improved or replaced, your local Field Office will contact you if there is a change in part number.

# **PARTS LIST**

# Type 126

		Bulbs		Tektronix Part Number
B101	# 47			150-001
		Capacitors		
Values fixed unless marke Tolerances $\pm 20\%$ unless				
C105	.0047 µf	PT	400 v	285-506

C105	.0047 µ1	11	-00 •		100 000
C114	.01 µf	PT	400 v		<b>28</b> 5-510
C118A,B	2 x 15 μf	EMC	350 v	-10%+100%	290-056
C120	$2 \times 20 \mu f$	EMC	450 v	—10%+50%	290-037
C132	.01 µf	PT	400 v		285-510

#### Fuses

Fuse	lamp 3A	AG Fast-Blo for 117 v, 60 cycle operation	159-022
Fuse	0.5 amp 3 A	G Fast-Blo for 234 v, 60 cycle operation	159-025
Fuse	lamp 3 A	AG Slo-Blo for 117 v, 50 cycle operation	159-019
Fuse	0.5 amp 3 A	AG Slo-Blo for 234 v, 50 cycle operation	159-032

#### Resistors

Resistors are fixed, composition,  $\pm 10\%$  unless otherwise indicated.

R105 R107 R108 R110 R112	47 k 47 k 150 k 2.2 meg 1 k	1/2 w 1/2 w 1/2 w 1/2 w 1/2 w 1/2 w 1/2 w				302-473 302-473 302-154 302-225 302-102
R114 R116 R117 R118 R122	470 k 38 k 10 k 38 k 560 k	$\frac{1}{2} \le \frac{1}{2} \le \frac{1}$	Var.	Prec. WW Prec.	1% —170 Adjust 1%	302-474 309-124 311-015 309-124 302-564
R123 R124 R130 R132 R133	47 k 390 k 1 meg 1 k 500 k	$\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$		Prec.	1%	302-473 302-394 302-105 302-102 309-003
R134 R140 R141 R143	370 k 111 k 220 k 150 k	1/2 w 1/2 w 1/2 w 1/2 w 1/2 w		Prec. Prec. Prec.	1% 1% 1%	309-055 309-046 309-052 302-154

1

Switches Tektronix Part Number 260-134 SW101 POWER ON Toggie **Transformers** \*120-076 T101 Power Transformer **Electron Tubes** 154-052 V105 5651 154-022 V110 6AU6 154-044 V115 12**B**4 154-119 V118 6BW4 154-119 6BW4 V120 154-044 V125 12B4 154-078 V130 6AN8

## Type 160 & 160A

#### Bulbs

B1	Х <b>620</b> -ир	# 47				150-001			
Capacitors Values fixed unless marked variable									
Tolerance $\pm 2$	20% unless otherw	vise indicated.							
C1 & 2	101-323 324-619 620-up	2 × 20 μf 2 × 40 μf 2 × 20 μf	EMC EMC EMC	450 v 450 v 450 v	—10+50% —10+50% 10+50%	290-037 290-043 290-043			
C3 C4	101-619X 101-619X	.005 μf .005 μf	Discap Discap	500 v 500 v	GMV GMV	283-001 283-001			
C5 & 6 C7 C8 C9	101-619Х 101-619Х Х620-ир	2 x 20 μf .005 μf .005 μf .047 μf	EMC Discap Discap PT	450 v 500 v 500 v 400 v	—10+50% GMV GMV	290-036 283-001 283-001 285-519			
C11	Х620-ир	.1 μf	PT	400 v		<b>285</b> -526			
C30 C41 C47	Х620-ир Х620-ир Х620-ир	2 x 40 μf .047 μf .005 μf	EMC PT Discap	450 v 400 v 500 v	—10+50% GMV	290-043 285-519 283-001			

#### Fuses

101-619	3 amp 3 AG Slo-Blo for 117 V, 60 cycle operation	159-005
620-up	4 amp 3 AG Slo-Blo for 117 V, 50-60 operation	159-027
101-619	1.6 amp 3 AG Slo-Blo for 234 V, 50 cycle operation	159-003
620-up	2 amp 3 AG Slo-Blo for 234 V, 50-60 operation	159-023

#### Resistors

Resistors are fixed, composition,  $\pm 10\%$  unless otherwise indicated.

						F	Part Number
RI	101-619 620-up	220 k 47 k	1 w 1⁄2 w				<b>304-2</b> 24 <b>302-4</b> 73
R2	101-619	1 meg	1/2 W				<b>302-10</b> 5 <b>302-15</b> 4
R3	620-ир 101-619	150 k 47 k	½ w 1 w				302-154
NO	620-up	2.2 meg	1∕₂ w				302-225
R4	101-619X	10 k	¹∕₂ w				<b>302-10</b> 3
R5	101-619X	470 k	% <sup>1</sup> /₂ <sup>1</sup> /₂				302-474
R5A	101-619X	50 k	2 w	Var.	Prec.	ADJ TO +225 1%	V 311-023 309-001
R5B R5C	101-619X 101-619X	433 k 333 k	½ w ½ w		Prec.	1%	309-053
R7	X620-up	47 k	1∕₂ w				<b>302-4</b> 73
R8	101-619	270 k	¹∕₂ w				302-274
50	620-up	470 k	1/2 W		Dues	1 0/	302-474 309-003
R9	101-619 620-up	500 k 38 k	½ w ½ w		Prec. Prec.	1% 1%	309-124
	020-0p	50 K	/2 **		1100.		
R10	101-619 620-up	500 k 10 k	½ w 2 w	Var.	Prec. WW	1% ADJ TO —170\	309-003 / 311-015
R11	101-619	220 k	1 w				304-224
	620-up	38 k	1/2 W		Prec.	1%	309-124
R12	101-619X	1 meg	1∕2 w				<b>302</b> -105
R13	101-619	1 k	¹∕₂ w				302-102
<b></b>	620-up	10 k	1/2 W				<b>302-10</b> 3
R14	101-619 620-up	33 k 100 k	1∕2 w 1∕2 w				<b>302-3</b> 33 <b>302-1</b> 04
<b>R1</b> 5	82 <b>0-</b> 0p	470 k	/₂ ₩ /⁄₂ ₩				302-474
R15A	101-619X	10 k	2 w	Var.	WW	ADJ TO	
R15B	101-323	82 k	1∕₂ w				Use 309-043
R15C	324-619X 101-323	82 k 82 k	1/₂ w		Prec.	1%	309-043 Use 309-043
RIDC	324-619X	82 k	$\frac{1}{2} \le \frac{1}{2} \le \frac{1}$		Prec.	1%	309-043
R16	X324-619	100 k	1∕₂ w				302-104
517	620-up	1 k	1∕₂ w				302-102 302-102
R17 R20	Х620-ир Х620-ир	1 k 100 k	½ w ½ w				302-102
R30	Х620-ор	330 k	72 ₩ 1⁄2 ₩				302-334
R31	Х620-ир	220 k	1∕₂ w				302-224
R32	X620-739	390 k	1∕₂ w				Use 302-564
R33	740-up Х620-up	560 k 1 meg	1∕₂ w 1∕₂ w				<b>302-564</b> <b>302</b> -105
R34	Х620-ир	1 k	1/2 W 1/2 W				302-102
<b>R3</b> 5	X620-up	1 k	1∕₂ w				302-102
R40	X620-up	470 k	¹∕₂ w				302-474
R41	X620-up	490 k	½ w		Prec.		309-002
R42 R43	Х620-up Х620-up	50 k 333 k	2 w 1⁄2 w	Var.	Prec.	ADJ TO +225\ 1%	/ 311-023 309-053
	Х620-ир				1160.	' /0	
R46	X620-up	270 k	<sup>1</sup> /₂ w		Prec.	1 %	302-274 309-056
R47 R48	Х620-up Х620-2277	390 k 433 k	½ w ½ w		Prec. Prec.	1% 1%	Use 309-170
N <del>4</del> 0	2278-up	433 k 429 k	/₂ w 1∕₂ w			1%	309-170
	•		. –				

Tektronix

	Switches Tektron							
			Part Number					
SW1		Toggle	260-134					
		Transformers						
TI	101-619	Power Transformer T160PA	*120-009					
		Primary: 117-234 volts 60 cycle						
		Secondary: Term. 5, 6, 7, 210-0-210 v at 175 ma						
		Term. 8, 9, 10, 260-0-260 v at 175 ma Term. 11, 12, 5.2 v at 2A Term. 13, 14, 5.2 v at 2A						
		Term. 15, 16, 6.5 v at 15A						
	620-up	Power Transformer T160PB1	*120-054					
		Primary: 117/234 volts 50-60 cycle						
		Secondary: Term. 7, 8, 9, 260-0-260 at 250 ma						
		Term. 14, 15, 16,, 227-0-227 at 150 ma Term. 5, 6, 6.3 vac at 12.5A Term. 10, 11, 6.3 vac at 12.5A Term. 12, 13, 5 vac at 4A Term. 20, 21, 5 vac at 2A						

#### **Electron Tubes**

V1 V2 V3 V4 V5	101-619X 101-619X 101-619X 101-619X	5 <b>V4G</b> 5V4G 6AS7G 6AU6 5661	154-008 154-008 154-020 154-022 154-052
V6	101-619	6AU6	154-022
	620-up	5651	154-052
V7	101-619	12AU7	154-041
	620-up	6U8	154-033
V8	X324-619X	5V4G	154-008
V16	Х620-ир	1284	154-044
V17	X620-up	12B4	154-044
V30	X620-up	5V4G	154-008
V31	X620-up	5V4G	154-008
V33	X620-up	6AU6	154-022
V35	X620-up	6080 (Alternate-6AS7G)	154-056
V47	X620-up	6AW8	154-095

# Type 161

#### Capacitors

Tolerance  $\pm 20\%$  unless otherwise indicated. Values fixed unless marked Variable.

C1A,B	2 x 15 μf	EMC	350 v	-10+100%	290-034
C2	.1 μf ΄	PTM	400 v		285-526
C3	12 µµf	Cer.	500 v	10%	281-506
C4	22 µµf	Cer.	500 v		281-510
C5	$100 \ \mu\mu$ f	Mica	500 v	10%	283-505

#### **Capacitors** (continued)

Tektronix Part Number

C6A C6B C7		82 μμf 7-45 μμf .001 μf	Cer. Cer. Mica	Var.	500 v 500 v 500 v	10% Selected	281-528 281-012 *295-030
C8 C9		.01 μf .1 μf	PTM PTM		400 v } 400 v }	Selected	275-030
<b>C</b> 10		0.10	c	M.	<b>600</b>		281-007
C10		3-12 μμf	Cer.	Var.	500 v		
C11		1.5-7 μμf	Cer.	Var.	500 v		281-005
C12	101-135	1.5-7 μμf	Cer.	Var.	500 v		Use 281-010
	136-up	4.5-25 μμf	Cer.	Var.	500 v		281-010
C21	X1396-up	2.2 μμf	Cer.		500 v	±0.5 μμf	281-500

#### Inductors

L36	Х1396-ир	1.2 mh	*10	8-122
100	N1070-0p	1.4 1111		

### Resistors

Resistors are fixed, composition,  $\pm 10\%$  unless otherwise indicated.

R1 R2 R3 R4 R5		180 k 100 k 100 k 100 Ω 10 k	1 w 1/2 w 2 w 1/2 w 5 w			ww	5%	304-184 302-104 306-104 302-101 308-008
R6 R7 R8 R9A R9B		27 k 100 k 470 k 100 k 100 k	$     \begin{array}{c}       1 & w \\       V_2 & w \\       V_2 & w \\       2 & w \\       2 & w \\       2 & w     \end{array} $	Var. Var.	output	pulse dela	y (Pos. Trigger Bi Pos. Delay Li	
R9C		50 k	2 w	Var.			Neg. Delay Li	
<b>R</b> 10	101-135 136-2044 2045-up	1 meg 1.1 meg 1 meg	½ ₩ ½ ₩ ½ ₩				5% 1%	Mod w/R11 Mod w/R11 309-014
R11	101-2044 2045-up	1 meg 1 meg	1/₂ w 1/₂ w				2% 1%	Mod w/R10 309-014
R12		22 k	1 w					304-223
R13		2.7 k	1/2 W					<b>302-272</b> <b>304-22</b> 3
R14 R15		22 k 470 k	1 w 1⁄2 w					302-474
R16		560 k	1/2 w					<b>302</b> -564
R17		47 k	½ w					302-473
R18		22 k	1/2 W					302-223 302-824
R19 R20	101-2167	820 k 120 k	$\frac{1}{2}$ w $\frac{1}{2}$ w					Mod w/R34
1120	2168-3819	150 k	½ w					Mod w/R34
	3820-up	150 k	1/2 w				5%	<b>301</b> -154
R21		1.0 meg	½ w					302-105
R22	141 1445	820 k	1/2 w					302-824 306-223
R23	101-1395 1396-up	22 k 12 k	2 w 2 w				Pulse Width	<b>3</b> 06-223 <b>3</b> 06-123
R24		2 meg	Selected for linearity				Multiplier	*312-104

**Resistors** (continued)

Tektronix Part Number

R25 R26 R27 R28		Selected to ma 50 k 47 k 1 meg	tch <b>R24. (</b> See 1 2 w 1 w ½ w	Гехt) Var.		Pulse Width Neg. Pulse A	<b>304-47</b> 3 <b>302-10</b> 5
R29		5 k	2 w	Var.	WW	Adj.	311-012
R30 R31	101-2542 2543-2712 2713-up	2 meg 5 k 10 k 15 k 6 k	2 w 2 w 2 w 1/2 w 2 w	Var. Var. Var.	ww ww ww	Pos. Pulse Am Adj. Pulse Amplita	311-042B Use 311-128 Use 311-128
R32	101-1395 1396-up	1.2 meg 1 meg	½ ₩ ½ ₩				<b>302-12</b> 5 <b>302-</b> 105
R33 R34	101-3819 3820-up	5.6 k 120 k 120 k	2 w 1/ <sub>2</sub> w 1/ <sub>2</sub> w			5%	306-562 Mod w/R20 301-124
R35 R36	Х1396-ир	2.7 k 10 k	2 w 1/2 w				306-272 302-103

#### **Switches**

			Wired	Unwired
SW1	toggle	TRIGGER SELECTOR	*262-011	260-014
SW2	rotary	PULSE WIDTH		*260-030
SW3	toggle	PULSE POLARITY		260-014

**Electron Tubes** 

V1 V2 V3 V4		12AU7 12AT7 12AT7 12AT7 12AT7	154-041 154-039 154-039 154-039
V5	101-3193	6J6	154-032
	3194-up	6DJ8	154-187

# Type 162

#### Capacitors

Values fixed unless marked Variable. Tolerance  $\pm 20\%$  unless otherwise indicated.

C1A,B	2 x 15 μf	EMC		350 v	-10+100%	290-034
C2	.1 μf	PT		600 v		285-528
C3A	12 μμf	Cer.		500 v	10%	281-506
C3B	82 $\mu\mu$ f	Cer.		500 v	10%	281-528
C3C	7-45 μμf	Cer.	Var.	500 v		<b>281-0</b> 12

### **Capacitors** (continued)

Tektronix Part Number

C3D C3E C3F C3G	101-562 101-562 101-562 101-562	.001 μf .01 μf .1 μf 1 μf	Selec	ted Timing Se	eries		Use *050-059
C3D C3E	563-ир 563-ир	.001 μf .01 μf	Mylar )				*291-008
C3F C3G	563-up 563-up	.1 μf 1.0 μf	{Myla	r Timing Serie	s		*291-004
C4	900-0p	22 μμf	J		500 v		281-510
C5 C6		.005 μf 470 μμf	Discap Cer.		500 v 500 v	GMV	283-001 281-525
C7		25 μμf	Cer.		500 v	5%	281-552
C8 C9	101-1506	$22 \mu\mu f$	Cer. Cer.		500 v 500 v	Selected	281-510 *295-001
C9	1507-up	4.7 μμf 3-12 μμf	Cer.	Var.	500 v 500 v	Jelecieu	281-009
C10	101-119	$12 \mu\mu f$	Cer.		500 v	10%	281-506 281-510
C12	120-ир X7015-ир	22 μμf .005 μf	Cer. Discap		500 v 500 v		<b>281-510</b> <b>283-001</b>

#### Resistors

Resistors are fixed, composition,  $\pm 10\%$  unless otherwise indicated.

101-119 120-159 160-ор	220 Ω 8 k 47 k 1 meg 22 k 10 k 8.2 k	1/2 w 5 w 1/2 w 1/2 w 1/2 w 1 w 1 w 1 w	ww	<b>5%</b> 5%	302-221 308-007 302-473 302-105 Mod w/R16 Mod w/R16 Use 303-822
101-119 120-up	680 k 750 k	1/2 W 1/2 W	Prec.	1%	302-684 309-010
101-119 120-up	1.2 k 33 k	1 w 2 w			304-122 306-333
101-119 120-up	1 meg 700 k	1/2 w 1/2 w	Prec.	1%	302-105 309-008
101-119 120-up	22 k 15 k	l w l w			304-223 304-153
•	470 k	¹/₂ w			302-474
101-159 160-ир	560 k 470 k	1∕2 w 1∕2 w			Use 302-474 302-474
	2.2 meg	1/2 W			<b>302-22</b> 5
	47 k	ĩw			<b>30</b> 4-473
101-3294 3295-up		<sup>1</sup> ∕ <sub>2</sub> ₩ <sup>1</sup> ⁄ <sub>2</sub> ₩		5%	Use 301-474 301-474
101-3294 3295-up	680 k 680 k	½ w ½ w		5%	Use 301-684 301-684
101-159	18 k 22 k	2 w 2 w			Mod w/R5 <b>306-223</b>
	l meg	1∕₂ w			<b>302-10</b> 5
	1.5 meg 100 k 1.5 meg .39 meg .49 meg	$\frac{1}{2} w$ 1 w $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$	Prec. Prec. Prec.	1% 1% 1%	302-155 304-104 309-017 309-056 309-002
	120-159 160-up 101-119 120-up 101-119 120-up 101-119 120-up 101-119 120-up 101-159 160-up 101-3294 3295-up 101-3294 3295-up	8 k 47 k 1 meg 101-119 22 k 120-159 10 k 160-up 8.2 k 101-119 680 k 120-up 750 k 101-119 1.2 k 120-up 33 k 101-119 1 meg 120-up 700 k 101-119 22 k 101-119 22 k 101-159 560 k 101-159 560 k 101-159 560 k 101-3294 470 k 3295-up 470 k 101-3294 680 k 3295-up 680 k 101-159 18 k 100 k 1.5 meg .39 meg	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	8k         5w         WW           47 k $\frac{1}{2}$ w           1 meg $\frac{1}{2}$ w           101-119         22 k         1 w           120-159         10 k         1 w           101-119         8.2 k         1 w           101-119         680 k $\frac{1}{2}$ w         Prec.           101-119         1.2 k         1 w         Prec.           101-119         22 k         1 w         Prec.           101-119         22 k         1 w         Prec.           101-119         22 k         1 w         Prec.           101-159         560 k $\frac{1}{2}$ w         Prec.           101-3294         470 k $\frac{1}{2}$ w         Prec.           101-3294         680 k $\frac{1}{2}$ w         Prec.           101-159         18 k         2 w         Prec.           101-159         18 k         2 w <td< td=""><td>8k <math>5w</math>       WW       <math>5%</math> <math>47k</math> <math>1/2w</math> <math>1/2w</math> <math>1/2w</math> <math>101-119</math> <math>22k</math> <math>1w</math> <math>5%</math> <math>120-159</math> <math>10k</math> <math>1w</math> <math>5%</math> <math>101-119</math> <math>8.2k</math> <math>1w</math> <math>5%</math> <math>101-119</math> <math>8.2k</math> <math>1w</math> <math>5%</math> <math>101-119</math> <math>1.2k</math> <math>1w</math> <math>5%</math> <math>101-119</math> <math>1.2k</math> <math>1w</math> <math>1%</math> <math>120-up</math> <math>33k</math> <math>2w</math> <math>Prec.</math> <math>1%</math> <math>101-119</math> <math>1.2k</math> <math>1w</math> <math>1%</math> <math>1%</math> <math>120-up</math> <math>700k</math> <math>1/2w</math> <math>Prec.</math> <math>1%</math> <math>101-119</math> <math>1.2k</math> <math>1w</math> <math>1%</math> <math>1%</math> <math>120-up</math> <math>700k</math> <math>1/2w</math> <math>Prec.</math> <math>1%</math> <math>101-159</math> <math>560k</math> <math>1/2w</math> <math>7%</math> <math>7%</math> <math>101-3294</math> <math>470k</math> <math>1/2w</math> <math>5%</math> <math>101-3294</math> <math>680k</math> <math>1/2w</math> <math>5%</math> <math>160-up</math> <math>22k</math> <math>2w</math> <math>1.5meg</math> <math>1/2w</math> <math>1.6meg</math> <math>1/2w</math> <math>1w</math></td></td<>	8k $5w$ WW $5%$ $47k$ $1/2w$ $1/2w$ $1/2w$ $101-119$ $22k$ $1w$ $5%$ $120-159$ $10k$ $1w$ $5%$ $101-119$ $8.2k$ $1w$ $5%$ $101-119$ $8.2k$ $1w$ $5%$ $101-119$ $1.2k$ $1w$ $5%$ $101-119$ $1.2k$ $1w$ $1%$ $120-up$ $33k$ $2w$ $Prec.$ $1%$ $101-119$ $1.2k$ $1w$ $1%$ $1%$ $120-up$ $700k$ $1/2w$ $Prec.$ $1%$ $101-119$ $1.2k$ $1w$ $1%$ $1%$ $120-up$ $700k$ $1/2w$ $Prec.$ $1%$ $101-159$ $560k$ $1/2w$ $7%$ $7%$ $101-3294$ $470k$ $1/2w$ $5%$ $101-3294$ $680k$ $1/2w$ $5%$ $160-up$ $22k$ $2w$ $1.5meg$ $1/2w$ $1.6meg$ $1/2w$ $1w$

**Resistors** (continued)

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Part	Number

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							Farr INUMber
R20D R20E R20F R20G R20H		.61 meg .78 meg .97 meg 1.23 meg 1.55 meg	1/2 W 1/2 W 1/2 W 1/2 W 1/2 W 1/2 W		Prec. Prec. Prec. Prec. Prec.	1% 1% 1% 1% 1%	309-006 309-011 309-012 309-016 309-018
R201 R20J R20K R21 A	101-212 213-up	1.94 meg 2.44 meg 3.10 meg 50 k 20 k	1/2 w 1/2 w 1/2 w 2 w 2 w 2 w	Var. Var.	Prec. Prec. Prec.	1% 1% 1% Vernier Vernier	309-022 309-024 309-027 311-023 311-018
R21B R21C R22	101-212 213-ир 101-212 213-ир	50 k 20 k 150 k 56 k 27 k	2 w 2 w 1 w 1 w 2 w	Var. Var.		Cal. Cal.	311-023 311-018 304-154 304-563 306-273
R23 R24 R25 R26 R27		150 k 220 Ω 47 k 470 k 470 k	1/2 w 1/2 w 1 w 1/2 w 1/2 w				302-154 302-221 304-473 302-474 302-474
R28 R29 R30 R31 R32	101-159 160-ир	27 k 27 k 470 k 27 k 680 k 220 k	1 w 2 w 1/2 w 2 w 1/2 w 1/2 w				Use 306-273 306-273 302-474 306-273 302-684 302-224

#### **Switches**

		Wired Unwired
SW1	Rotary OPERATING MODE	*262-013 *260-044
SW2	Pushbutton MANUAL	*260-017
SW3	Rotary MULTIPLIER	<b>*262-012 *260-038</b>
SW4	Toggle GATE OUT, PULSE OUT	260-014
SW5	Rotary WAVEFORM DURATION	<b>*262-014 *260-024</b>

#### **Electron Tubes**

V1 V2 V3 V4	12AU7 12AU7 12AU7 6BH6 12AU7	154-041 154-041 154-041 154-026 154-041
V5	12AU7	154-041
V6	12AU7	104-041

# Type 163

#### Capacitors

	l unless marked Va ⊵20% unless otherv					Tektronix Part Number
C5 C11 C15 C23	101-182 183-up	2 x 15 μf .001 μf .01 μf 22 μμf 12 μμf	EMC Cer. PT Cer. Cer.	350 v 500 v 600 v 500 v 500 v	—10+100% GMV 10%	290-034 283-000 285-511 281-510 281-506
C33 C42 C50 C51	101-182 183-ир	22 μμf 39 μμf .01 μf 7-45 μμf 56 μμf	Cer. Cer. PT Cer. Cer.	500 v 500 v 400 v 500 v 500 v	10% 10%	281-510 281-516 285-510 281-012 281-521
C52 C53 C54 C63	101-1372 1373-ир	.001 μf .01 μf .1 μf 1.5-7 μμf 3-12 μμf	Mica PT PT Cer. Cer.	Timing Capacitors Selected See Text 500 v 500 v		*295-059 Use 281-009 281-009

#### Resistors

Resistors are fixed, composition,  $\pm 10\%$  unless otherwise indicated.

R5 R6 R10 R11 R13		10 Ω 8 k 180 k 100 k 47 Ω	1/2 w 5 w 1/2 w 1/2 w 1/2 w		ww	5%	302-100 308-007 302-184 302-104 302-470
R14 R15 R16 R20		22 k 470 k 100 k 100 k	½ w ½ w 2 w 2 w			Pos. Delay Limit	302-223 302-474 306-104 311-026
R21		100 k	2 w			Output Pulse Delo Trigger Bias	ay, Pos. 311-026
R22 R23	101-182	50 k 220 k	2 w ½ w	Var.		Neg. Delay Limit	302-224
R24	183-ир 101-182 183-ир	220 k 470 k 500 k	$\frac{1}{2} \le \frac{1}{2} \le \frac{1}$		Prec. Prec.	1% 1%	309-052 302-474 309-003
R30 R31	101-182 183-up	2.2 k 10 k 8.2 k	1/2 w 2 w 2 w				302-222 306-103 306-822
<b>R32</b> R33	101-182 183-up	3.3 k 220 k 220 k	$\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$		Prec.	1%	302-332 302-224 309-052
R34	101-182 183-up	390 k 433 k	1/2 W 1/2 W		Prec.	1%	302-394 309-001
R40	101-3939 3940-up	2.7 k 2.5 k	2 w 5 w		ww	5%	306-272 308-127
R41		47 Ω	¹∕₂ w				302-470

#### **Resistors** (continued)

			Resisions (CO	mmoeuj			
						Par	Tektronix t Number
						Pul <del>se</del> Width	
R42		100 k	2 w	Var.		Calibrator	311-026
R43		470 k	1/2 w	vui.		Calibrator	302-474
R45		18 k	2 w				306-183
R46		39 k	l w				304-393
R47		18 k	2 w				306-183
R48	101-182	4.7 k	2 w				306-472
	183-up	8.2 k	2 w			(2)	
R49	•	47 Ω	½ w			.,	302-470
R50	101-3289	Selected (nom	inal value 2.7 k)			10%	302-272
R50	3290-up		inal value 4.7 k)			10%	302-472
R51		100 k Select	ed for linearity	Var.		Pulse Width Mult.	*312-014
R52	Х3290-ир	1 m	¹/₂ w			10%	302-105
R60		15 <b>0</b> k	1 w				<b>304-</b> 154
						Pulse Amplitude	
R61	101-182	10 k	2 w	Var.		Calibrator Pulse Amplitude	311-016
	183-up	20 k	2 w	Var.		Calibrator	311-018
R62		700 k	1/2 W		Prec.	1%	309-008
R63	101-182	750 k	1/2 w		Prec.	1%	309-010
	183-up	780 k	1/2 w		Prec.	1%	309-011
R64	•	47 Ω	1∕₂ w				302-470
R65		47 Ω	1/2 w				302-470
R66		2 k	2 w	Var.		Pulse Amplitude	311-008
			Switch	P <b>C</b>			
						\ <b>\</b> /!	I Investment
0.1420		<b>-</b> •				Wired	Unwired
SW10			GER SELECTOR			+0/0 01 0	260-014
SW20		Rotary PULS	e width			*262-015	*260-030

#### **Electron Tubes**

V10	6U8	154-033
V11	6U8	154-033
V12	6AL5	154-016
V13	12BY7	154-047
V14	12BY7	154-047
V15	6BQ7A	154-028

# Type 360

#### Bulbs

#### Capacitors

# Values fixed unless marked Variable. Tolerance $\pm 20\,\%$ unless otherwise indicated.

C1	4.5-25 μμf	Cer.	Var.	500 v	281-010
C2	4.5-25 μμf	Cer.	Var.	500 v	281-010
C3	100 μμf	Cer.		350 v	281-523
C4	4.5-25 μμf	Cer.	Var.	500 v	281-010
C5	4.5-25 μμf	Cer.	Var.	500 v	281-010

#### Capacitors (continued)

Tektronix Part Number

							Part Number
C6 C7 C10 C30 C31		.001 μf 47 μμf .1 μf 4.7 μμf .001 μf	Mica Cer. PTM Cer. Cer.		500 v 500 v 400 v 500 v 500 v	5% ±1 μμf GMV	283-527 281-518 285-526 281-501 283-000
C39 C40 C73 C76 C90	X132-ир 101-131X	.01 μf .005 μf 2.2 μμf 82 μμf .047 μf	Discap Discap Cer. Cer. PTM		500 v 500 v 500 v 500 v 400 v	±.3 μμf 10%	283-002 283-001 281-500 281-528 285-519
C92 C104 C106 C107 C114	Х132-ир	.01 μf .001 μf .001 μf .001 μf .02 μf	Cer. Discap Discap PTM Discap		500 v 500 v 500 v 1000 v 150 v	GMV GMV GMV GMV	283-002 283-000 283-000 285-502 283-004
C116 C116 C117 C117 C120	101-1929 1930-ир 101-1929 1930-ир Х1930-ир	.0068 μf .01 μf .0068 μf .01 μf .001 μf	PTM Discap PTM Discap Discap		3000 v 2000 v 3000 v 2000 v 500 v	GMV	285-508 283-011 285-508 283-011 283-000
C131 C132 C133 C133 C134	101-1929 1930-ир 101-1929	.047 μf .022 μf .0068 μf .01 μf .0068 μf	PTM PTM PTM Discap PTM		400 v 400 v 3000 v 2000 v 3000 v		285-519 285-515 285-508 283-011 285-508
C134 C136 C136 C140A,B	1930-ир 101-1929 1930-ир	.01 μf .0068 μf .01 μf 2 x 20 μf	Discap PTM Discap EMC		2000 v 3000 v 2000 v 450 v		283-011 285-508 283-011 290-037
			Resistors	i			
Resistors are fixe R2 R3 R5 R6 R30	:d, composition, ±	=10% unless otherw 900 k 111 k 990 k 10.1 k 1 meg	vise indicated. 1/2 w 1/2 w 1/2 w 1/2 w 1/2 w 1/2 w		Prec. Prec. Prec. Prec. Prec.	1% 1% 1% 1% 1%	309-111 309-046 309-013 309-034 309-014
R31 R32 R33 R34 R35		100 k 5.6 k 82 k 7 k 82 k	1 w 1 w 2 w 1 w 1 w	Var.		5% 5% Volts/Div Variable 5%	302-104 303-562 Use 303-823 Use 311-223 Use 303-823
R37 R38 R39 R40	Х1690-ир	150 k 500 k 220 k 2.2 k	1/2 w .2 w 1/2 w 1/2 w	Var.		DC Bal	302-154 311-068 302-224 302-222

R38 R39 R40 R41	500 k 220 k 2.2 k 5.6 k	.2 w 1/2 w 1/2 w 1/2 w 1 w	Var.		DC Bal 5%	311-068 302-224 302-222 303-562
R45 R46 R47 R50 R51	270 k 2 x 100 k 270 k 10 k 1 k	1/2 w (Concentric w/R71) 1/2 w 5 w 1/2 w		ww	Horiz. Pos. 5%	302-274 311-064 302-274 308-008 302-102
R54 R55 R56 R57 R58	12 k 12 k 500 k 12 k 12 k	2 w 2 w .2 w 2 w 2 w 2 w	Var.		Vert Gain Adj.	306-123 306-123 311-066 306-123 306-123

**Resistors** (continued)

Tektronix Part Number

R60 R61 R62 R63		1 k 10 k 1 k 1.5 k	½ ₩ 5 ₩ 1 ₩ 1 ₩		WW	5%	302-102 308-008 304-102 304-152
R70 R70 R71 R71 R72A,B R72	101-131 132-ир 101-131 132-ир 101-131 132-ир	47 Ω 180 k 47 Ω 100 k (Concentric 150 k 490 k	$\frac{1}{2}$ w $\frac{1}{2}$ w with R46) 2 w $\frac{1}{2}$ w		Prec.	Vert. Pos. 1%	302-470 302-184 302-470 311-064 306-154 309-002
R73 R73 R74 R75 R75	101-131 132-up 101-131X 101-131 132-up	5 k 750 k 82 k 150 k 666.6 k	.2 w 1/2 w 1/2 w 1/2 w 1/2 w	Var.	Prec. Prec.	1%	311-067 309-010 302-823 302-154 309-007
R76 R76 R77 R77 R78	101-131 132-up 101-131 132-up Х132-up	56 k 39 k 270 k 5 k 47 Ω	$\frac{1}{2} \approx \frac{1}{2} = \frac{1}$	Var.		Sweep Cal.	302-563 302-393 302-274 311-067 302-470
R80 R83 R83 R84 R84	101-131Х 101-131 132-up 101-131 132-up	470 k 666.6 k 1.2 meg 608 k 800 k	$\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$		Prec. Prec. Prec. Prec.	1% 1% 1% 1%	302-474 309-007 309-149 309-005 309-110
R85 R85 R86 R86 R90	101-131 132-ир 101-131 132-ир	970 k 1.2 meg 100 k 47 k 10 k	$\frac{1}{2} \le \frac{1}{2} \le \frac{1}$		Prec. Prec.	1% 1%	309-012 309-149 302-104 302-473 302-103
R91 R92 R100 R104 R105		270 k 120 k 1 meg 47 k 47 k	$\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$ $\frac{1}{2} w$				302-274 302-124 302-105 306-473 <b>302</b> -473
R106 R113 R114 R115 R116	Х132-ир Х132-ир 101-1929	1.5 k 180 k 56 k 1 meg 100 k	$\frac{1}{2} = \frac{1}{2} = \frac{1}$				302-152 302-184 302-563 302-105 302-104
R116 R117 R118 R119 R120	1930-ир 101-131Х	56 k 6.8 meg 6.8 meg 1 meg 1.5 meg	$\frac{1}{2} \approx \frac{1}{2} \approx \frac{1}$	Var.		Intensity	302-563 306-685 306-685 311-041 302-155
R120 R121 R122 R130 R131	Х317-ир Х1930-ир	3.3 meg 1.5 meg 33 k 1 k 1 meg	$\frac{1}{2} \approx \frac{1}{2} \approx \frac{1}$				302-335 302-155 302-333 302-102 302-105
R132 R133 R134 R135 R136 R138		2 meg 3.9 meg 2 meg 1.5 meg 27 k 50 k	2 w 2 w 2 w $1/_2 w$ $1/_2 w$ $1/_2 w$ 2 w	Var. Var. Var.		H.V. Adj. Focus Astigmatism	311-042 306-395 311-043 302-155 302-273 311-023
-						-	

			<b>Resistors</b> (c	ontinued)		
						Tektronix Part Number
R140 R141		270 Ω 10 k	½ w 5 w		5%	302-271 308-008
R141		270 Ω	'∕₂ w		5 /6	302-271
R145		27 k	2 w	Mara	Saula Illum	306-273 311-055
R146		50 Ω	2 w	Var.	Scale Illum.	311-000
			Switch	185		
0.170	101 070	<b>-</b> 1			Wir	ed Unwired 260-134
SW9	101-378 379-up	Toggle Toggle	AC-DC AC-DC			260-014
SW10		Rotary	VOLTS/DIV		*262	-098 *260-119
SW <b>80</b>	Х132-ир	Toggle	SAWTOOTH POLA	RITY		260-014
			Transfor	mers		
т100		CRT Supply	y T3150A2			*120-011
		Primary:	68-0-136 vac			
		Secondary:	1240 vac			
			1310 vac 2 heater winding	gs		
T140		CRT Heater	r Isolating Transform	er T360FA1		*120-065
		Primary:	6.3 vac			
		Secondary:	6.3 vac, <b>.6 a</b> mp			

## **Electron Tubes**

V30 V32 V50 V52 V70 V72	101-131X X132-up	6AU6 6AU6 6EW6/6AU6 6EW6/6AU6 6BQ7A 6AN8	154-022 154-022 Use 154-212 Use 154-212 154-028 154-078
V80 V100 V104 V115 V116		6AU6 12AT7 6AQ5 5642 5642 T310/3WP CRT P2 Standard Phosphor	154-022 154-039 154-017 154-051 154-051 154-059

# Type 126 Mechanical Parts List

	Tektronix Part Number
ADAPTOR, 3 WIRE TO 2 WIRE	103-013
CABINET	437-051
CABLE, HARNESS	179-111
CAP, FUSE	200-015
CAP, CABLE SIDE ACCESS	200-098
CHASSIS, POWER	441-125
CLAMP, CABLE 1/4 PLASTIC	343-003
CONNECTOR, CHAS. MT 2 CONT. MALE SN 101-240	131-010
CONNECTOR, CHAS. MT 3 WIRE MALE SN 241-up	131-102
GROMMET, RUBBER 1/4	348-002
GROMMET, RUBBER 3/8	348-004
HOLDER, FUSE	352-010
JEWEL, LIGHT PILOT RED DRAKE	378-518
LOCKWASHER, INT. #4	210-004
LOCKWASHER, EXT. #6	210-005
LOCKWASHER, INT. #6	210-006
LOCKWASHER, INT. #8	210-008
NUT, HEX, 4-40 x <sup>3</sup> / <sub>16</sub>	210-406
NUT, HEX, 6-32 x ¼	210-407
NUT, HEX, 3/8-32 x 1/2	210-413
NUT, HEX, <sup>15</sup> / <sub>32</sub> -32 x <sup>9</sup> / <sub>16</sub>	210-414
NUT, SWITCH, 12 SIDED	210-473
PANEL, FRONT	333-224
PLATE, BOTTOM .	387-559
PLATE, TOP	387-560
SCREW, 4-40 x $\frac{5}{16}$ PAN HS W/LOCKWASHER	211-033
SCREW, 6-32 x <sup>5</sup> / <sub>16</sub> BHS	211-507
SCREW, 6-32 x 3/4 BHS	211-514
SCREW, 6-32 × 7/₃ BHS	211-516
SCREW, 6-32 x <sup>5</sup> /16 PHS W/LOCKWASHER	211-534
SCREW, 6-32 x 1/4 FHS 100°, CSK, PHILLIPS	211-541
SCREW, 8-32 x ¾ OHS	
SCREW, THREAD FORMING $#4 \times \frac{1}{4}$ PHS PHILLIPS	213-088
SOCKET, STM7G	136-008

#### Mechanical Parts List (continued)

Tektronix Part Number

	Part Number
SOCKET, STB8R	136-012
SOCKET, STM9G	1 <b>36-01</b> 5
SOCKET, LIGHT JEWEL DRAKE	136-025
SPACER, NYLON MOLDED 3/32 FOR CERAMIC STRIP SN 220-up	361-007
STRIP, CERAMIC 3/4 × 11 NOTCHES 1/8 SPACING SN 101-219	124-015
STRIP, CERAMIC 3/4 x 11 NOTCHES, CLIP MTD. SN 220-up	124-091
TAG, VOLTAGE RATING	334-649
TUBE, SPACER .180 x $\frac{1}{4}$ x $\frac{1}{2}$ LG.	166-035
WASHER, STEEL 6L x ¾	210-803
WASHER, STEEL, FINISHING	210-832
WASHER, STEEL, .390 x %16 x .020	210-840
WASHER, RUBBER FOR FUSE HOLDER	210-873
WASHER, STEEL, FLAT $.470 \times \frac{21}{32} \times .030$	210-902

# Type 160A Mechanical Parts List

	Tektronix Part Number
ADAPTOR, POWER CORD, 3-WIRE TO 2-WIRE SN 3057-up	103-013
BAR RIGHT FRAME, W/1 THREADED HOLE	381-043
BAR LEFT FRAME, W/2 THREADED HOLES	381-044
BAR DD MOTOR, ALUM. $\frac{1}{8} \times \frac{3}{4} \times \frac{3}{4}$	381-045
BUSHING, ALUM. 3/8-32 x 9/16 x .412	358-010
CABINET BLUE WRINKLE FINISH SN 620-4399	437-029
CABINET BLUE VINYL FINISH SN 4400-up	437-052
CABLE HARNESS, POWER #1	179-083
CABLE HARNESS, POWER #2	179-084
CAP, FUSE	200-015
CHASSIS	441-097
CLAMP, CABLE, 3/16" PLASTIC	343-002
CONNECTOR CHASSIS MTD., 2 CONTACT MALE SN 620-3056	131-010
CONNECTOR CHASSIS MTD., 3 CONTACT MALE SN 3057-up	131-102
CORD POWER, 2 CONDUCTOR SN 620-3056	161-001
CORD POWER, 3 CONDUCTOR SN 3057-up	161-010
FAN, 3½ CLOCKWISE, ½" BORE	369-008
GROMMET RUBBER, 1/4	348-002
GROMMET RUBBER, 1/2	<b>348-00</b> 5
HOLDER, FUSE	352-010
LOCKWASHER INT. #4	210-004
LOCKWASHER INT. #6	210-006
LOCKWASHER INT. #10	210-010
LOCKWASHER INT. 3/8 x <sup>11</sup> / <sub>16</sub>	210-013
LUG, SOLDER, SE6, W/2 WIRE HOLES	210-202
NUT HEX 4-40 x <sup>3</sup> /16	210-406
NUT HEX 6-32 x ¼	210-407
NUT HEX <sup>15</sup> / <sub>32</sub> -32 × <sup>9</sup> / <sub>16</sub>	210-414
NUT KEPS 6-32 x <sup>5</sup> / <sub>16</sub>	210-457
NUT KEPS 8-32 x <sup>11</sup> / <sub>32</sub>	210-458
NUT 12 SIDED <sup>15</sup> / <sub>32</sub> -32 x <sup>5</sup> / <sub>64</sub>	210-473
NUT HEX $\frac{3}{8}-32 \times \frac{1}{2} \times \frac{1}{16}$	210-494
PANEL, FRONT	
PLATE, FRAME BACK, ALUM., .063 x 3 x 9 <sup>13</sup> / <sub>16</sub> x 3	

#### Mechanical Parts List (continued)

	Mechanical Parts List (continued)	Tektronix Part Number
SCREW	5-40 x ¾,6 PAN HS	211-029
SCREW	4-40 x <sup>5</sup> /16 PAN HS W/LOCKWASHER	211-033
SCREW	6-32 × ³/₀ BHS	211-510
SCREW	6-32 x ⁵/16 PAN HS W/LOCKWASHER	211-534
SCREW	6-32 × ⁵/16 FHS, 100°, CSK, PHILLIPS	211-538
SCREW	8-32 x <sup>3</sup> / <sub>8</sub> OHS	212-019
SCREW	8-32 × 1/2 TRUSS	212-045
SCREW	10-32 × <sup>3</sup> / <sub>8</sub> BHS	212-507
SCREW	THREAD FORMING 4-40 x 1/4 PHS, PHILLIPS	213-088
SOCKET	STM7G	136-008
SOCKET	STM8, GROUND	136-011
SOCKET	STM8, MOLDED	136-013
SOCKET	STM9G	316-015
SOCKET	LIGHT W/GREEN JEWEL	136-027
SPACER, N	NYLON, 5/16, FOR CERAMIC STRIP	361-009
STRIP C	CERAMIC, 3/4 × 7 NOTCHES, CLIP MOUNTED	124-089
STRIP (	CERAMIC, 3/4 x 11 NOTCHES, CLIP MOUNTED	124-091
TAG, VOL	TAGE RATING	334-649
WASHER	STEEL 6L x 3/8 x .032	210-803
WASHER	STEEL 8S × ¾ × ,032	210-804
WASHER	STEEL FINISHING #8	210-832
WASHER	RUBBER $\frac{1}{2} \times \frac{11}{16} \times \frac{3}{64}$ FOR FUSE HOLDER	210-873
WASHER	STEEL .470 x <sup>21</sup> / <sub>32</sub> x .030	210-902

# Type 161 Mechanical Parts List

Tektronix

	Part Number
BUSHING POT FRONT PANEL	35 <b>8-0</b> 10
BUSHING NYLON	358-036
CHASSIS (S/N 101-3193)	441-012
CHASSIS (S/N 3194-up)	441-267
GROMMET, RUBBER 1/4	348-002
KNOB RAW 4104	366-007
KNOB DIAL ASS'Y R/B 366-506 (S/N 101-1806)	366-506
KNOB DIAL ASS'Y R/B 366-525 (S/N 1807-4054)	366-522
KNOB DIAL ASS'Y R/B 366-525 (S/N 4055-up)	366-525
LOCKWASHER STEEL INT. #4	210-004
LOCKWASHER STEEL INT. #6	210-006
LOCKWASHER, STEEL INT., POT $\frac{3}{8} \times \frac{1}{2}$	210-012
LOCKWASHER STEEL INT., $\frac{3}{8} \times \frac{11}{16}$	210-013
LUG SOLDER SE6 W/2 WIRE HOLES	210-202
LUG SOLDER DE6	210-204
LUG SOLDER SE10, LONG	210-206
LUG SOLDER POT, PLAIN, 3/8	210-207
NUT HEX 4-40 x <sup>3</sup> / <sub>16</sub>	210-406
NUT HEX 6-32 x 1/4	210-407
NUT HEX 10-32 x 5/16	210-410
NUT HEX 3/8-32 × 1/2	210-413
NUT HEX <sup>15</sup> / <sub>32</sub> -32 x % <sub>16</sub>	210-414
NUT HEX BUSHING $\frac{3}{8}-32 \times \frac{1}{2} \times 1\frac{1}{16}$	210-429
NUT HEX $10-32 \times \frac{3}{8} \times \frac{1}{8}$	210-445
NUT KEPS 6-32 × ⁵/16	210-457
NUT 12-SIDED <sup>15</sup> / <sub>32</sub> -32 × <sup>5</sup> / <sub>64</sub>	210-473
NUT HEX 6-32 x <sup>5</sup> / <sub>16</sub> x .194 (5-10 W Resistor Mtg.)	210-478
NUT HEX $\frac{3}{8} - 32 \times \frac{1}{2} \times \frac{1}{16}$	210-494
PANEL FRONT (S/N 101-1375)	333-027
PANEL FRONT (S/N 1376-up & 1294)	333-294
PLATE FOR 8 PIN PLUG	<b>386-2</b> 51
PLATE SUB PANEL (S/N 101-1375)	386-294
PLATE SUB PANEL (S/N 1376-up & 1294)	386-581
PLATE FRAME BACK	426-019
PLUG, 8 PIN, OCTAL-MOLDED	134-006
POST BINDING, 5-WAY (S/N 101-1375)	129-001
POST BINDING, METAL CAP (S/N 1376-up & 1294)	129-020
POST BINDING, 5-WAY STEM & CAP ASS'Y	129-036
RING SOCKET RETAINING	354-002
Mechanical Parts List (continued)	
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	Tektronix Part Number
RING LOCKING	<b>3</b> 54- <b>0</b> 55
ROD NYLON, 5/16 x 15/16 TAPPED 6-32 THRU W/PIN	358-071
ROD DELRIN, 5/16 x 15/16 MTG. HOLE 3/8" DEEP W/2 CROSS HOLES	<b>358-13</b> 5
SCREW 4-40 x 3/8 RHS	211-013
SCREW 4-40 x 5/16 PAN HS W/LOCKWASHER	211-033
SCREW 6-32 x 5/16 BHS	211-507
SCREW 6-32 x 5/16 PAN HS W/LOCKWASHER	211-534
SCREW 6-32 x <sup>5</sup> / <sub>16</sub> 100°, CSK, PHILLIPS	211-538
SCREW 6-32 x 3/4 TRUSS HS, PHILLIPS	211-544
SCREW 8-32 x 3/8 OHS	212-019
SCREW THREAD CUTTING 6-32 x 3/8 TRUSS HS, PHILLIPS	213-041
SOCKET STM7G (S/N 101-3193)	136-008
SOCKET STM8, MOLDED	136-013
SOCKET STM9G (S/N 3194-up)	1 <b>36-0</b> 15
WASHER STEEL 6L x 3/8 x .032	210-803
WASHER STEEL FINISHING #8	210-832
WASHER STEEL .390 x $\gamma_{16}$ x .020	210-840
WASHER STEEL $.470 \times {}^{21}/_{32} \times .030$	210-902

# Type 162 Mechanical Parts List

	Tektronix Part Number
BUSHING ANODIZED ALUM.	358-010
BUSHING NYLON	358-036
CABLE, HARNESS	179-085
CHASSIS	441-013
KNOB, 4104	366-007
LOCKWASHER STEEL INT. #4	210-004
LOCKWASHER STEEL INT. #6	210-006
LOCKWASHER STEEL INT. #10	210-010
LOCKWASHER STEEL INT. POT, $\frac{3}{8} \times \frac{1}{2}$	210-012
LOCKWASHER STEEL INT. 3/8 x 11/16	210-013
LUG SOLDER SE6 W/2 WIRE HOLES	210-202
LUG SOLDER SE10, LONG	210-206
NUT HEX 4-40 x <sup>3</sup> / <sub>16</sub>	210-406
NUT HEX 6-32 x 1/4	210-407
NUT HEX 10-32 x 5/16	210-410
NUT HEX 3/8-32 x 1/2	210-413
NUT HEX 15/32-32 x 9/16	210-414
NUT HEX 10-32 x ¾ x ⅓	210-445
NUT KEPS 6-32 x <sup>5</sup> / <sub>16</sub>	210-457
NUT 12-SIDED, <sup>15</sup> / <sub>32</sub> -32 x <sup>5</sup> / <sub>64</sub>	210-473
NUT HEX 6-32 x <sup>5</sup> / <sub>16</sub> x .194 (5-10 W Resistor Mtg.)	210-478
NUT HEX 3/8-32 x 1/2 x 11/16	210-494
PANEL FRONT (S/N 101-1610)	333-029
PANEL FRONT (S/N 1611-up)	333-295
PLATE FOR 8 PIN PLUG	386-251
PLATE SUB PANEL (S/N 101-1610)	386-295
PLATE SUB PANEL (S/N 1611-up)	386-582
PLATE FRAME BACK	426-019
PLUG, 8 PIN, OCTAL-MOLDED	134-006
POST BINDING HEX CAP (S/N 101-1610)	129-001
POST BINDING PLATED (S/N 1611-up)	1 <b>29-02</b> 0
POST BINDING FLUTED	129-036
RING RETAINING (For Socket)	354-002
RING LOCKING SWITCH	354-055
ROD, DELRIN, 5/16 x 15/16 W/2 CROSS HOLES	385-135
SCREW 4-40 x <sup>5</sup> /16 PAN HS W/LOCKWASHER	211-033
SCREW 6-32 x <sup>3</sup> / <sub>16</sub> BHS	211-503
SCREW 6-32 x 5/16 PAN HS W/LOCKWASHER	211-534

## Mechanical Parts List (continued)

Tektronix Part Number

SCREW 6-32 x <sup>5</sup> /16 FHS, 100°, CSK, PHILLIPS	211-538
SCREW 6-32 x 3/4 TRUSS HS, PHILLIPS	211-544
SCREW 8-32 × 3/8 OHS	212-019
SCREW THREAD CUTTING, 6-32 x 3/8 TRUSS HS, PHILLIPS	213-041
SOCKET STM7G	136-008
SOCKET STM8, MOLDED	136-013
SOCKET STM9G	136-015
WASHER STEEL $6L \times \frac{3}{8} \times .032$	210-803
WASHER STEEL FINISHING #8	210-832
WASHER STEEL .390 x %16 x .020	210-840
WASHER STEEL $.470 \times {}^{21}/_{32} \times .030$	210-902

# Type 163 Mechanical Parts List

	Te <b>ktro</b> nix Part Number
BUSHING ANODIZED ALUM.	358-010
BUSHING NYLON	358-036
CABLE, HARNESS SN 101-909	179-128
CHASSIS	441-014
FRAME, BACK	426-020
GROMMET, RUBBER, 3/8"	348-004
KNOB RAW, 4104 (BLACK)	366-007
KNOB DIAL ASS'Y SN 101-1698	366-506
KNOB DIAY ASS'Y SN 1699-2889	366-523
KNOB DIAL ASS'Y SN 1699-up	366-524
KNOB DIAL ASS'Y SN 2890-up	366-525
LOCKWASHER STEEL INT. #4	210-004
LOCKWASHER STEEL INT. #6	210-006
LOCKWASHER STEEL INT. #10	210-010
LOCKWASHER STEEL INT. POT. $\frac{3}{8} \times \frac{1}{2}$	210-012
LOCKWASHER STEEL INT. ¾ x 11/16	210-013
LUG SOLDER SE6 W/2 WIRE HOLES	210-202
LUG SOLDER SE10 LONG	210-206
LUG SOLDER POT PLAIN, 3/8	210-207
NUT HEX 4-40 x 3/16	210-406
NUT HEX 6-32 x ¼	210-407
NUT HEX 10-32 x ⁵/16	210-410
NUT HEX 3/8-32 x 1/2	210-413
NUT HEX <sup>15</sup> / <sub>32</sub> -32 x <sup>9</sup> / <sub>16</sub>	210-414
NUT HEX BUSHING, 3/8-32 x 1/2 x 1 1/16	210-429
NUT HEX 10-32 x ¾ x ½	210-445
NUT KEPS 6-32 x <sup>5</sup> /16	210-457
NUT 12 SIDED, <sup>15</sup> / <sub>32</sub> -32 × <sup>5</sup> / <sub>64</sub>	210-473
NUT HEX 6-32 x 5/16 x .194 (5-10 W RESISTOR MTG.)	210-478
NUT HEX $\frac{3}{8}-32 \times \frac{1}{2} \times \frac{11}{16}$	210-494
PANEL FRONT SN 101-866	333-030
PANEL FRONT SN 867-up	333-296
PLATE FOR 8 PIN PLUG	386-251
PLATE SUB PANEL SN 101-1435	386-296

### **Mechanical Parts List** (continued)

Tektronix

	Part Number
PLATE SUB PANEL SN 1436-up	386-583
PLUG, 8 PIN, OCTAL-MOLDED	134-006
POST BINDING HEX CAP SN 101-1435	129-001
POST BINDING PLATE SN 1436-up	129-020
POST BINDING FLUTED CAP	129-036
RING SOCKET RETAINING	354-002
RING LOCKING SWITCH	354-055
SCREW 4-40 x <sup>5</sup> / <sub>16</sub> PAN HS W/LOCKWASHER	211-033
SCREW 6-32 x <sup>5</sup> / <sub>16</sub> BHS	211-507
SCREW 6-32 x 5/16 PAN HS W/LOCKWASHER	211-534
SCREW 6-32 x 5/16 FHS, 100°, CSK, PHILLIPS	211-538
SCREW 6-32 x 3/4 TRUSS HS, PHILLIPS	211-544
SCREW 8-32 x 3/8 OHS	212-019
SOCKET STM7G	136-008
SOCKET STM8, GROUND	136-013
SOCKET STM9G	136-015
STRIP CERAMIC 3/4 x 7 NOTCHES, CLIP MOUNTED	124-089
STRIP CERAMIC 3/4 x 11 NOTCHES, CLIP MOUNTED	124-091
WASHER STEEL 6L × 3/8 × .039	210-803
WASHER STEEL FINISHING #8	210-832
WASHER STEEL .390 x %16 x .020	210-840
WASHER STEEL .470 x <sup>21</sup> / <sub>32</sub> x .030	210-902

# Type 360 Mechanical Parts List

Tektronix

	Part Number					
BAR, 3/8 x 3/8 x 133/16 TAPPED 6-32 BOTH ENDS	381-049					
BAR, 3/8 x 3/8 x 133/16 W/2 PINS AND 3 6-32 HOLES	381-050					
BAR, 3/8 x 3/8 x 133/16 W/2 PINS AND FRAME	381-051					
BRACKET, 3 POT MTG., .063 x 2 <sup>11</sup> / <sub>32</sub> x 17/ <sub>8</sub>	406-162					
BRACKET, CAP. MTG., .063 × 35/8 × 47/8 × 1/2 SN 101-1000	406-163					
BRACKET, CAP. MTG., .063 x 21/16 x 47/8 x 1/2 SN 1001-up	<b>406-38</b> 5					
BUSHING, NYLON, INS. FOR 5-WAY BINDING POST	358-036					
CABINET, BLUE WRINKLE SN 101-1949	437-032					
CABINET, BLUE VINYL SN 1950-up	437-054					
CABLE, HARNESS, MAIN SN 101-1000	179-095					
CABLE, HARNESS, IND. SN 1001-up	179-244					
CABLE, HARNESS, SUBPANEL SN 101-1000	179-096					
CABLE, HARNESS, F & I SN 101-1000	1 <b>79-09</b> 7					
CABLE, HARNESS, F & I SN 1001-up	17 <b>9-2</b> 47					
CHASSIS SN 1001-up	<b>441-20</b> 7					
CLAMP, CABLE, 1/2" PLASTIC	343-006					
CLAMP, CRT SOCKET, 17/16" DIA.						
CONNECTOR, CHASSIS MTD.	131-038					
COUPLING, POT	376-014					
COVER, GRATICULE	200-073					
FELT, GRAY	124-050					
FILTER, LIGHT, PLEXIGLAS, GREEN	378-509					
GRATICULE, 3", 8 VERT. 10 HORIZONTAL	331-027					
GROMMET, RUBBER, 1/4	348-002					
GROMMET, RUBBER, 5/16	348-003					
GROMMET, RUBBER, 3/8	348-004					
GROMMET, RUBBER, 1/2						
GROMMET, RUBBER, 5/8						
KNOB, LARGE BLACK, ¼ HOLE THRU	366-029					
KNOB, LARGE BLACK, .265 HOLE THRU	366-030					
KNOB, SMALL RED, 1/8 HOLE PART WAY						
KNOB, SMALL RED, 3/16 HOLE PART WAY						
KNOB, SMALL BLACK, 1/4 HOLE PART WAY						
LOCKWASHER, INT. #4	210-004					

LOCKWASHER, INT. #10   210-0     LOCKWASHER, INT. //   210-0     LOCKWASHER, INT. //   210-0     LOCKWASHER, INT., POT, $\frac{3}{6} \times \frac{1}{2}$ 210-0     LOCKWASHER, INT., $\frac{3}{6} \times \frac{1}{2}$ 210-0     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, POT, PLAIN, $\frac{3}{6}$ 210-2     NUT, HEX, 4-40 × $\frac{3}{16}$ 210-4     NUT, HEX, 4-40 × $\frac{3}{16}$ 210-4     NUT, HEX, $\frac{4}{3}$ , $\frac{2}{3}$ , $\frac{3}{2}$ 210-4     NUT, HEX, $\frac{1}{3}$ , $\frac{2}{3}$ , $\frac{2}{3}$ , $\frac{2}{3}$ 210-4     NUT, KNURLED, GRATICULE, 10-32, $\frac{5}{15}$ , $\frac{3}{16}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   333-4     PLATE, FONT SN 515-up   336-6 <t< th=""><th></th><th></th></t<>		
LOCKWASHER, INT. $1/4$ 210-0     LOCKWASHER, INT., POT, $3/6 \times 1/2$ 210-0     LOCKWASHER, INT., $3/6 \times 1/2_6$ 210-0     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, POT, PLAIN, $3/6$ 210-2     NUT, HEX, $4-40 \times 3/16$ 210-4     NUT, HEX, $4-40 \times 3/16$ 210-4     NUT, HEX, $1/2_{32} \times 2/2_{33}$ 210-4     NUT, HEX, $1/2_{32} \times 3/16 \times 1/2_{32}$ 210-4     NUT, HEX, $1/2_{32} \times 3/16 \times 3/12_{32}$ 210-4     NUT, HEX, $1/2_{32} \times 3/16 \times 3/16_{32}$ 210-4     NUT, KNURLED, GRATICULE, $10.32 \times .515 \times 3/6$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   333-4     PLATE, FOR 8 PIN PLUG   386-62     PLATE, FRAME, $.080 \times 3/7_6 \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASSY (HEX CAP) SN 101-1409	LOCKWASHER, INT. #6	21 <b>0-00</b> 6
LOCKWASHER, INT., POT, $\frac{1}{6} \times \frac{1}{2}$ 210-0     LOCKWASHER, INT., $\frac{3}{6} \times \frac{1}{16}$ 210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, POT, PLAIN, $\frac{9}{6}$ 210-2     NUT, HEX, 4-40 × $\frac{3}{16}$ 210-4     NUT, HEX, 6-32 × $\frac{1}{4}$ 210-4     NUT, HEX, 6-32 × $\frac{1}{4}$ 210-4     NUT, HEX, 10-32 × $\frac{9}{16}$ × $\frac{1}{9}$ 210-4     NUT, HEX, 10-32 × $\frac{1}{16}$ 210-4     NUT, KNURLED, GRATICULE, 10-32 × $\frac{1}{10}$ 210-4     NUT, SQUARE, 10-32 × $\frac{1}{16}$ 210-4     NUT, SQUARE, 10-32 × $\frac{1}{16}$ 210-5     PANEL, FRONT SN 151-5up   333-4     PLATE, FOR 8 PIN PLUG   386-2     PLATE, FRAME, 080 × $\frac{3}{16}$ × 10   36-3     PLATE, FRAME, 080 × $\frac{3}{16}$ × 10   37-5	LOCKWASHER, INT. #10	210-010
LOCKWASHER, INT, $\frac{3}{2} \times \frac{1}{14}$ 210-0     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, POT, PLAIN, $\frac{3}{6}$ 210-2     NUT, HEX, 4-40 $\times \frac{3}{16}$ 210-4     NUT, HEX, 4-40 $\times \frac{3}{16}$ 210-4     NUT, HEX, 6-32 $\times \frac{1}{4}$ 210-4     NUT, HEX, 6-32 $\times \frac{1}{4}$ 210-4     NUT, HEX, 10-32 $\times \frac{3}{16} \times \frac{1}{9}$ 210-4     NUT, HEX, 10-32 $\times \frac{1}{4}$ 210-4     NUT, HEX, 6-32 $\times \frac{1}{4}$ 210-4     NUT, HEX, 10-32 $\times \frac{1}{4}$ 210-4     NUT, KNURLED, GRATICULE, 10-32 $\times .515 \times \frac{3}{6}$ 210-4     NUT, SQUARE, 10-32 $\times \frac{3}{4}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 151-5up   333-4     PLATE, FOR 8 PIN PLUG   386-3     PLATE, FRAME, 080 $\times \frac{3}{6} \times 10$ 36-6     PLATE, FRAME, 080 $\times \frac{3}{6} \times 10$ 370-5     PLATE, FRA	LOCKWASHER, INT. 1/4	210-011
LUG, SOLDER, SE4   210-2     LUG, SOLDER, SE6 W/2 WIRE HOLES   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, POT, PLAIN, $\frac{9}{6}$ 210-2     NUT, HEX, 4-40 $\frac{3}{16}$ 210-4     NUT, HEX, 4-40 $\frac{3}{16}$ 210-4     NUT, HEX, 6-32 $\frac{1}{4}$ 210-4     NUT, HEX, 6-32 $\frac{3}{16}$ 210-4     NUT, HEX, 10-32 $\frac{3}{2} \frac{1}{2}$ 210-4     NUT, HEX, 6-32 $\frac{3}{16} \frac{1}{2}$ 210-4     NUT, HEX, 6-32 $\frac{3}{16} \frac{1}{2}$ 210-4     NUT, HEX, 6-32 $\frac{3}{16} \frac{1}{2}$ 210-4     NUT, KNURLED, GRATICULE, 10-32 $\frac{1}{2} \frac{1}{2}$ 210-4     NUT, SQUARE, 10-32 $\frac{3}{16} \frac{1}{2}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 151-up   334-4     PLATE, FOR 8 PIN PLUG   386-2     PLATE, FRAME, 0.080 $\frac{3}{16} \frac{1}{10} \frac{3}{16} \frac{1}{16} \frac{1}{16} \frac{3}{10} \frac{36}{10} \frac{36}$	LOCKWASHER, INT., POT, $\frac{3}{8} \times \frac{1}{2}$	210-012
LUG, SOLDER, SE6 W/2 WIRE HOLES   210-2     LUG, SOLDER, SE10, LONG   210-2     LUG, SOLDER, POT, PLAIN, $\frac{3}{6}$ 210-2     NUT, HEX, 4-40 × $\frac{3}{16}$ 210-4     NUT, HEX, 6-32 × $\frac{1}{2}$ 210-4     NUT, HEX, $\frac{4}{92}$ 210-4     NUT, HEX, $\frac{4}{92}$ 210-4     NUT, HEX, $\frac{4}{92}$ 22     NUT, HEX, $\frac{1}{92}$ 32 × $\frac{1}{2}$ NUT, HEX, $\frac{1}{92}$ 32 × $\frac{1}{16}$ NUT, HEX, $1-32 \times \frac{3}{8} \times \frac{1}{8}$ 210-4     NUT, HEX, $6-32 \times \frac{3}{8} \times \frac{3}{322}$ 210-4     NUT, KIURLED, GRATICULE, $10-32 \times .515 \times \frac{3}{6}$ 210-4     NUT, SQUARE, $10-32 \times \frac{3}{8} \times \frac{3}{22} \times \frac{5}{44}$ 210-4     NUT, SQUARE, $10-32 \times \frac{3}{8} \times \frac{10}{22} \times \frac{5}{24} \times \frac{210-5}{20}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   333-4     PLATE, SUBPANEL   386-3     PLATE, SUBPANEL   386-3     PLATE, FRAME, $0.80 \times 3\frac{3}{8} \times 10$ 387-5     PLUG, 8	LOCKWASHER, INT., 3/8 x <sup>11</sup> /16	210-013
LUG, SOLDER, SEIO, LONG   210-2     LUG, SOLDER, POT, PLAIN, $\frac{3}{6}$ 210-2     NUT, HEX, 4-40 × $\frac{3}{16}$ 210-4     NUT, HEX, $\frac{4}{6}$ × $\frac{3}{2}$ × $\frac{1}{4}$ 210-4     NUT, HEX, $\frac{4}{9}$ × $\frac{3}{2}$ × $\frac{1}{2}$ 210-4     NUT, HEX, $\frac{1}{9}$ × $\frac{3}{2}$ × $\frac{1}{2}$ 210-4     NUT, HEX, $\frac{1}{9}$ × $\frac{3}{2}$ × $\frac{1}{2}$ 210-4     NUT, HEX, $\frac{1}{9}$ × $\frac{3}{8}$ × $\frac{1}{9}$ 210-4     NUT, HEX, $\frac{1}{9}$ × $\frac{3}{8}$ × $\frac{1}{9}$ 210-4     NUT, HEX, $\frac{1}{2}$ × $\frac{3}{6}$ × $\frac{3}{9}$ 210-4     NUT, HEX, $\frac{1}{2}$ × $\frac{3}{8}$ × $\frac{1}{9}$ 210-4     NUT, HEX, $\frac{1}{2}$ × $\frac{3}{8}$ × $\frac{1}{9}$ 210-4     NUT, HEX, $\frac{1}{2}$ × $\frac{3}{8}$ × $\frac{3}{9}$ 210-4     NUT, KNURLED, GRATICULE, $10$ × $\frac{2}{10}$ × $\frac{515}{8}$ 210-4     NUT, KNURLED, GRATICULE, $10.32$ × $.515$ × $\frac{3}{6}$ 210-4     NUT, SQUARE, $10.32$ × $\frac{3}{9}$ 210-5     PANEL, FRONT SN 101-514   233-1     PANEL, FRONT SN 515-up   336-4     PLATE, SUBPANEL   386-3	LUG, SOLDER, SE4	210-201
LUG, SOLDER, POT, PLAIN, $\frac{3}{6}$ 210-2     NUT, HEX, 4-40 × $\frac{3}{16}$ 210-4     NUT, HEX, 6-32 × $\frac{1}{2}$ 210-4     NUT, HEX, $\frac{1}{52}$ , $\frac{32}{2}$ × $\frac{1}{2}$ 210-4     NUT, HEX, $\frac{1}{12}$ , $\frac{1}{23}$ × $\frac{3}{8}$ × $\frac{3}{22}$ 210-4     NUT, HEX, $\frac{1}{2}$ , $\frac{2}{2}$ × $\frac{3}{16}$ × $\frac{3}{22}$ 210-4     NUT, HEX, $\frac{1}{2}$ , $\frac{2}{28}$ × $\frac{3}{16}$ × $\frac{3}{22}$ 210-4     NUT, KNURLED, GRATICULE, 10-32 × .515 × $\frac{3}{16}$ 210-4     NUT, KNURLED, GRATICULE, 10-32 × .515 × $\frac{3}{6}$ 210-4     NUT, SQUARE, 10-32 × $\frac{3}{6}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   333-4     PLATE, SUBPANEL   386-3     PLATE, SUBPANEL   386-3     PLATE, FRAME, 0.80 × $\frac{3}{6}$ × 10   387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASSY (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASSY (FLUTED CAP) SN 1410-up   129-0     POST, BINDING, SWITCH <sup>23</sup> / <sub>23</sub> × <sup>15</sup> / <sub>32</sub> </td <td>LUG, SOLDER, SE6 W/2 WIRE HOLES</td> <td>210-202</td>	LUG, SOLDER, SE6 W/2 WIRE HOLES	210-202
NUT, HEX, 4-40 x $\frac{3}{16}$ 210-4     NUT, HEX, 6-32 x $\frac{1}{4}$ 210-4     NUT, HEX, $\frac{3}{9}$ -32 x $\frac{1}{4}$ 210-4     NUT, HEX, $\frac{3}{9}$ -32 x $\frac{1}{4}$ 210-4     NUT, HEX, $\frac{1}{9}$ -32 x $\frac{1}{9}$ 210-4     NUT, KIURLED, GRATICULE, $10-32$ x $\frac{515}{9}$ 210-4     NUT, SQUARE, $10-32$ x $\frac{3}{9}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   33-4     PLATE, FOR 8 PIN PLUG   386-3     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16}$ x $5^{15}/16$ x $10^{14}$ SN 101-1000   386-42     PLATE, FRAME, $0.60 \times 37_{6} \times 10$ 387-5     PLUG, 8 PIN, DCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASSY (HEX CAP) SN 101-1409   129-0     POST, BINDING, ASSY (METAL)	LUG, SOLDER, SE10, LONG	210-206
NUT, HEX, $6.32 \times \frac{1}{4}$ 210.4     NUT, HEX, $\frac{9}{4}-32 \times \frac{1}{4}$ 210.4     NUT, HEX, $\frac{19}{32}-32 \times \frac{1}{16}$ 210.4     NUT, HEX, $1\frac{19}{32}-32 \times \frac{1}{16}$ 210.4     NUT, HEX, $1\frac{19}{32}-32 \times \frac{1}{6} \times \frac{1}{6}$ 210.4     NUT, HEX, $10-32 \times \frac{1}{9} \times \frac{1}{9} \times \frac{1}{9}$ 210.4     NUT, HEX, $10-32 \times \frac{1}{9} \times \frac{1}{9} \times \frac{1}{9}$ 210.4     NUT, HEX, $(-3.32 \times \frac{1}{9} \times \frac{1}$	LUG, SOLDER, POT, PLAIN, 3/8	210-207
NUT, HEX, $3_{6}-32 \times 1/2$ 210.4     NUT, HEX, $1^{4}/_{32}-32 \times 7/_{16}$ 210.4     NUT, HEX, $1^{-5}/_{32}-32 \times 7/_{16}$ 210.4     NUT, HEX, $1^{-2}/_{32} \times 3/_{8} \times 1/_{8}$ 210.4     NUT, HEX, $10-32 \times 3/_{8} \times 1/_{8}$ 210.4     NUT, HEX, $1/_{4}-28 \times 3/_{8} \times 3/_{32}$ 210.4     NUT, KNURLED, GRATICULE, 10-32 $\times .515 \times 3/_{8}$ 210.4     NUT, SQUARE, 10-32 $\times 3/_{8} \times 1.94$ 210.4     NUT, SQUARE, 10-32 $\times 3/_{8}$ 210.5     PANEL, FRONT SN 101-514   333.1     PANEL, FRONT SN 515-up   333.4     PLATE, FOR 8 PIN PLUG   386-3     PLATE, SUBPANEL   386-3     PLATE, FOR 8 PIN PLUG   387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $^{-2}_{3}/_{32} \times 1^{5}/_{32}$ 364-0     ROD, S/16 KIS, PHILLIPS   211-0	NUT, HEX, 4-40 x <sup>3</sup> / <sub>16</sub>	210-406
NUT, HEX, $1^{5}/_{32}-32 \times 7/_{16}$ 210-4     NUT, HEX, $1^{-5}/_{32}-32 \times 7/_{16}$ 210-4     NUT, HEX, $10-32 \times 3/_{8} \times 1/_{8}$ 210-4     NUT, HEX, $1/_{4}-28 \times 3/_{8} \times 3/_{32}$ 210-4     NUT, HEX, $7/_{4}-28 \times 3/_{8} \times 1.94$ (5-10 W RES. MTG.)   210-4     NUT, KNURLED, GRATICULE, $10-32 \times .515 \times 3/_{8}$ 210-4     NUT, SQUARE, $10-32 \times 3/_{8} \times 1.94$ 210-4     NUT, SQUARE, $10-32 \times 3/_{8}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   33-4     PLATE, FOR 8 PIN PLUG   386-3     PLATE, SUBPANEL   386-3     PLATE, FRAME, $.080 \times 3/_{8} \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $2^{3}_{32} \times 1^{5}_{32}$ 364-0     ROD, PLUON, $5/_{16} \times 3^{3}_{32}$ 384-0     ROD, NYLON, $5/_{16} \times 3^{3}_{32}$ 384-0     ROD, NYLON, $5/_{16} \times 3^{3}_{32}$ 384-0     SCREW, $4.40 \times 5/_{16}$ FHS,	NUT, HEX, 6-32 × ¼	210-407
NUT, HEX, 10-32 $\times \frac{3}{9} \times \frac{1}{8}$ 210.4     NUT, HEX, 10-32 $\times \frac{3}{9} \times \frac{1}{8}$ 210.4     NUT, HEX, 10-32 $\times \frac{3}{9} \times \frac{1}{9} \times \frac{3}{32}$ 210.4     NUT, HEX, 6-32 $\times \frac{5}{16} \times .194$ (5-10 W RES. MTG.)   210.4     NUT, KNURLED, GRATICULE, 10-32 $\times .515 \times \frac{3}{8}$ 210.4     NUT, I2 SIDED, SWITCH, $\frac{15}{32} \cdot 32 \times \frac{5}{64}$ 210.4     NUT, SQUARE, 10-32 $\times \frac{3}{8}$ 210.4     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   336-2     PLATE, FOR 8 PIN PLUG   386-3     PLATE, FOR 8 PIN PLUG   386-3     PLATE, FRAME, .080 $\times 37_6 \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASSY (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASSY (FLUTED CAP) SN 1410-up   129-0     POST, BINDING, SSWITCH $\frac{23}{52} \times \frac{15}{32}$ 354-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $\frac{23}{52} \times \frac{15}{32}$ 364-0     ROD, NYLON, $\frac{5}{16} \times \frac{14}{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 $\times \frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, 4-32 $\times \frac{14}{8}$ BHS   211-0	NUT, HEX, 3/8-32 × 1/2	210-413
NUT, HEX, $1/4 - 28 \times 3/8 \times $	NUT, HEX, <sup>15</sup> / <sub>32</sub> -32 x <sup>9</sup> / <sub>16</sub>	210-414
NUT, HEX, $6.32 \times \frac{5}{16} \times .194$ (5-10 W RES. MTG.)   210.4     NUT, KNURLED, GRATICULE, $10.32 \times .515 \times \frac{3}{6}$ 210.4     NUT, 12 SIDED, SWITCH, $\frac{15}{32}.32 \times \frac{5}{64}$ 210.4     NUT, SQUARE, $10.32 \times \frac{3}{6}$ 210.5     PANEL, FRONT   SN 101-514   333-1     PANEL, FRONT   SN 101-514   333-1     PANEL, FRONT   SN 515-up   336-2     PLATE, FOR 8 PIN PLUG   386-3     PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15}/_{16} \times 10^{1/4}$ SN 101-1000     PLATE, FRAME, $.080 \times 3\frac{7}{8} \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0   354-0     RING, LOCKING SWITCH $\frac{29}{32} \times \frac{15}{32}$ 384-0   384-0     ROD, NYLON, $\frac{5}{16} \times 1\frac{9}{6}$ , TAPPED 6-32 ONE END SN 1001-up   385-1   384-0     SCREW, $4.40 \times \frac{5}{16}$ , FHS, PHILLIPS   211-0   211-0     SCREW, $6.32 \times \frac{1}{4}$ BHS   211-5   211-5	NUT, HEX, 10-32 × 3/8 × 1/8	210-445
NUT, KNURLED, GRATICULE, 10-32 x .515 x $\frac{3}{6}$ 210-4     NUT, 12 SIDED, SWITCH, $\frac{15}{32}$ -32 x $\frac{5}{64}$ 210-4     NUT, SQUARE, 10-32 x $\frac{3}{6}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   334     PLATE, FOR 8 PIN PLUG   386-2     PLATE, SUBPANEL   386-3     PLATE, SUBPANEL   386-3     PLATE, FRAME, .080 x $\frac{3}{6}$ x 10   387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP) SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     RING, LOCKING SWITCH $\frac{29}{32} \times \frac{15}{32}$ 384-0     ROD, EXTENSION, $\frac{1}{6}$ x $\frac{11}{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 x $\frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, 6-32 x $\frac{1}{4}$ BHS   211-5	NUT, HEX, ¼-28 × ¾ × ¾	<b>210-4</b> 55
NUT, 12 SIDED, SWITCH, $15/32-32 \times 5/64$ 210.4     NUT, SQUARE, 10-32 × $3/6$ 210.5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   333-4     PLATE, FOR 8 PIN PLUG   386-2     PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, $1/16 \times 5^{15}/16 \times 10^{1/4}$ SN 101-1000   386-4     PLATE, FRAME, .080 x $37/6 \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP) SN 1410-up   129-0     POST, BINDING, S-WAY ASS'Y (METAL) SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, SOCKET, RETAINING   354-0     ROD, EXTENSION, $1/8 \times 3^{3}/32$ 384-0     ROD, NYLON, $5/16 \times 11/6$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $4-40 \times 5/16$ FHS, PHILLIPS   211-0     SCREW, $6-32 \times 1/4$ BHS   211-5	NUT, HEX, 6-32 x <sup>5</sup> / <sub>16</sub> x .194 (5-10 W RES. MTG.)	210-478
NUT, SQUARE, 10-32 x $\frac{3}{8}$ 210-5     PANEL, FRONT SN 101-514   333-1     PANEL, FRONT SN 515-up   333-4     PLATE, FOR 8 PIN PLUG   386-2     PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16}$ x 51 $\frac{5}{16}$ x 10 $\frac{1}{4}$ SN 101-1000   386-4     PLATE, FRAME, .080 x $3\frac{7}{16}$ x 10   387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $\frac{23}{32} \times \frac{15}{32}$ 354-0     ROD, EXTENSION, $\frac{1}{8} \times 3\frac{3}{32}$ 384-0     ROD, NYLON, $\frac{5}{16} \times 1\frac{1}{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	NUT, KNURLED, GRATICULE, 10-32 x .515 x $\frac{3}{8}$	210-434
PANEL, FRONT   SN 101-514   333-1     PANEL, FRONT   SN 515-up   333-4     PLATE, FOR 8 PIN PLUG   386-2     PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15} \frac{1}{16} \times 10^{1/4}$ SN 101-1000     PLATE, FRAME, .080 $\times 37_8 \times 10$ 387-55     PLUG, 8 PIN, OCTAL-MOLDED   134-00     POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up     POST, BINDING, ASS'Y (METAL)   SN 1410-up     POST, BINDING, ASS'Y (METAL)   SN 1410-up     POST, BINDING, ASS'Y (METAL)   SN 1410-up     RING, SOCKET, RETAINING   354-00     ROD, EXTENSION, $\frac{1}{8} \times 3^3_{52}$ 384-00     ROD, NYLON, $\frac{5}{16} \times 1\frac{1}{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-11     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	NUT, 12 SIDED, SWITCH, <sup>15</sup> / <sub>32</sub> -32 × <sup>5</sup> / <sub>64</sub>	210-473
PANEL, FRONT   SN 515-up   333-4     PLATE, FOR 8 PIN PLUG   386-2     PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15}/_{16} \times 10^{1/4}$ SN 101-1000     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15}/_{16} \times 10^{1/4}$ SN 101-1000     PLATE, FRAME, .080 $\times 37_6 \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up     POST, BINDING, ASS'Y (METAL)   SN 1410-up     POST, BINDING, ASS'Y (METAL)   SN 1410-up     POST, BINDING, SWITCH $^{23}/_{32} \times ^{15}/_{32}$ 354-0     RING, LOCKING SWITCH $^{23}/_{32} \times ^{15}/_{32}$ 384-0     ROD, EXTENSION, $\frac{1}{6} \times 3^{3}/_{32}$ 384-0     ROD, NYLON, $\frac{5}{16} \times 11/_8$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-0     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	NUT, SQUARE, 10-32 x 3/8	210-501
PLATE, FOR 8 PIN PLUG   386-2     PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, 1/16 × 515/16 × 101/4   SN 101-1000     PLATE, FRAME, .080 × 37/8 × 10   387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up     POST, BINDING, ASS'Y (METAL)   SN 1410-up     RING, LOCKING SWITCH 23/32 × 15/32   354-0     ROD, EXTENSION, 1/8 × 33/32   384-0     ROD, NYLON, 5/16 × 11/8, TAPPED 6-32 ONE END   SN 1001-up     SCREW, 4-40 × 5/16 FHS, PHILLIPS   211-0     SCREW, 6-32 × 1/4 BHS   211-5	PANEL, FRONT SN 101-514	333-133
PLATE, SUBPANEL   386-3     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15} \frac{1}{16} \times 10^{1} \frac{1}{2}$ SN 101-1000   386-4     PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15} \frac{1}{16} \times 10^{1} \frac{1}{2}$ SN 101-1000   386-4     PLATE, FRAME, .080 x $3\frac{7}{8} \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP) SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $\frac{23}{32} \times \frac{15}{32}$ 354-0     ROD, EXTENSION, $\frac{1}{8} \times 3^{3}/_{32}$ 384-0     ROD, NYLON, $\frac{5}{16} \times 11^{1}_{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $4-40 \times \frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	PANEL, FRONT SN 515-up	333-422
PLATE, ETCHED CQT., FORMICA, $\frac{1}{16} \times 5^{15}/_{16} \times 10^{1}/_{4}$ SN 101-1000   386-4     PLATE, FRAME, .080 × $3\frac{7}{8} \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP) SN 1410-up   129-0     POST, BINDING, 5-WAY ASS'Y (METAL) SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL) SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $\frac{23}{32} \times \frac{15}{32}$ 354-0     ROD, EXTENSION, $\frac{1}{8} \times 3^{3}/_{32}$ 384-0     ROD, NYLON, $\frac{5}{16} \times 11/8$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $4-40 \times \frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	PLATE, FOR 8 PIN PLUG	386-251
PLATE, FRAME, .080 x $37_8 \times 10$ 387-5     PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up   129-0     POST, BINDING, 5-WAY ASS'Y (METAL)   SN 1410-up   129-0     POST, BINDING, S-WAY ASS'Y (METAL)   SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $^{23}/_{32} \times ^{15}/_{32}$ 354-0     ROD, EXTENSION, $\frac{1}{8} \times 3^{3}/_{32}$ 384-0     ROD, NYLON, $\frac{5}{16} \times 11/_8$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $4-40 \times \frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	PLATE, SUBPANEL	386-397
PLUG, 8 PIN, OCTAL-MOLDED   134-0     POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL)   SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL)   SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $^{23}/_{32} \times ^{15}/_{32}$ 354-0     ROD, EXTENSION, $1/_8 \times 3^3/_{32}$ 384-0     ROD, NYLON, $5/_{16} \times 11/_8$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, $4-40 \times 5/_{16}$ FHS, PHILLIPS   211-0     SCREW, $6-32 \times 1/_4$ BHS   211-0	PLATE, ETCHED CQT., FORMICA, 1/16 x 515/16 x 101/4 SN 101-1000	386-441
POST, BINDING, 5-WAY ASS'Y (HEX CAP)   SN 101-1409   129-0     POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL)   SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $^{23}/_{32} \times ^{15}/_{32}$ 354-0     ROD, EXTENSION, $\frac{1}{8} \times 3^{3}/_{32}$ 384-0     ROD, NYLON, $\frac{5}{16} \times 1\frac{1}{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 × $\frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, 6-32 × $\frac{1}{4}$ BHS   211-5	PLATE, FRAME, .080 x 37/8 x 10	387-546
POST, BINDING, 5-WAY ASS'Y (FLUTED CAP)   SN 1410-up   129-0     POST, BINDING, ASS'Y (METAL)   SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH $2^{3}/_{32} \times 1^{5}/_{32}$ 354-0     ROD, EXTENSION, $1/_{8} \times 3^{3}/_{32}$ 384-0     ROD, NYLON, $5/_{16} \times 11/_{8}$ , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 $\times 5/_{16}$ FHS, PHILLIPS   211-0     SCREW, 6-32 $\times 1/_{4}$ BHS   211-0	PLUG, 8 PIN, OCTAL-MOLDED	134-006
POST, BINDING, ASS'Y (METAL)   SN 1410-up   129-0     RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH 23/32 × 15/32   354-0     ROD, EXTENSION, 1/8 × 33/32   384-0     ROD, NYLON, 5/16 × 11/8, TAPPED 6-32 ONE END   SN 1001-up     SCREW, 4-40 × 5/16   FHS, PHILLIPS     SCREW, 6-32 × 1/4   BHS	POST, BINDING, 5-WAY ASS'Y (HEX CAP) SN 101-1409	129-030
RING, SOCKET, RETAINING   354-0     RING, LOCKING SWITCH <sup>23</sup> / <sub>32</sub> × <sup>15</sup> / <sub>32</sub> 354-0     ROD, EXTENSION, <sup>1</sup> / <sub>8</sub> × 3 <sup>3</sup> / <sub>32</sub> 384-0     ROD, NYLON, <sup>5</sup> / <sub>16</sub> × 1 <sup>1</sup> / <sub>8</sub> , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 × <sup>5</sup> / <sub>16</sub> FHS, PHILLIPS   211-0     SCREW, 6-32 × <sup>1</sup> / <sub>4</sub> BHS   211-5	POST, BINDING, 5-WAY ASS'Y (FLUTED CAP) SN 1410-up	129-036
RING, LOCKING SWITCH <sup>23</sup> / <sub>32</sub> x <sup>15</sup> / <sub>32</sub> 354-0     ROD, EXTENSION, <sup>1</sup> / <sub>8</sub> x 3 <sup>3</sup> / <sub>32</sub> 384-0     ROD, NYLON, <sup>5</sup> / <sub>16</sub> x 1 <sup>1</sup> / <sub>8</sub> , TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 x <sup>5</sup> / <sub>16</sub> FHS, PHILLIPS   211-0     SCREW, 6-32 x <sup>1</sup> / <sub>4</sub> BHS   211-5	POST, BINDING, ASS'Y (METAL) SN 1410-up	129-051
ROD, EXTENSION, 1/8 × 33/32   384-0     ROD, NYLON, 5/16 × 11/8, TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 × 5/16 FHS, PHILLIPS   211-0     SCREW, 6-32 × 1/4 BHS   211-5	RING, SOCKET, RETAINING	354-002
ROD, NYLON, 5/16 x 11/8, TAPPED 6-32 ONE END SN 1001-up   385-1     SCREW, 4-40 x 5/16 FHS, PHILLIPS   211-0     SCREW, 6-32 x 1/4 BHS   211-5	RING, LOCKING SWITCH $23/32 \times 15/32$	354-055
SCREW, $4-40 \times \frac{5}{16}$ FHS, PHILLIPS   211-0     SCREW, $6-32 \times \frac{1}{4}$ BHS   211-5	ROD, EXTENSION, $\frac{1}{8} \times \frac{3^3}{32}$	384-077
SCREW, 6-32 x 1/4 BHS 211-5	ROD, NYLON, 5/16 x 11/8, TAPPED 6-32 ONE END SN 1001-up	385-113
	SCREW, 4-40 x <sup>5</sup> /16 FHS, PHILLIPS	211-038
SCREW, 6-32 x <sup>5</sup> /16 BHS 211-5	SCREW, 6-32 × ¼ BHS	211-504
	SCREW, 6-32 x ⁵/16 BHS	211-507

	Tektronix Part Number
SCREW, 6-32 × 3/8 BHS	211-510
SCREW, 6-32 x 11/4 BHS	211-529
SCREW, 6-32 x ⁵/16 PHS W/LOCKWASHER	211-534
SCREW, 6-32 x ⁵/16 FHS, 100°, CSK, PHILLIPS	211-538
SCREW, 6-32 x 3/4, TRUSS HS, PHILLIPS	211-544
SCREW, 8-32 × 3/8 OHS	212-019
SCREW, 10-32 x 5/₀ BHS	212-509
SCREW, 10-32 x 7/8 RHS	212-548
SCREW, 10-32 x $\frac{1}{2}$ RHS (STAINLESS STEEL)	212-557
SCREW, 5-32 x $^{3}$ /16 PAN HS, THREAD CUTTING	213-044
SHIELD, CRT 3"	337-101
SHIELD, .040 x 47/8 x 55/8 x 23/32 (H.V.) SN 101-1000	337-112
SHIELD, .040 × 47/8 × 55/8 × 7 (H.V.) SN 101-1000	337-113
SHIELD, .040 x 2 <sup>3</sup> / <sub>8</sub> x 2 <sup>3</sup> / <sub>8</sub> x 2 <sup>9</sup> / <sub>16</sub> SN 101-1000	337-115
SHIELD, .040 x 2 <sup>3</sup> / <sub>8</sub> x 2 <sup>3</sup> / <sub>4</sub> x 2 <sup>1</sup> / <sub>8</sub> (ATTEN.) SN 1001-up	337-252
SHIELD, .040 x 47/8 x 55/8 x 5/16 (H.V.) SN 1001-up	337-253
SHIELD, .040 x 47⁄8 x 5⁵⁄8 x 2¹⁄₄ (H.V.) SN 1001-up	337-254
SOCKET, STM8	136-013
SOCKET, STM12 CRT W/WIRE LEADS	1 <b>36-02</b> 3
SOCKET, GRATICULE LIGHT W/GROUND LUG	136-035
SOCKET, 7 PIN, 2 PRONG (FOR ETCHED CKT.) SN 101-1000	136-032
SOCKET, STM7G SN 1001-up	136-008
SOCKET, 9 PIN (FOR ETCHED CKT.) SN 101-1000	136-034
SOCKET, STM9G SN 1001-up	136-015
SPACER, NYLON, $\eta_{16}$ , FOR CERAMIC STRIP	361-007
SPACER, NYLON, 5/16, FOR CERAMIC STRIP	361-009
STRAP, MTG., .025 x 5/16 x 41/4 W/214-009 EACH END	346-001
STRAP, MTG., TRANSF., .040 x $\frac{1}{2}$ x 1 <sup>5</sup> / <sub>8</sub> x 1 $\frac{1}{16}$ W/210-617 EACH END	346-006
STRIP, CERAMIC, $\frac{3}{4} \times 7$ NOTCHES, CLIP MTD.	124-089
STRIP, CERAMIC, 3/4 x 9 NOTCHES, CLIP MTD.	124-090
STRIP, CERAMIC, 3/4 × 11 NOTCHES, CLIP MTD.	124-091
TUBE, SPACER, .180 x 1/4 x 3/16 SN 101-1000	166- <b>03</b> 0

Tektronix Part Number

35
39
03
32
40
44
02
3333



### PROBES THIS SHEET COVERS

#### P6017

43 inches	Tektronix Part No.	010-038
6 ft.		010-056
9 ft.		010-057
12 ft.		010-058

#### P6022

43 inches	Tektronix Part No.	010-064
6 ft.		010-066
9 ft.		010-067
12 ft.		010-068

#### TABLE I ELECTRICAL PARTS

Ckt. No.	Model No.	Cable Length	Value		Der	scription		Tektronix Part No.
C1 C2	A11 A11 A11 A11 1	43 inches 6 ft. 9 ft. 12 ft. All Lengths	11μμf 14μμf 18μ <b>af</b> 21μμf 8-50μμf	Cer. Cer.	Fixed Var.	500v -	+or- 5%	281-576 281-577 281-578 281-579 281-013
C2	2	All Lengths	5-80µµf	Mica	Var.	500v		281-062
R1 R2	All All	All Lengths All Lengths	9 meg	1/2 w Select	Fixed ed for protection, F	Prec. oper cabl	2% e	309-232

#### NOTE

On the underside of the lid for the Compensation Box is the Model Number. If the probe shows no number it will be Model Number One.

#### TABLE II MECHANICAL PARTS

ltem No,	Probe Type	Model No.	Cable Length	Part Title	Tektronix Part No.
1	P6017/P6022	All	All Lengths	Probe Body	204-054
2	P6017/P6022	A11	43 inches	Attenuation Assembly	011-038
			6 ft.		011-037
			9 ft.		011-039
			12 ft.		011-040
3	P6017/P6022	A11	43 inches	Cable Assembly	175-143
			6 ft.		175-185
			9 ft.		175-186
			12 ft.		175-187
4	P6017/P6022	1	All Lengths	Compensator Box	202-051
		2			202-068
5	P6017/P6022	A11	All Lengths	Allen Set Screws 4-40 x 3/32	213-075
6	P6017/P6022	2 only	All Lengths	Positioning Insulator	200-098
7	P6017/P6022	1 2	All Lengths	Compensating Capacitor Compensating Capacitor	281-013
				and Spring Clip Assembly	281-059
8	P6017/P6022	A11	All Lengths	Plate Cover	200-248
9	P6017/P6022	A11	All Lengths	Thread Cutting Screw 4-40 x 1/4	213-035
10 A	P6017	All	All Lengths	Connector UHF	131-058
10	P6022	All	All Lengths	Connector, BNC	131-186

MRH

344-046
134-013
352-024
206-023
206-060
013-027
175-125
013-020 206-061 206-054 206-052 206-045 205-034
206-015
175-124
175-124

Accessories Supplied with Probe



V/25 SERIES REGULATOR





TYPE 160 POWER SUPPLY S/N 101-619





+















AA

TYPE 161 PULSE GENE





L.A.P. E.S





TYPE 162 WAVEFORM GENERATOR



L.U.P. 10-5-53

AA

BLOCK DIAGRAM



AC

-

-



AC

~

TYPE 162 WAVEFORM GENERATOR

L. Q.P. 9 - 5 - 57

+



TEKTRONIX TYPE 163 PU



X TYPE 163 PULSE GENERATOR AA BLOCK DIAGRAM

V.B. 6.5.53



VIO GUB COMPARATOR

### TEKTRONIX TYPE 163 PULSE GENERATOR

VIZA ZGAL5 DISCONNECT DIODE

VII GUB REGENERATIVE TRIGGER AMPLIFIER

+



GENERATOR

AB

SCHEMATIC DIAGRAM

















VE





HORIZONTAL AMPLIFIER





C31 .001

-16

~~~

R31 100 K



↓ C30 ↓ 4.7 =

----R 30 1 M



VE







TYPE 360 INDICATOR

+

AC,





TYPE 360 INDICATOR

+



рвн 5-25-61

CRT CIRCUIT

AA2

+

## MANUAL CHANGE INFORMATION

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At Tektronix, we continually strive to keep up with latest electronic developments by adding circuit and component improvements to our instruments as soon as they are developed and tested.

Sometimes, due to printing and shipping requirements, we can't get these changes immediately into printed manuals. Hence, your manual may contain new change information on following pages. If it does not, your manual is correct as printed.

# TYPE 163 Direct Replacement (30) Mod 5918

| R40 Char | ge to 2.5k | 5w | ww | 308-127 |
|----------|------------|----|----|---------|
|----------|------------|----|----|---------|

# TYPE 360 MOD 5366 - Tent S/N 2826 (31) Direct Replacement

|  | R34 | Change to 7k | Pot. Comp | 10% | 311-223 |
|--|-----|--------------|-----------|-----|---------|
|--|-----|--------------|-----------|-----|---------|

# TYPE 160A MOD 6042 - Tent S/N 6820

| R13 | Remove and | i replace w | vith wire strap | )   |         |
|-----|------------|-------------|-----------------|-----|---------|
| R15 | Change to  | 1.5m        | 1 <b>/2w</b>    | 10% | 302-155 |