

MANUAL # M360645

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DCR-B2 SERIES

500-Watt & 1000-Watt Power Supplies

Service Manual

Manual covers DCR-B2 models:

<u>500-Watt</u>	<u>1000-Watt</u>
10-40B2	10-80B2
20-25B2	20-50B2
40-13B2	40-25B2
60-9B2	60-18B2
80-6B2	80-12B2
150-3B2	150-6B2
300-1.5B2	300-3B2
600-.75B2	600-1.5B2

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TABLE OF CONTENTS

SECTION 1	THEORY OF OPERATION	PAGE
1.1 INTRODUCTION	1	
1.2 PHASE CONTROL PRINCIPLE	1	
1.3 BLOCK DIAGRAM ANALYSIS (FIGURE 1-2)	3	
1.4 DETAILED CIRCUIT DESCRIPTION	3	
1.4.1 REFERENCE AND BIAS SUPPLIES	3	
1.4.2 VOLTAGE MODE SECTION	4	
1.4.3 CURRENT MODE SECTION	5	
1.4.4 RAMP GENERATOR, RESET CIRCUIT AND COMPARATOR	5	
1.4.5 BLOCKING OSCILLATOR CIRCUIT	6	
1.4.6 TURN-ON AND SHUT-DOWN CIRCUIT	6	
1.4.7 POWER SECTION.....	7	
1.4.8 OVERVOLTAGE PROTECTOR	7	
1.4.9 INDICATOR LAMPS	7	
1.4.10 CHANGEABLE CURRENT PROGRAMMING PARAMETERS	8	
SECTION 2	MAINTENANCE	
2.1 GENERAL.....	9	
2.2 PERIODIC SERVICING	9	
2.3 TROUBLESHOOTING	9	
2.4 CALIBRATION.....	9	
2.5 PERFORMANCE TESTING	11	
2.5.1 VOLTAGE MODE REGULATION AND RIPPLE	12	
2.5.2 CURRENT MODE REGULATION	13	
2.5.3 TRANSIENT RESPONSE.....	13	
2.6 HI-POT TEST PROCEDURE	16	
SECTION 3 DRAWINGS AND PARTS LISTS		
3.1 GENERAL.....	17	
3.1.1 CIRCUIT SYMBOL.....	17	
3.1.2 SORENSEN PART NUMBER.....	17	
3.2 REPLACEMENT PARTS LISTS.....	17	
3.3 ASSEMBLY DRAWINGS (SEE ATTACHED)	17	

LIST OF FIGURES

FIGURE	TITLE	PAGE
1-1	Phase Control Firing Angles.....	1
1-2	DCR-B2 Functional Block Diagram.....	2
1-3	Passing Stage Principle.....	4
2-1	Performance Test Setup.....	12

LIST OF TABLES

TABLE	TITLE	PAGE
2-1	DCR-B2 Troubleshooting.....	11
2-2	Sensing Resistor Values.....	14
2-3	Unit Calibration Specification.....	15

SECTION 1

THEORY OF OPERATION

1.1 INTRODUCTION

This section provides a basic discussion of unit operating principles, which may be used in conjunction with the troubleshooting chart provided in Section 3, to enable the logical and rapid isolation of unit faults. A brief description of the phase control principle is given first, followed by a block diagram analysis of system functions. The function of each section is then described in detail.

1.2 PHASE CONTROL PRINCIPLE

The sinusoidal wave in Figure 1-1 represents normal ac line voltage. If, by some means, conduction of this voltage is delayed, the average voltage output will be reduced. Control of the delay then results in control of the average voltage. This is phase control. The silicon controlled rectifier (SCR) acts like a switch, activated by the delay circuit, to provide the phase control. The delay is expressed in degrees and is known as the firing angle. Figure 1-1 shows firing angles of 60° and 120°.

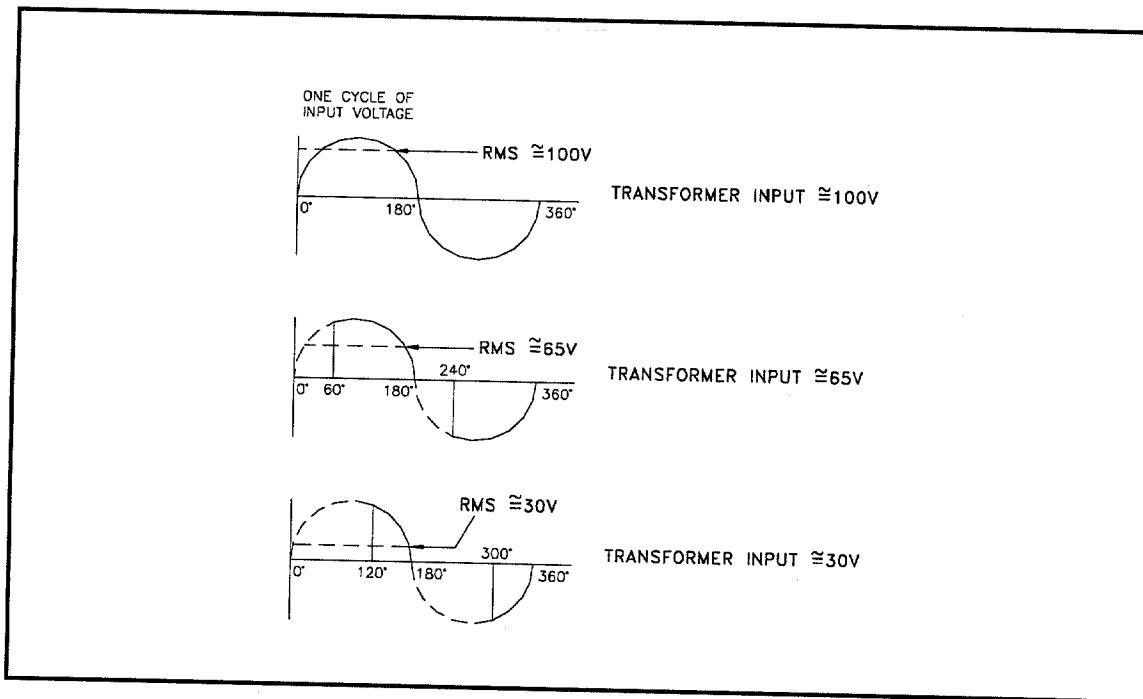


Figure 1-1 Phase Control Firing Angles

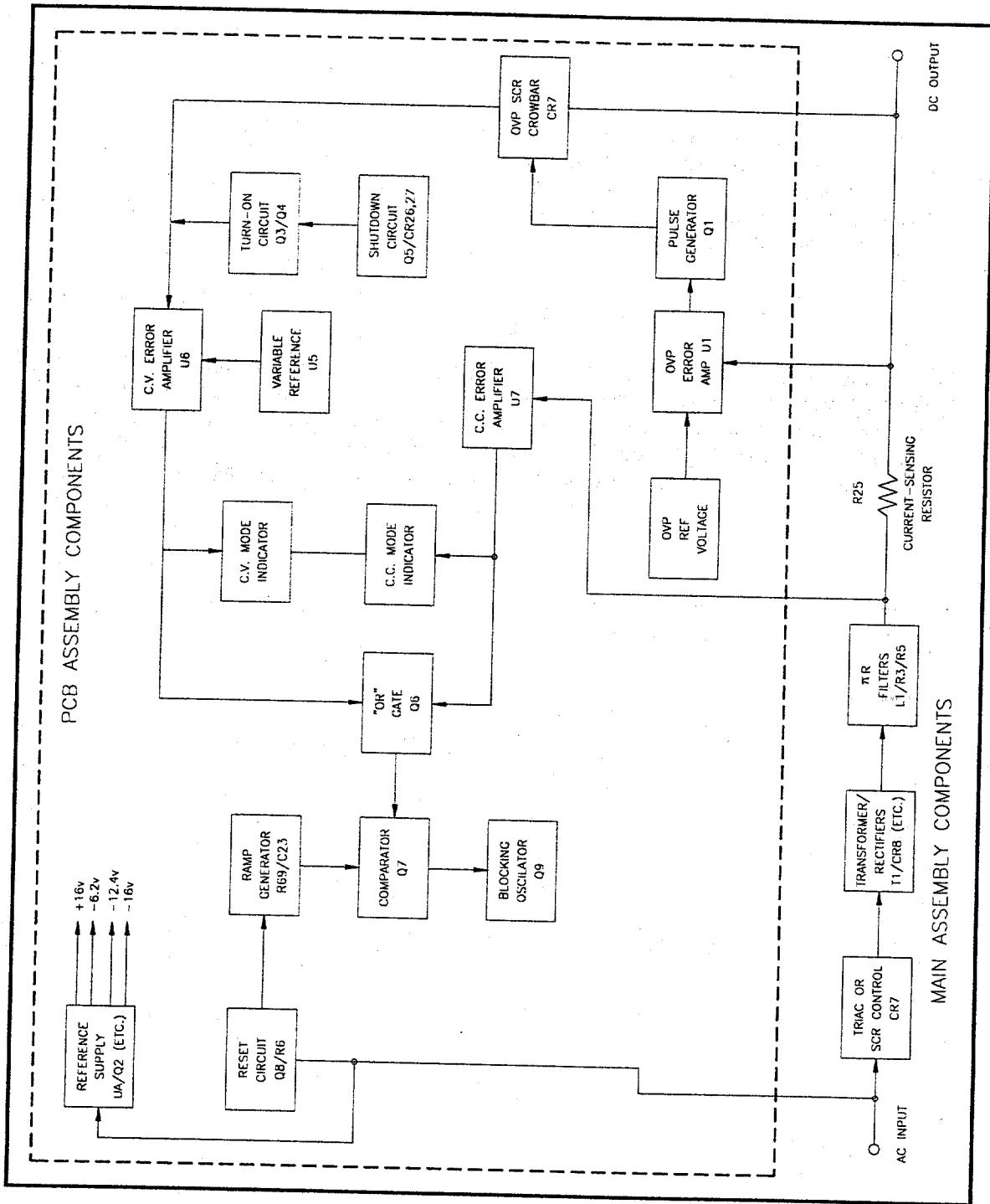


Figure 1-2 DCR-B2 Functional Block Diagram

1.3 BLOCK DIAGRAM ANALYSIS (FIGURE 1-2)

The ac input voltage is first applied to CR7 (Triac), which is in series with power transformer T1. CR7 functions with the control circuits to form a feedback loop which prevents a change in output voltage when either the line or load changes.

To accomplish this, the control circuits issue a phase adjusted firing pulse to CR7 once during each half cycle of the input ac voltage. These circuits continuously sample the output voltage, which establishes the precise time at which the firing pulse is to be generated. The phase controlled ac voltage is stepped up or down by power transformer T1, and coupled through a full-wave rectifier and filtering circuits to the output terminals.

Feedback signals from the output back to CR7 originate in the constant voltage/current error amplifiers U6/U7. In the constant voltage mode, U6 continuously compares the supply output with a reference voltage generated by a variable reference programming circuit, (U5). A difference in these voltages appears as an error signal, which is delivered to amplifier U6. This dc error signal is applied to Q6 (comparator input #1). A sawtooth ramp voltage, generated by Q8, R69 and C23, is applied to Q7 (comparator input #2). The comparator output (across R62) sets the conduction angle of blocking oscillator Q9. The duration of Q9 conduction is directly proportional to the error signal, and its output triggers CR7 into conduction. CR7 acts as a switch, whose firing angle is dependent on the magnitude of dc error signal, thus controlling the overall supply output.

Similarly, in the constant current mode, changes in line or load are sensed by R25, in series with the output. It is then amplified by U7, and applied to Q6 comparator input. Output control from this point is essentially the same as in the constant voltage analysis, above.

1.4 DETAILED CIRCUIT DESCRIPTION

NOTE

All component designators are referenced to PCB schematic diagram Figure 3-1 unless otherwise noted.

1.4.1 REFERENCE AND BIAS SUPPLIES

The precisely regulated voltage required for operation of the control circuitry is produced by a reference supply consisting of zener diodes D5/D6, operational amplifier U4, passing stage Q2, transformer T2 and center-tapped full wave rectifier D35/D36/D37/D38. (See main schematic).

The reference supply output appears across a comparison bridge composed of divider R31/R32, D16, and R77. Error signals are sensed across this bridge and amplified by U4. The variable impedance characteristic of passing stage Q2 changes the level of absorbed voltage across the stage, maintaining the output at a precisely controlled negative 12.4 volts (Figure 1-3).

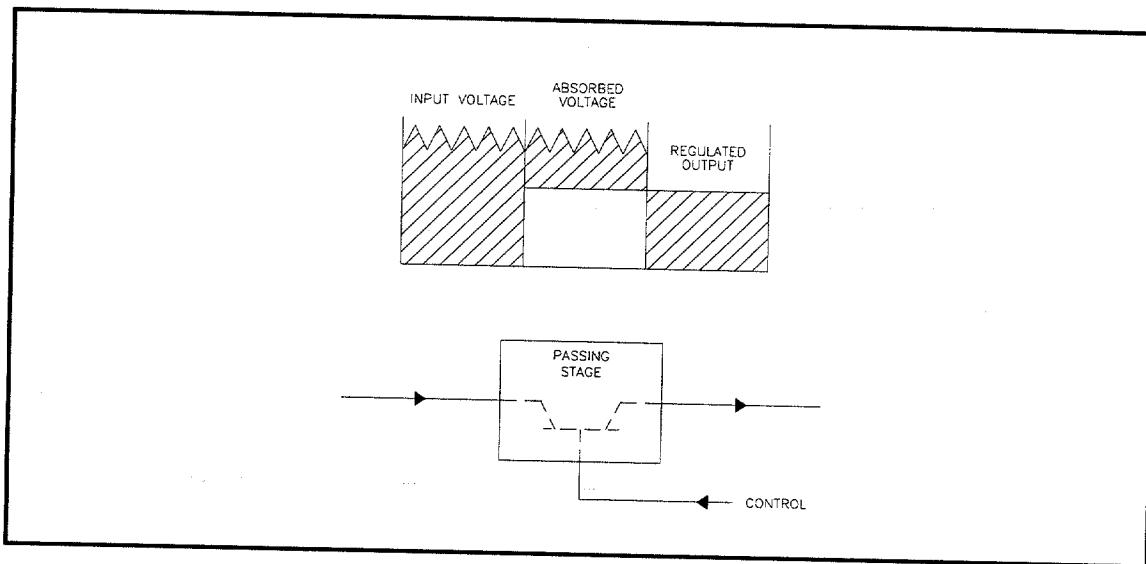


Figure 1-3 Passing Stage Principle

To illustrate circuit operation, assume an increase in the T2 (Figure 3-4) supply output. Pin 2 of U4 will become more negative, and the output at pin 6 more positive, tending to turn Q2 off. The reduction in drive current increases the impedance of Q2, and consequently its absorbed voltage, resulting in precise regulation of reference supply output.

Several other bias supplies are used to power the control circuitry:

1. +20 volts from D7. Note that there is no filtering on this 20 volt output. This signal is used as a time reference to the ac line. The +20 volt source is then gated through D21, and filtered by C18 to provide the +20 Vdc primary operating power for the control PCB.
2. The 20 volts across C18 is fed to R47 and D8, to create +16 volts for sections of the control circuitry. The +16 volts across D8 is then fed to R23 and D4 to generate and precisely regulate the +11.7V for the current amplifier reference voltage.
3. +30 Vdc unregulated (D35 and D37 on the overall schematic) is used to operate the current/voltage mode lamps, OVP control circuit, and remote current voltage select reference.

1.4.2 VOLTAGE MODE SECTION

Primary components of this circuit include constant voltage error amplifier U6, variable reference voltage programmer U5, and emitter-follower stage Q6. The circuit functions as follows:

Pin 3 of U5 is connected to plus sense. Front panel voltage controls R10/R11 function as variable feedback resistances from U5 pin 6 to pin 2. The negative 12.4 volt reference through R39/38/37 establishes the desired programming current range, so that 0 to 10 volt signal is obtained at pin 6 of U5.

The main error amplifier is U6. Pin 4 of U6 is at virtual dc ground since pin 5 is at ground (+sense). Thus, the current through R74 can be varied from 0 to 1 milliamper. This current, through R79, programs the supply to the desired output. U6 pin 5 senses this output, and compares it to the voltage developed at U6 pin 4. The resultant is an error signal, amplified by U6, and coupled to R61 through the emitter of Q6.

An illustration of voltage mode operation An increase in system output drives U6 pin 4 more negative. U6 pin 11, and thus the Q6 emitter also become more negative, creating the error voltage necessary to retard the firing angle of CR7 through T1/Q9 action as noted in the block diagram analysis.

C15/R44 establishes ac loop stability, aided by C16/R45.

1.4.3 CURRENT MODE SECTION

The primary component in this section is constant current amplifier U7. The 11.7V reference voltage is divided down by bridge dividers R20/R21 and R24/R19 to U7 pins 5 and 4 respectively. The resultant voltages are referenced to the positive output, through a current sensing resistor (R21), with R12/R13 serving as the front panel current adjust potentiometers.

R46/C17 establishes ac loop stability. C11/R36 (Variable) is a secondary stability network used for inductive load compensation.

R22/C7 acts to prevent rapid changes in the phase delay angle, caused by large transients. This protects the power components from overstress.

Trimmer R17 is used to adjust zero output current (compensating for current tolerances and offset voltage of U7).

Trimmer R18 is used to adjust for maximum current setting (compensating for tolerances in panel pot R12 and current shunt R25).

An illustration of current mode operation: If the output current approaches the current limit setting, the voltage across the sensing resistor becomes larger. This is seen as a positive error voltage at U7 pin 5, which is amplified and applied to the U7 output, pin 10. The output of U7, pin 10 (emitter) is passed through D20 to the base of the output stage of U7 at pin 13. The injected current causes the collector of U7, pin 11 to fall, reducing output. (See Voltage Mode section, para. 1.4.2, for additional details).

1.4.4 RAMP GENERATOR, RESET CIRCUIT AND COMPARATOR

The ramp generator consists of R69 and C23. The ramp voltage at the junction of R69/C23 is coupled through D30 to the base of Q7. This voltage starts at a maximum level, and decreases exponentially until reset by Q8 at 8.3 millisecond intervals (each 1/2 cycle of line voltage). The reset pulse for Q8 is generated through D7/R48 as follows:

The reset circuit consists of Q8 and R68. The full wave rectified ac input from T2 is impressed across D7/R48. D7 clamps the base of Q8 at its zener level, keeping it shut off (D21 is forward biased). As the impressed voltage drops toward zero, the zener voltage follows. D21 becomes reverse biased. Q8 then turns on from base bias through R68, charging C23 when the line voltage crosses zero.

The comparator consists of Q7/Q6, D30, R61, and R62. Comparator Q7/Q6 compares the dc signal from either the voltage or current mode amplifier (applied to Q6) with the ramp generator voltage. The varying output of Q7 (across R62) establishes the conduction angle of blocking oscillator Q9.

1.4.5 BLOCKING OSCILLATOR CIRCUIT

Q9 functions as a switch, providing the triggering voltage for D33 and D32 proportional to the error signal received from the comparator circuit. The blocking oscillator circuit functions as follows: Assume that at a given time the Q7 dc emitter voltage is several volts below the reference level provided by the reference supply circuit (paragraph 1.4.1). At a point when the ramp voltage, appearing at the base of Q7, is more negative than that on its emitter, Q7 conducts. This drives the base of Q9 positive, causing Q9 to conduct. As its collector current (I_c) increases, regenerative action occurs through pulse transformer T2, forcing Q9 into saturation. (I_c) continues to increase until T2 core saturates. Then T2 voltage decreases, removing Q9 base current. At this point Q9 comes out of saturation. The cycle is then repeated. The output of the pulse generator is a series of narrow pulses, continuing until the end of the line halfcycle.

1.4.6 .. TURN-ON AND SHUT-DOWN CIRCUITS

Primary components of the turn-on circuit are Q3, Q4, R56, R55, D28 and C22. Circuit operation is as follows: When power is initially applied to the unit, the bases of Q3/Q4 are driven positive, due to C22 coupling the rising voltage of the +16 volt bias supply. Q3 and Q4 are thus in saturation. The resultant negative voltage at the Q3/Q4 collector maintains voltage error amplifier U6 and the blocking oscillator/mixer circuits at cut off.

This action inhibits the output of the power supply from coming up. As C22 charges, the supply output will increase exponentially. Q3/Q4 gradually come out of saturation until the voltage across C22 reaches the point where they are shut off. The supply is then functioning in its normal manner.

The shut-down circuit, consisting of Q5, R58, R59, and D26/D27, cuts off the unit output when the cathode of either diode is connected to the plus sense connection. The circuit function is to actuate Q5, which turns Q3 and Q4 on. When the connection is removed, the power supply returns to normal, with the slow start described above.

D27 (TB3 pin 11) is available for customer use to shut down the dc output. Terminal 11 can be connected to +sense (TB3 Term 1) by either an isolated relay contact or an open collector logic signal (sinking approximately 0.2mA).

D26 is used internally to shut down the DCR-B2 output when the OVP is tripped.

1.4.7 POWER SECTION

The input ac voltage is applied to the primary of power transformer T1 through an SCR, (CR7). The output is rectified by a full wave bridge, and filtered by a Pi network with a damping resistor (R3). The filtered dc is then applied to the output terminals.

1.4.8 OVERVOLTAGE PROTECTOR

The OVP consists of a fast-response silicon-controlled rectifier crowbar (CR8). A reference voltage (+12V) is generated by zener D1 and R3. This reference voltage is compared to the output voltage in a bridge circuit, by the ratio of R6 to R16 plus R18 (adjust pot). The bridge output is applied to U1, pins 3 and 4. Assume that the resistor ratio is set (by adjust pot R18) to produce a balanced bridge at a specified output voltage. If the output voltage exceeds this preset value, U41, pin 3 will be driven positive relative to pin 4. The result is a positive output at pin 9 to turn on Q1. Q1 applies the +30V unregulated voltage to the primary of T1. The induced current in the secondary of T1 provides a trigger for the SCR crowbar. D12 activates the SCR, causing a crowbar function across the power supply output terminals.

The SCR recovers as soon as the output voltage is dropped, and removes the crowbar current. R5 supplies holding current to CR8 to hold the crowbar on.

To reset the OVP, power must be removed from the power supply input. After a moment to reset, lower the output voltage control, and reapply power to the input.

1.4.9 INDICATOR LAMPS

DS2, which indicates Constant Voltage mode, is wired across P19 and P1-19 as shown on the Control PCB schematic, Figure 6-1. DS3, which indicates Constant Current mode, is wired across P1-9 and P1-19.

U8 is an operational amplifier used to drive DS2 and DS3. The lamps and U8 are powered from the +30V supply.

The input signal to U8 determines which lamp lights, as follows:

A. Constant Current Mode (Current Limit) DS3

The input terminals of U8 are pins 2 and 3. Pin 2 is driven positive relative to pin 3 when the current amplifier (U7) output (pin 10) is in control (i.e., during current mode operation). Pin 2 positive signal will drive U8 output (pin 6) low (towards the +30V return). Pin 6 acts to reduce the voltage on DS2 and increases the voltage on DS3. DS3 is turned on brightly and DS2 is turned off.

B. Constant Voltage Mode (DS2)

During Voltage Mode operation, U8 pin 2 polarity reverses due to loss of U7 pin 10 voltage, so that U8 pin 6 output is driven high (towards +30V). This turns on DS2 and turns off DS3.

1.4.10 CHANGEABLE CURRENT PROGRAMMING PARAMETERS

0-400 mV Operation:

Dual range current mode signal programming is controlled by SW1, U3, U2 and associated parts. The signal programming voltage is applied between TB3-8(+) and TB3-9(+) with the jumper between TB3-7 and TB3-8 removed. For 0-400mV signal control voltage, SW1-1 is closed. This directly connects TB3-8 to R17 as in the standard DCR-B2 current mode signal programming. SW1-2 and SW1-3 are open.

0-10V Operation:

For 0-10V signal control voltage, SW1 is open; SW2 and SW3 are closed. Thus, the input voltage goes to pin U3B-5 via R12 and R11. D3 and R12 limit the input voltage to 15V maximum. R11, R9, R10 and U3A (pins 1,2,&3) comprise an inverting amplifier with a gain of 20-25. The gain inverting amplifier is set so that the output at SW1-2 is equal to .4V with Vin=10V (approx. 24). As input voltage goes from 0-10V, the output voltage goes from 0-400mV.

U2 and associated parts allow the front panel control pots to output a variable voltage even when they are disconnected from the control circuitry, ie, TB3-8.

SECTION 2

MAINTENANCE

2.1 GENERAL

This section provides troubleshooting data, periodic servicing, calibration, performance and hi-pot testing procedures. The troubleshooting data should be used in conjunction with the schematic diagrams and Section 1 which outlines the principles of operation. Any questions pertaining to repair should be directed to the nearest Sorensen representative or to the factory. Include the model and serial numbers in any correspondence. Should it be necessary to return a unit to the factory for repair, prior authorization from Sorensen Company must be obtained.

2.2 PERIODIC SERVICING

Whenever a unit is removed from service, it should be cleaned, using naphtha or an equivalent solvent on painted surfaces, and a weak solution of soap and warm water for the front panel. Compressed air may be used to blow dust from in and around components.

2.3 TROUBLESHOOTING

Table 2-1 provides a list of malfunction symptoms along with a tabulation of the possible cause(s) for each symptom. Note that the failure of a single component may result in a chain reaction effect. As additional aids to troubleshooting, voltage checkpoints have been designated on the printed circuit schematic diagram.

2.4 CALIBRATION

Following repair, the unit should be recalibrated to insure that replacement components have not altered performance. Refer to Table 2-3 for unit calibration specifications. The following is the calibration procedure to ensure that full rated voltage output is available:

1. Make sure input power has been removed from unit and circuit breaker set to "OFF" position.
2. Set SW1 on PCB to "ON", "OFF", "OFF".
3. Adjust course voltage knob to midpoint and course current fully clockwise.
4. Set power to unit and turn circuit breaker "ON".
5. Check to see if output is approximately 1/2 rated voltage.
6. Adjust course voltage fully clockwise. With maximum voltage pot (R37 on PCB) adjust output voltage to 105% of rated.
7. Set output to rated voltage with four significant digits.
8. Set both course and fine current knobs fully counter clockwise.

9. Verify unit has gone from voltage mode to current mode by noting a significant drop in output voltage, by illumination of DS3.
10. Set fine current adjustment to midpoint and apply short circuit.
11. Using minimum current Adj. (R17 on PCB) adjust output current to exactly 0 amps.
12. Adjust fine current fully clockwise; slowly adjust course current fully clockwise.
13. Using maximum current Adj. (R18 on PCB) adjust output current to 115% of rated.
14. Turn circuit breaker "OFF".
15. Set SW1 to "OFF", "ON", "ON".
16. Turn course current knob counter clockwise fully.
17. Turn circuit breaker "ON".
18. Slowly Adj. course current knob fully clockwise.
19. With short circuit still applied, set current using 10V gain Adj. (R75 on PCB) to 115% of rated current.
20. Remove short circuit.
21. Turn unit "OFF". Reset SW1 to "ON", "OFF", "OFF".
22. Turn unit back "ON".
23. Apply rated load with rated voltage out.
24. With voltmeter (positive lead on inside of R21 and negative lead on cathode of D24) use R7 on front panel to set 400 MV, $\pm 1\%$. Reset current meter with R6.
25. Apply pot lock to all pots, also R6 & R7.
26. Calibration complete.

Table 2-1 DCR-B2 Troubleshooting

1	No output (voltage mode)	a) Wrong input voltage b) Open fuses and circuit breaker* c) Reference voltages (check levels) d) Defective U6 or U5 e) Collector to emitter short on Q8, Q6, Q3, Q5 or Q4 f) Q9 open or shorted
2	Fuse opens or circuit breaker trips	a) CR7 shorted* b) Input capacitors shorted* c) D32, D33 shorted or open*
3	High output voltage (meter pointer pegs)	a) Sensing or programming leads or link open* b) Defective U6 or U5 c) Q7 shorted collector to emitter d) Q6 open collector to emitter e) CR7 shorted*
4	No output (current mode), or unit will not current limit	a) Defective U7 b) C7 shorted c) D20 open d) Shorted COARSE CURRENT potentiometer* e) Collector to emitter short on Q8, Q6, Q3, Q5 or Q4 f) Q9 open or shorted
5	Output oscillates (current mode)	a) Potentiometer R36 on unit PCB improperly adjusted

*Chassis components (ref. Figure 2-3)

2.5 PERFORMANCE TESTING

Sensitive instruments like the DCR-B require rigorous testing methods if a true performance evaluation is to be made. Wherever possible, twisted leads should be used with test equipment to reduce stray pickup. At the power supply terminal board, these leads must be firmly held by the terminal screws. Alligator clips and similar types of connectors are not suitable. Grounding techniques in which more than one device in the setup is grounded may introduce extraneous ripple that, although unrelated to the power output ripple, is displayed on the test oscilloscope.

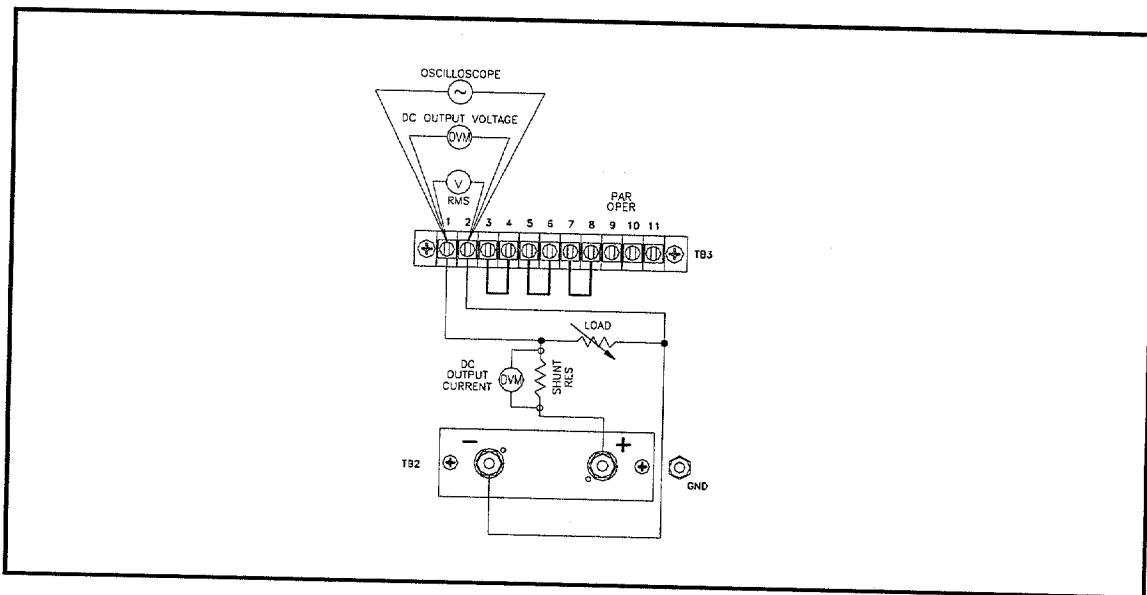


Figure 2-1 Performance Test Setup

2.5.1Voltage Mode Regulation and Ripple

To check voltage mode regulation and ripple, proceed as follows:

1. Connect a sensitive digital voltmeter and an RMS ac voltmeter across unit output terminals per Figure 2-1. Select a current shunt per Table 2-2 with a DVM for current output readings.

Use an autotransformer for AC line input with a current rating that exceeds the maximum unit input current called out in the unit specifications.

NOTE

Input devices such as autotransformers or line regulators can distort the input wave sufficiently to adversely affect performance measurements.

2. Apply high ac line input per specifications and remove load. Set the POWER switch to ON.
3. Rotate COARSE CURRENT control fully clockwise.
4. Use COARSE and FINE VOLTAGE controls to obtain rated output voltage. Note DVM reading after a few minutes of warm up time.

5. Decrease ac input voltage to low line specification. Output voltage change should not exceed limits specified in Table 2-3.
6. Close load switch and adjust load for rated current. Using high ac line specification and full load, verify ripple meets specification.

2.5.2 Current Mode Regulation

To check current mode regulation, proceed as follows:

1. At no load, adjust output to maximum rated voltage, and set COARSE CURRENT control fully clockwise.
2. Connect a sense resistor (Table 2-2) or a precision meter shunt in series with a variable load across the output terminals.
3. Connect input power at low line per unit specifications. Apply load until rated current of supply is reached. (Unit has voltage mode indicated.) Adjust COARSE CURRENT control until CURRENT mode indicator is lit and output voltage drops at least 5% offull scale value.
4. Connect a digital voltmeter across the sensing resistor, and note the indication.
5. Increase input voltage until voltage is at high line, and reduce the load resistance to zero (short). Note indication on the DVM. Change in voltmeter reading (expressed in millivolts) should be divided by sense resistor value to obtain regulation in milliamperes. Limits are provided in Table 2-3.

2.5.3 Transient Response

Test for transient response as follows:

1. Connect an oscilloscope across the unit output terminals.
2. Set unit POWER switch to ON. Adjust COARSE VOLTAGE control for rated output, and COARSE CURRENT control fully clockwise.
3. Apply half load, and then abruptly apply full load (or switch from full load to half load). Return to steady state operation should occur within 50 milliseconds (typical). See Table 2-3 for typical transient deviation voltage values.

NOTE

Load switching time should
be less than 3 milliseconds.

Table 2-2
Sensing Resistor Values (Current Mode Regulation Check)

DCR MODEL	SENSE RESISTOR (Ohms)
10-40B2	0.01, 50W
10-80B2	.00625, 50W
20-25B2	0.01, 50W
20-50B2	.0200, 50W
40-13B2	0.01, 50W
40-25B2	.0400, 25W
60-9B2	0.1, 25W
60-18B2	.0556, 20W
80-6B2	0.1, 25W
80-12B2	.0833, 12W
150-3B2	0.1, 25W
150-6B2	.167, 6W
300-1.5B2	1.0, 10W
300-3B2	.333, 3W
600-.75B2	1.0, 10W
600-1.5B2	.333, 1W

Table 2-3
Unit Calibration Specifications

DCR Model	<u>Regulation</u>		Ripple Volt Mode (mV)	Transient Deviation (Volts)	Maximum Compliance (Vdc)	Cur. Mode Upper Lim. Set Pt. (A)
	Voltage Mode (mV)	Current Mode (mA)				
10-40B2	3	100	65	0.6	10	46
10-80B2	3	200	65	1.0	10	92
20-25B2	6	62.5	65	1.2	20	28.75
20-50B2	10	125	65	1.6	20	58
40-13B2	12	32.5	90	2.4	40	14.95
40-25B2	12	63	90	2.9	40	29
60-9B2	18	22.5	125	3.6	60	10.35
60-18B2	18	45	125	4.0	60	21
80-6B2	24	15	150	4.8	80	6.9
80-12B2	24	33	150	5.3	80	14
150-3B2	45	7.5	300	9.0	150	3.45
150-6B2	45	16	300	9.5	150	7.0
300-1.5B2	90	3.75	700	18	300	1.725
300-3B2	90	8	700	20	300	3.5
600-75B2	180	2	1200	36	600	0.8625
600-1.5B2	180	4	1200	40	600	1.7

2.6HI-POT TEST PROCEDURE

High potential test procedures have been carefully carried out at the factory. These units are 100% tested and should not require further testing in the field.

CAUTION

High potential test can overstress or destroy the power semiconductors in this power supply if improperly applied.

Isolation measurements may be made using a standard VOM (Simpson 260 or equivalent) on the highest resistance scale available.

If it is essential to use the high potential test method, please contact the factory for information on special precautions that should be taken.

CAUTION

Sorensen Company cannot be held liable for any malfunctions resulting from the application of a high potential test (greater than 100V). See standard Sorensen Company warranty.

SECTION 3 _____ **DRAWINGS AND PARTS LISTS**

3.1.....GENERAL

This manual contains schematic diagrams, PCB parts location drawings, and replaceable parts lists. The parts lists are keyed to the applicable schematic diagrams, and assembly drawings by the Reference Designator and Item Number.

3.1.1.....Circuit Symbol (Reference Designator)

This is an alpha-numeric identification of the component as called out on the unit drawings.

3.1.2.....Sorensen Part Number

The Sorensen part number should be used when ordering parts directly from:

Sorensen
Sales & Technical Support
9250 Brown Deer Road
San Diego, CA 92121-2294
1-800-525-2024
Tel: (858) 450-0085
Fax: (858) 458-0267
Email: sales@sorensen.com
www.sorensen.com

3.2.....REPLACEMENT PARTS LISTS (See Attached)

3.3.....ASSEMBLY DRAWINGS (See Attached)

DRAWING #		DESCRIPTION
500 WATT	1000 WATT	
M360646	M360646	REPLACEMENT PARTS LIST
1063996	1063996	DWG OUTLINE
1064093	1064377	SCHEMATIC, UNIT
1063006	1063006	SCHEMATIC, CONTROL PCB
1063829	1064371	FINAL ASSY
	1064436	BASE ASSY
1063513	1063513	FRONT PANEL ASSY
1064468	1063514	REAR PANEL ASSY
1063005	1063005	CONTROL PCB ASSY
1063865	1063865	CAP ASSY
1063518	1063518	POT ASSY

8	7	6	5	4	3	2	1
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NOTES: UNLESS OTHERWISE SPECIFIED.

1. ASSEMBLE PER ELGAR WORKMANSHIP STANDARD
DOCUMENT NO. 0050003-01.

TORQUE ALL POTENTIOMETERS IN POSITION
SHOWN 10 IN-LBS.

REVISIONS	
ZONE REV	DESCRIPTION
A	PROD REL PER 89A340 AR
B	REV PER ECN N950370

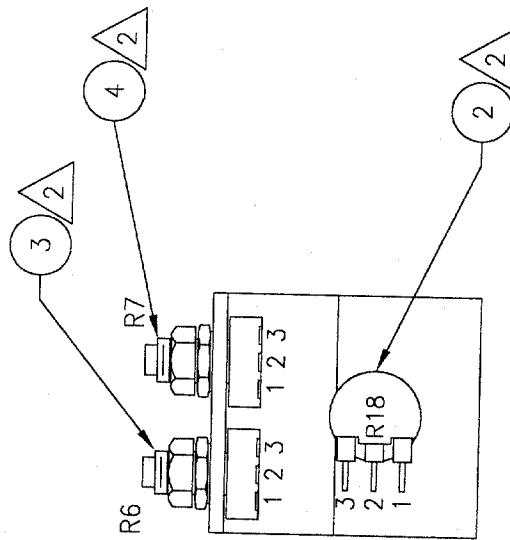
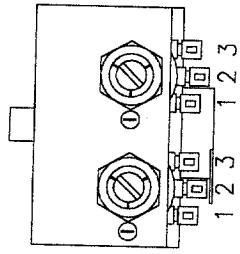
D

C

B

1063518

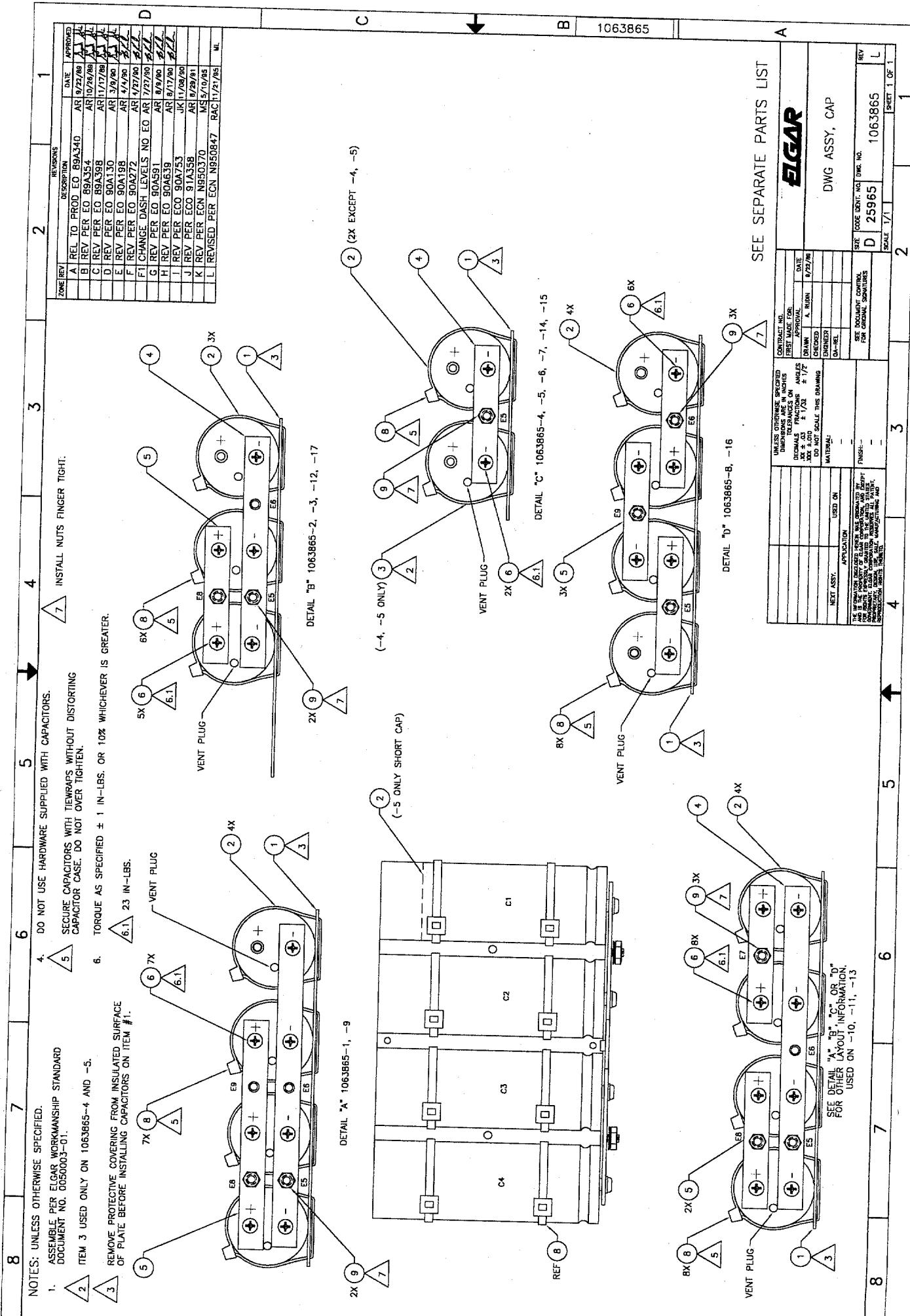
A



SEE SEPARATE PARTS LIST: 1063518-1 THRU -8

ELGAR	
UNLESS OTHERWISE SPECIFIED	CONTRACT NO.
ANGLES	FIRST MADE FOR:
DECIMAL FRACTION	APPROVAL DATE
TOLERANCES	DRWNS
INCHES	4/29/88
DEGREES	ANGLE
MM	± 1/32
MM	DO NOT SCALE THIS DRAWING
MM	CHECKED
MM	ENGINEER
MM	MAINTENANCE
MM	DATA REL
NEXT ASSY:	USED ON
APPLICATION:	
FINISH:	
RE. DOCUMENT CONTROL	
FOR ORIGINAL SIGNATURES	
SHEET 1 OF	

8	7	6	5	4	3	2	1
---	---	---	---	---	---	---	---



SEE SEPARATE PARTS LIST : 1063005-XXX

8	7	6	5	4	3	2	1
---	---	---	---	---	---	---	---

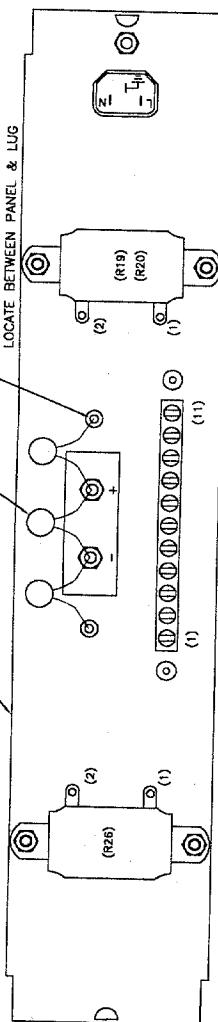
NOTES: UNLESS OTHERWISE SPECIFIED.

1. ASSEMBLE PER ELGAR WORKMANSHIP STANDARD
DOCUMENT NO. 0050003-01.

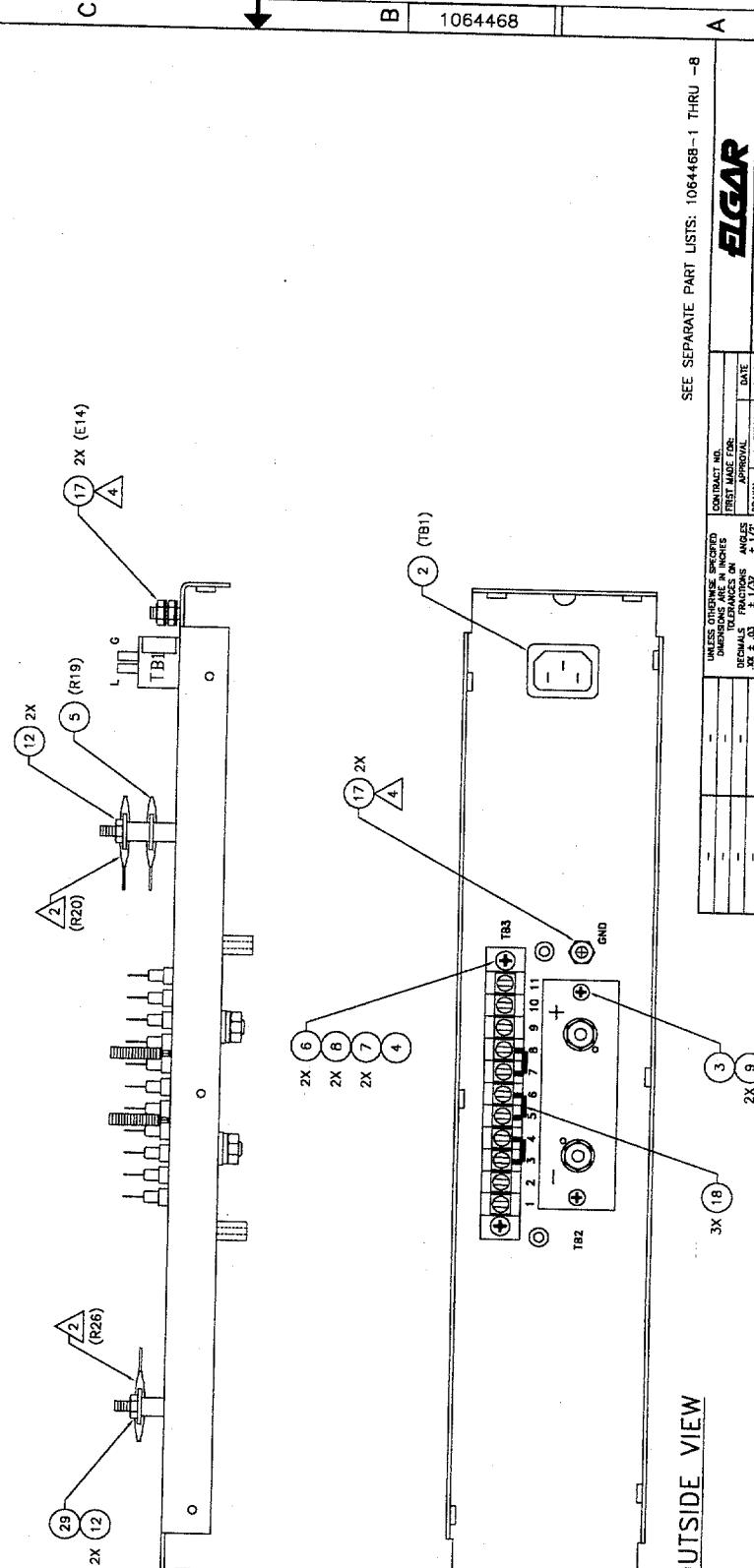
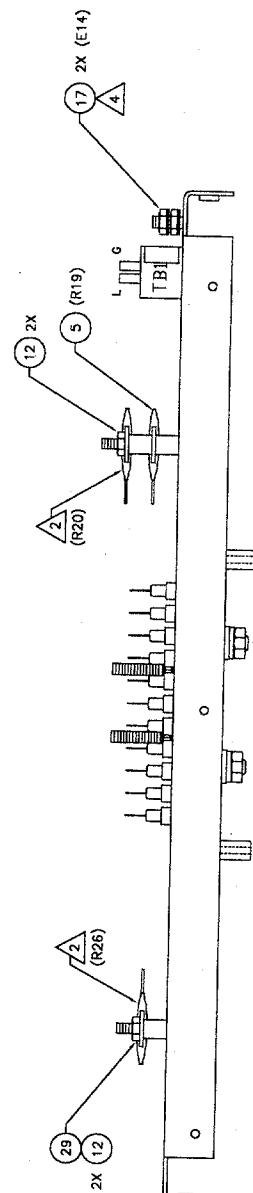
2. R20 AND R26 (ITEMS 5 AND 29) ARE USED
ON -7 AND -8 MODELS ONLY.

3. TEXT IN PARENTHESES () REFERENCES
WIRE LISTS AND SCHEMATICS.

4. BOTH NUTS: FINGER TIGHT.



INSIDE VIEW



OUTSIDE VIEW

REVISIONS	
ZONE REV	DESCRIPTION
A	REL TO MANUFAC.
B	REV PER ECO 91A
C	REV PER ECO 91A/169
D	REV PER ECO 92A/434
E	REV PER ECO 92A/627
F	REV PER ECO 92A/2
G	REVISED PER ECN N940122
H	REVISED PER ECN N950370
J	REVISED PER ECN N950818
K	REVISED PER ECN N970377

D	DATE APPROVED
A	9/6/90
B	4/20/91
C	9/27/91
D	9/27/92
E	10/12/92
F	6-30-94
G	941214
H	5/10/95
J	11/21/95
K	5/12/97

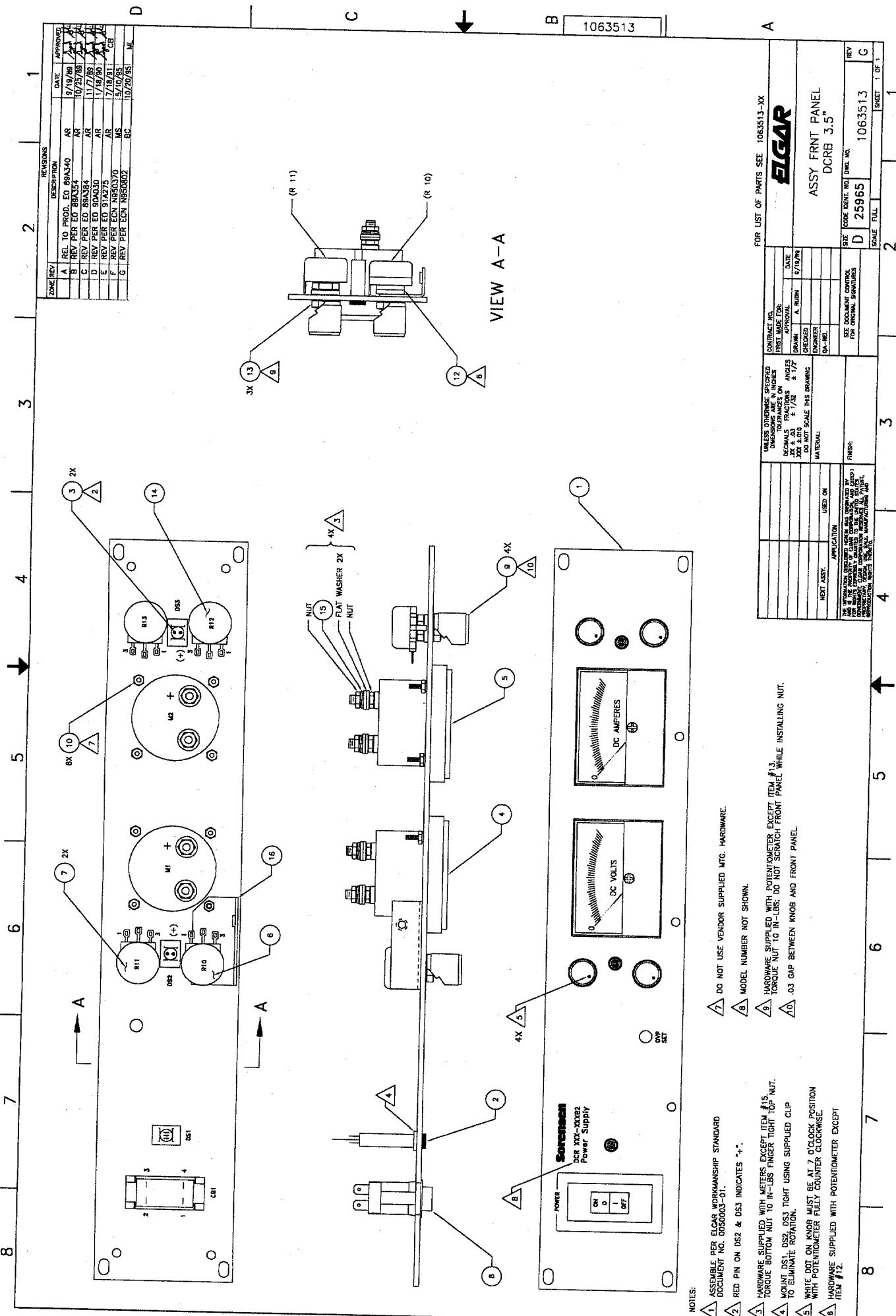
SEE SEPARATE PART LISTS: 1064468-1 THRU -8

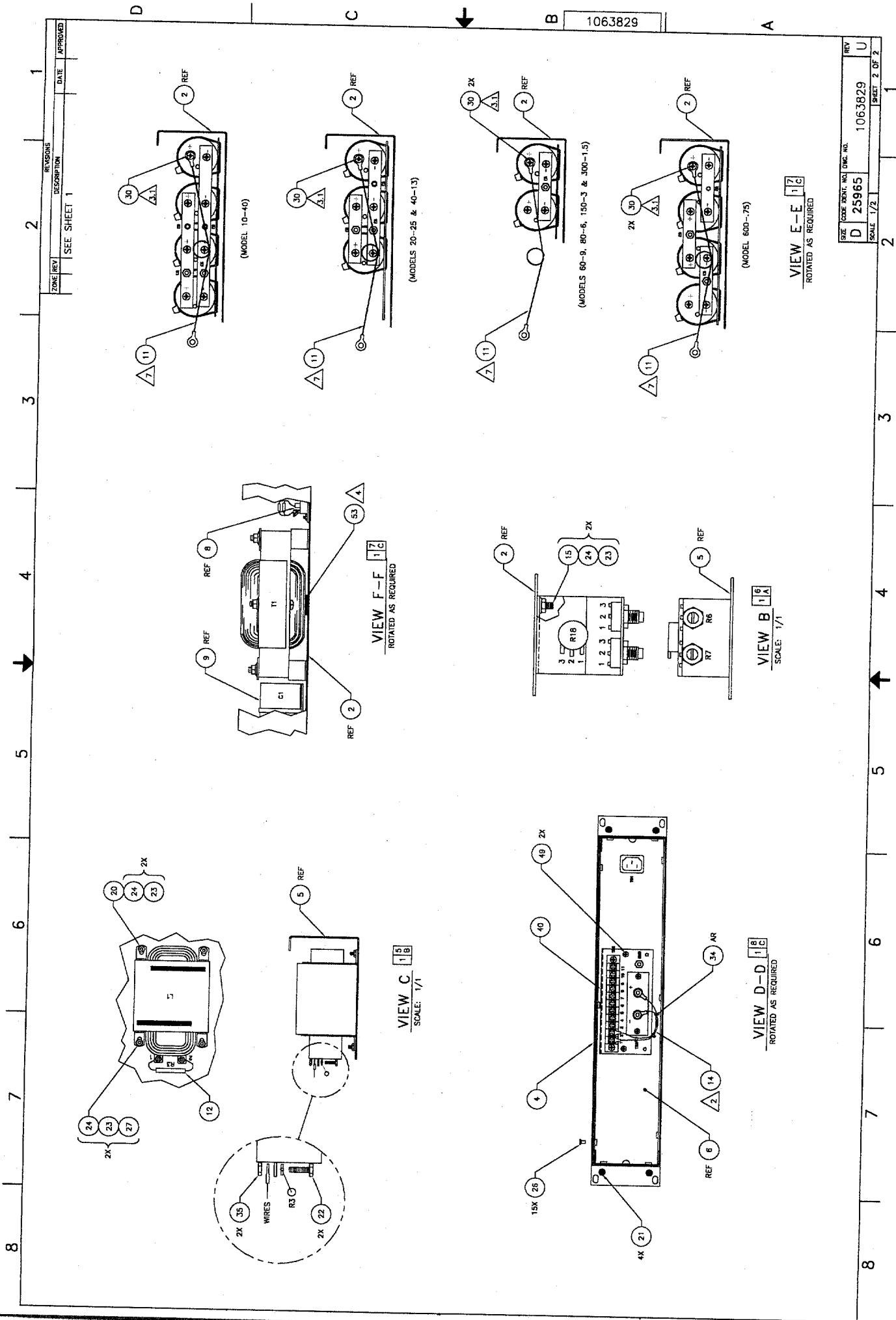
ELGAR

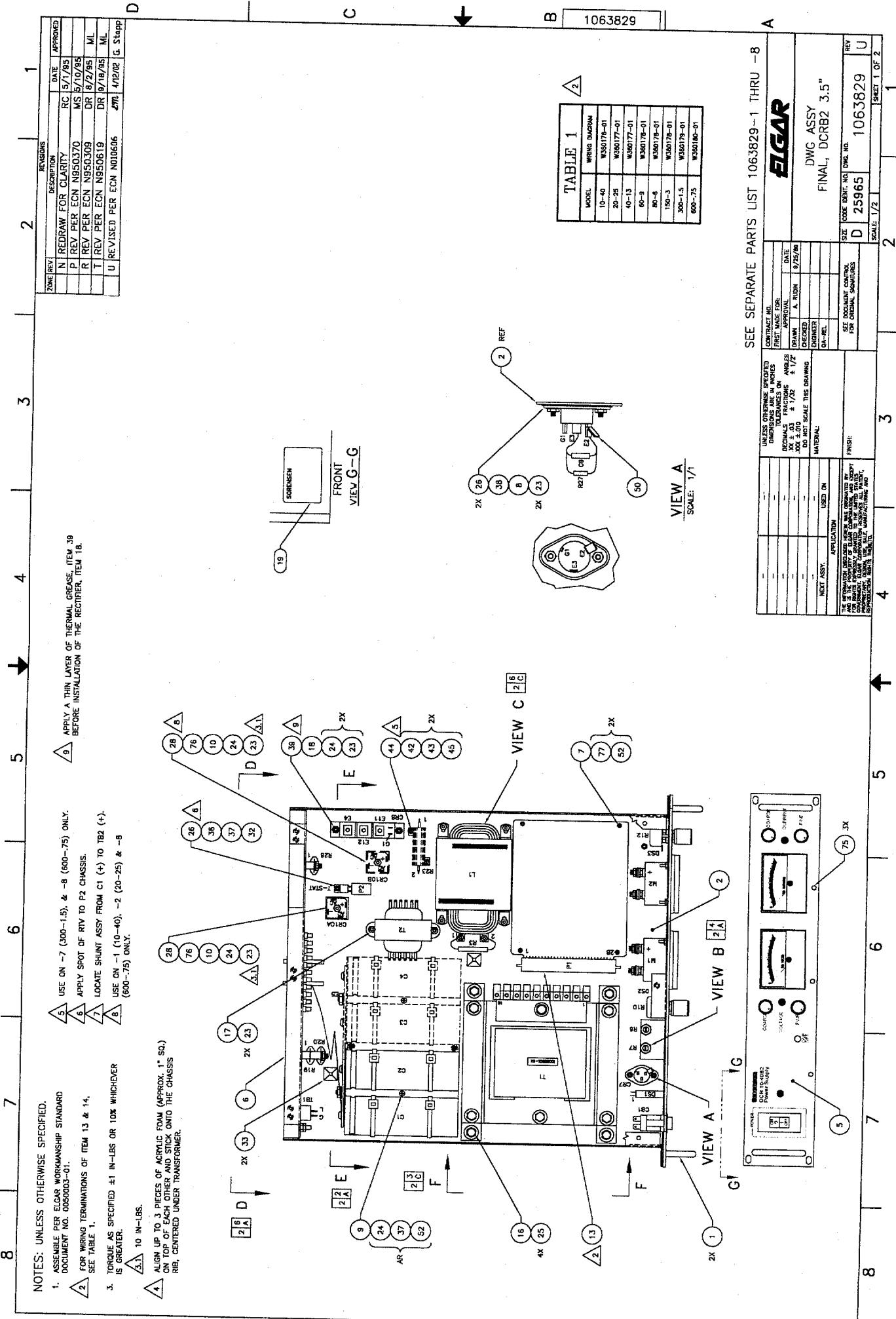
DWG ASSY
REAR PANEL

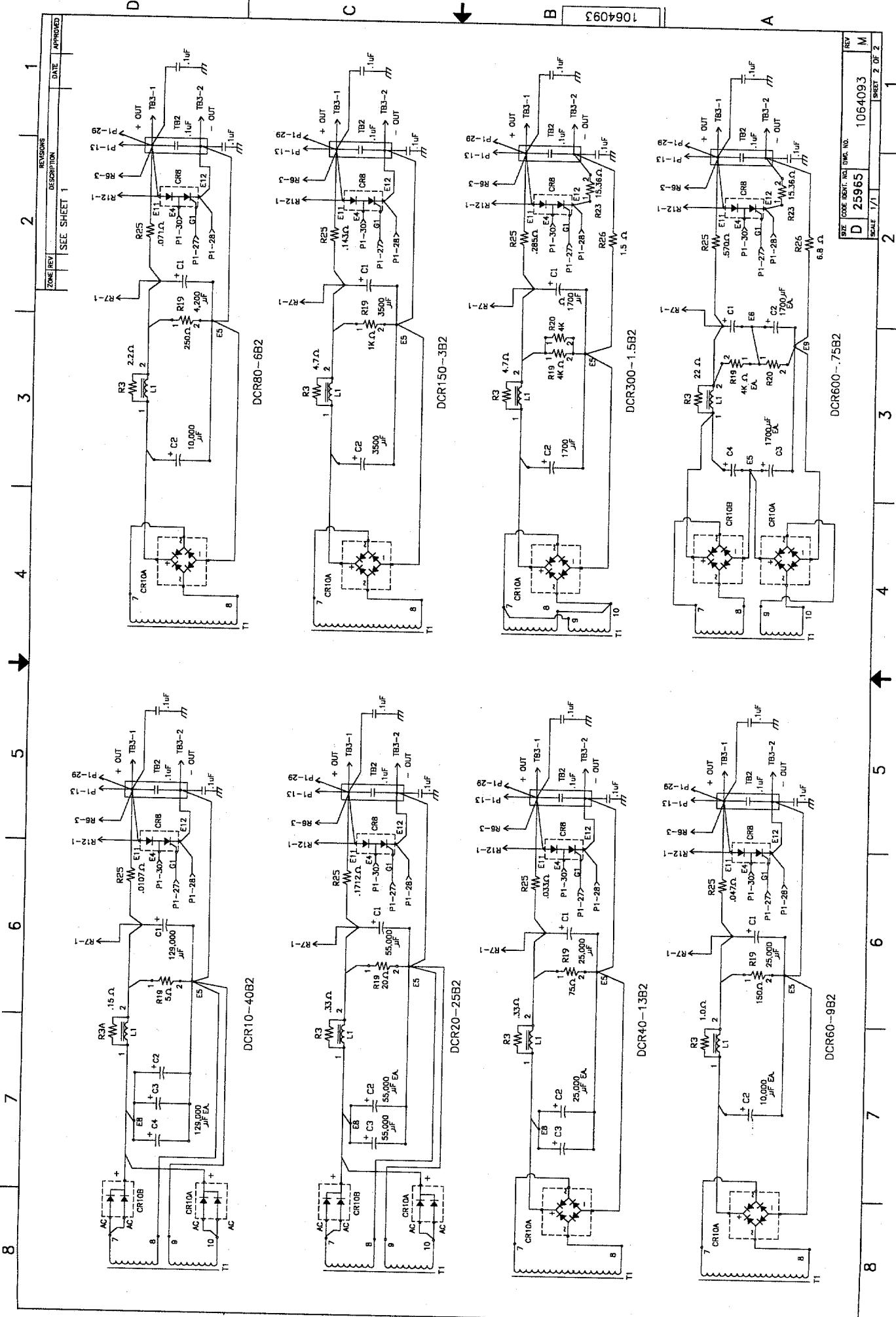
SIZE	CODE IDENT. NO.	NAME NO.	REV.
D	25965	1064468	K
SCALE 1/1			SHEET 1 OF 1

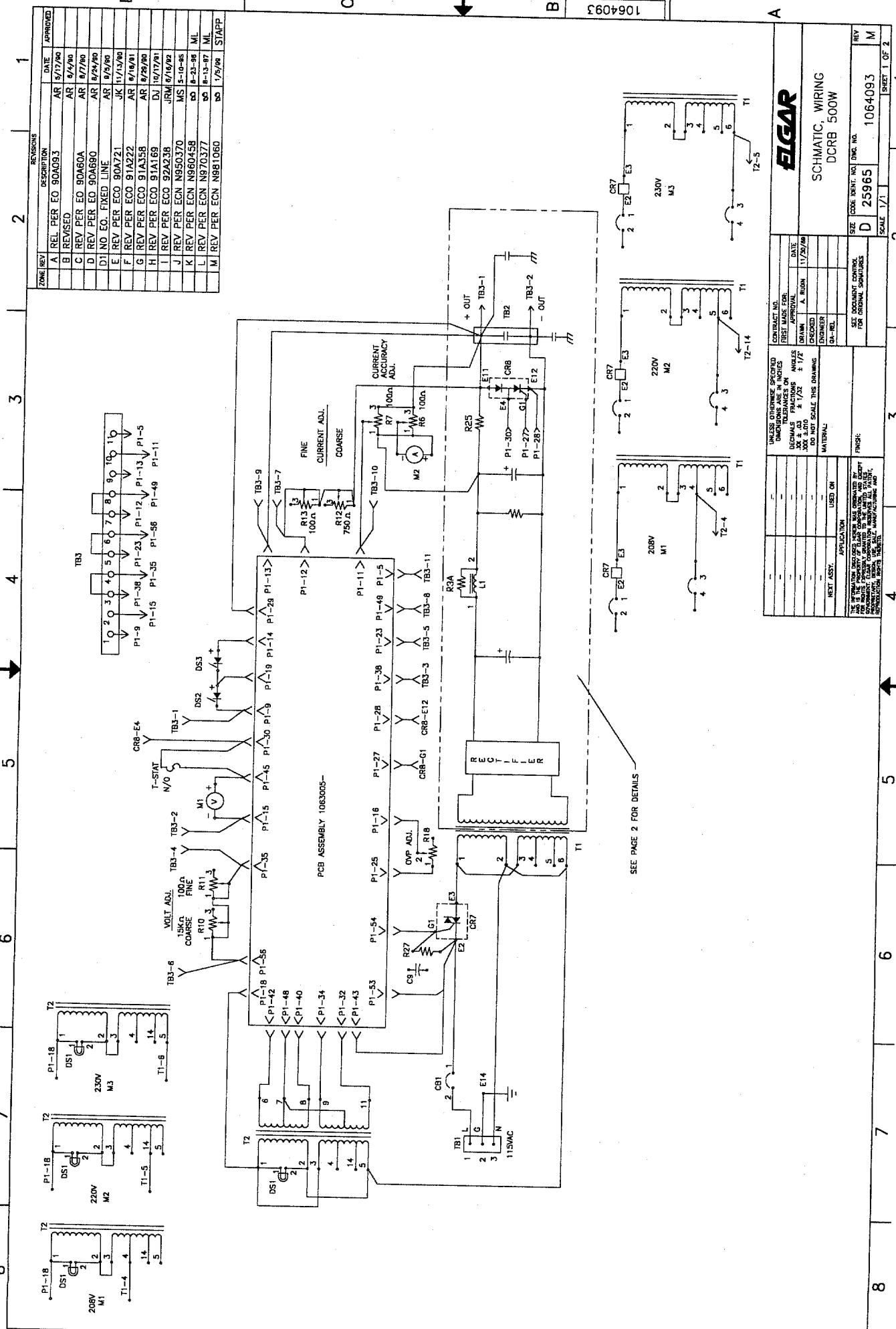
8	7	6	5	4	3	2	1
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8

7

6

5

4

3

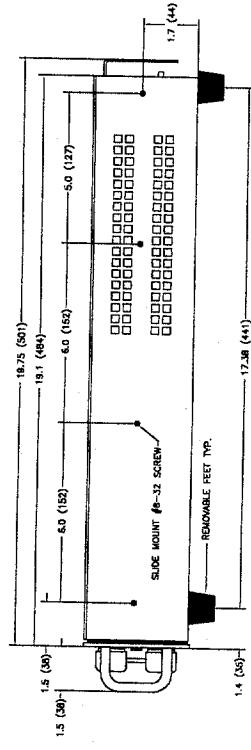
2

1

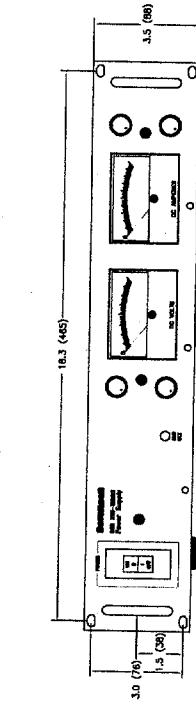
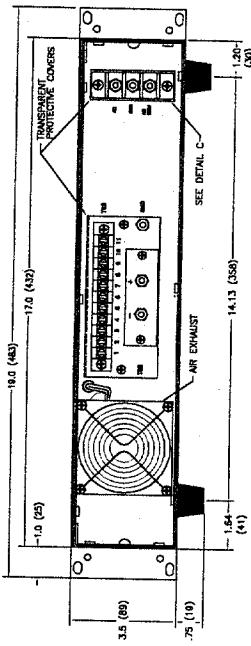
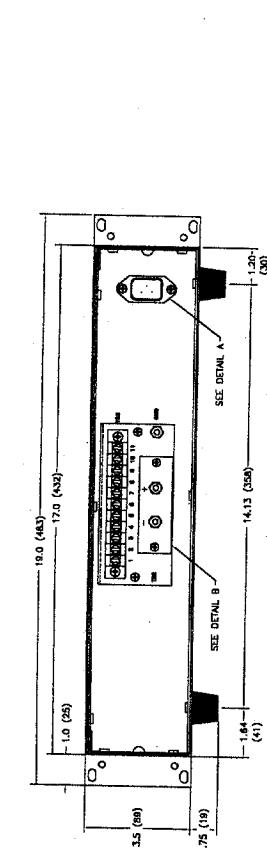
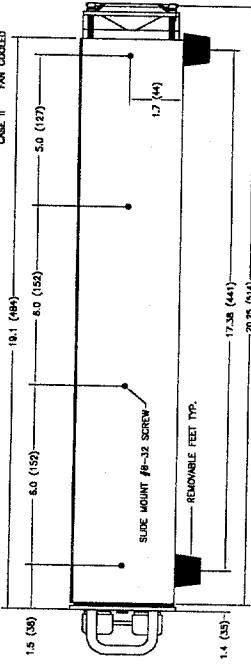
NOTES: UNLESS OTHERWISE SPECIFIED.
 1. ALL DIMENSIONS ARE IN INCHES (mm).
 2. SLIDE-RAIL OPTION AVAILABLE.

ZONE/REV	DESCRIPTION	DATE APPROVED
A	REDRAW FOR CLARITY	MS 4/4/95
B	REV PER ECN N980370	MS 5/10/95

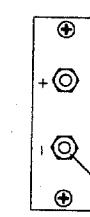
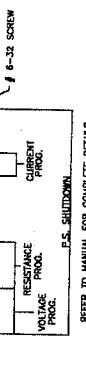
CASE I CONNECTION COOLED



CASE II FAN COOLED



CASE I AND II - FRONT VIEW



1/4-20 STUD
10-32 STUD
SCALE 1/1

DETAIL A
AC INPUT
(CONNECTION COOLED)
SEE DETAIL C
SCALE 1/1

DETAIL B
AC INPUT
(CONNECTION COOLED)
10-32 STUD
1/4-20 STUD
SEE DETAIL C
SCALE 1/1

ELGAR		DWG. OUTLINE DCRB2 3.5"	
CONTRACT NO.	1	DRAWN BY	DATE
FIRST MADE FOR	-	1/2	10/16/95
DECIMALS	-	ANGLE	
FRACTION	-	MIN. & SEC.	
INCHES	-	GRAPH SCALE THIS	
MM & CM	-	DRAWING	
1/16 & 1/32	-	CHECKED	
ASSEMBLY	-	ENGINEER	
NEXT ASSY.	DCRB2	DESIGNER	
APPROVATION	USED ON	DATA REL.	
REVISION		SET DOCUMENT CONTROL FOR EXTERNAL SIGNATURES	
SIZE	CODE IDENT. NO.	DOC. NO.	REV
CODE	1063996	1063996	B
DET. NO.			SCALE 1/2
1			SHEET 1 OF 1

8

6

4

3

2

1

8 | 7 | 6 | 5 | 4 | 3 | 2 | 1

REVISIONS	
ZONE / REV	DESCRIPTION
SEE SHEET 1	

PCB CONTROL ASSY DRAWING NUMBER		500W		1000W	
R4	DER 10-4092	DCR20-2592	DCR20-1382	DCR20-992	DCR20-892
R5				DCR300-1-562	DCR300-1-652
R6				DCR20-2592	DCR20-2592
R7				DCR20-682	DCR20-682
R8				DCR300-1-562	DCR300-1-652
R9				DCR20-2592	DCR20-2592
R10				DCR20-682	DCR20-682
R11				DCR300-1-562	DCR300-1-652
R12				DCR20-2592	DCR20-2592
R13				DCR20-682	DCR20-682
R14				DCR300-1-562	DCR300-1-652
R15				DCR20-2592	DCR20-2592
R16				DCR20-682	DCR20-682
R17				DCR300-1-562	DCR300-1-652
R18				DCR20-2592	DCR20-2592
R19				DCR20-682	DCR20-682
R20				DCR300-1-562	DCR300-1-652
R21				DCR20-2592	DCR20-2592
R22				DCR20-682	DCR20-682
R23				DCR300-1-562	DCR300-1-652
R24				DCR20-2592	DCR20-2592
R25				DCR20-682	DCR20-682
R26				DCR300-1-562	DCR300-1-652
R27				DCR20-2592	DCR20-2592
R28				DCR20-682	DCR20-682
R29				DCR300-1-562	DCR300-1-652
R30				DCR20-2592	DCR20-2592
R31				DCR20-682	DCR20-682
R32				DCR300-1-562	DCR300-1-652
R33				DCR20-2592	DCR20-2592
R34				DCR20-682	DCR20-682
R35				DCR300-1-562	DCR300-1-652
R36				DCR20-2592	DCR20-2592
R37				DCR20-682	DCR20-682
R38				DCR300-1-562	DCR300-1-652
R39				DCR20-2592	DCR20-2592
R40				DCR20-682	DCR20-682
R41				DCR300-1-562	DCR300-1-652
R42				DCR20-2592	DCR20-2592
R43				DCR20-682	DCR20-682
R44				DCR300-1-562	DCR300-1-652
R45				DCR20-2592	DCR20-2592
R46				DCR20-682	DCR20-682
R47				DCR300-1-562	DCR300-1-652
R48				DCR20-2592	DCR20-2592
R49				DCR20-682	DCR20-682
R50				DCR300-1-562	DCR300-1-652
R51				DCR20-2592	DCR20-2592
R52				DCR20-682	DCR20-682
R53				DCR300-1-562	DCR300-1-652
R54				DCR20-2592	DCR20-2592
R55				DCR20-682	DCR20-682
R56				DCR300-1-562	DCR300-1-652

SIZE CODE IDENT. NO. D 25965 M 360646
REV F
SHEET 4 OF 4

REVISIONS			
ZONE	REV	DESCRIPTION	DATE APPROVED
		SEE SHEET 1	

D

B

A

500W		1000W	
POB CONTROL ASSY	DCR10-40B2	DCR20-25B2	DCR40-13B2
DRAWING NUMBER	DCR60-9B2	DCR60-6B2	DCR150-3B2
R57	DCR10-1.5B2	DCR20-2.5B2	DCR60-7.5B2
R58	DCR10-40B2	DCR20-40B2	DCR60-40B2
R59	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R60	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R61	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R62	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R63	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R64	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R65	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R66	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R67	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R68	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R69	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R70	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R71	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R72	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R73	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R74	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R75	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R76	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R77	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R78	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
R79	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
SW1	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
T1	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
T2	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U1	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U2	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U3	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U4	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U5	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U6	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U7	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2
U8	DCR10-1.5B2	DCR20-1.5B2	DCR60-1.5B2

SIZE	CODE	PRINT.	NO.	DOC. NO.	REV
D	25965			M360646	F

2

1

PCB CONTROL ASSY		REVISIONS		APPROVED	
DRAWING NUMBER	ZONE REV	DESCRIPTION	DATE	SEE SHEET	
C8					
C9		235-7395P84	1083005		
C10		24-2015-1			
C11		1084980-1			
C12		235-7444813			
C13		235-7385P67			
C14		24-2037-7			
C15		235-7395P81			
C16		586385-5	586385-5	536385-5	536385-5
C17		235-7395P55			
C18		586385-5	586385-5	536385-5	536385-5
C19		1033881-7			
C20		1034980-2			
C21		1034980-1			
C22		24-2015-11			
C23		235-7395P56			
C24		1033885-8			
C25		24-2037-15			
C26		587626-65			
C27		24-2039-4			
D1		235-7395P67			
D2		586101-9			
D3		586101-15			
D4		586101-17			
D5		586105-7			
D6		586105-3			
D7		586102-12			
D8		586102-13			
D9		586102-12			
D10		322-7238P6			
D11		322-7238P6			
D12		588101-10			
D13		322-7238P6			
D14		322-7238P6			
D15		322-7238P6			
D16		322-7238P6			
D17		322-7238P6			
D18		322-7238P6			
D19		322-7238P6			
D20		322-7238P6			
D21		322-7238P6			
D22		322-7238P6			
D23		322-7238P6			
D24		322-7238P6			
D25		322-7238P6			
D26		322-7238P6			
D27		322-7238P6			
D28		322-7238P6			
D29		322-7238P6			
D30		322-7238P6			
D31		322-7238P6			
D32		322-7238P6			
D33		588102-10			
D34		1033539-3			
D35		322-7238P6			
D36		322-7238P6			
D37		322-7238P6			
D38		322-7238P6			
D39		588102-10			
F1		1033539-3			
Q1		1064104-2			
Q2		1100001-000			
Q3		1064104-2			

500W		1000W	
DCR10-40B2	DCR20-25B2	DCR40-13B2	DCR60-3B2
DCR60-3B2	DCR150-3B2	DCR300-5B2	DCR50-6B2
DCR60-5B2	DCR80-18B2	DCR80-18B2	DCR150-18B2
DCR80-18B2	DCR80-18B2	DCR300-18B2	DCR300-18B2
DCR80-18B2	DCR80-18B2	DCR300-18B2	DCR300-18B2

SIZE	CODE IDENT.	NO. DMC NO.	REV
D	25965	M360646	F
SCALE	1/1	SHEET 2 OF 4	1

NOTES: UNLESS OTHERWISE SPECIFIED.

NOTES: UNLESS OTHERWISE SPECIFIED

5 4 3 2 1

REVISIONS		DESCRIPTION		DATE	APPROVED
ZONE	REV	B	REVISED PER ECN	N910565A	6/16/97
C	REVISED PER ECN	N900442	REVISED PER ECN	N901042	TH/6/98
D	REVISED PER ECN	N911060	REVISED PER ECN	N910114	DO/15/98
E	REVISED PER ECN	N910014	REVISED PER ECN	N900297	2/24/99
F	REVISED PER ECN	N900297	REVISED PER ECN	N900297	2/24/99

		EGLAR		REPLACEMENT PARTS		500/1000W	
		UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES		CONTRACT NO.		REV.	
		DECIMALS	FRACTIONS	DRAWN	APPROVAL	SIZE	CODE IDENT. NO.
		IN & OZ	1/16 & 1/32	DRWNO.	SUBNO.	INCHES	DR. NO.
		DO NOT SCALE THIS DRAWING		CHECKED	LAID OUT	INCHES	
		MATERIAL:		ENGINEER	CHEMIST	INCHES	
		NEXT ASSY.		CH-REL.	DATE	INCHES	
		APPLICATION				INCHES	
							D
							25965
							M360646
							F



**REPLACEMENT
PARTS**

WOODS

M7606

M38083

三