SOLID STATE

BAND-PASS FILTER

MODEL 3500 SERIAL NO.

OPERATING AND MAINTENANCE

MANUAL



KROHN-HITE CORPORATION

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Model 3500

Figure 1. Model 3500 Filter

GENERAL DESCRIPTION

1.1 INTRODUCTION

The Model 3500 Filter, shown in Figure 1, is a variable, electronic band-pass filter that operates at frequencies from 20Hz to 200kHz. The filter consists basically of an input amplifier, a variable high-pass section, a variable low-pass section, and an output amplifier. The high-pass and low-pass sections are connected in series. The overall gain of the Filter is unity(0db). The cutoff frequencies of both the high-pass and low-pass sections can be adjusted independently over the full frequency range of 20Hz to 200kHz.

An optional rack-mounting kit, (Part No. RK-38) is available from Krohn-Hite, for installing the unit in a standard 19" rack spacing.

1.2 GENERAL SPECIFICATIONS

Frequency Range

Continuous coverage from 20Hz to 200kHz for both high cut-off and low cut-off frequencies independently. Frequency range is covered by separate calibrated dials and four-decade band switches. Center frequency and width of pass band in bandpass mode are continuously adjustable over the entire frequency range.

BAND	MULTIPLIER	FREQUENCY (Hz)
1	1	20 - 200
2	10	200 - 2,000
3	100	2,000 - 20,000
4	lK	20,000 - 200,000

Frequency Dials

Each dial is engraved and individually hand-calibrated with a single logarithmic scale reading directly in cycles per second, from 19 to 210. Dials are 2 inches in diameter with an effective scale length of 6 inches per band, giving a total effective scale length of 24 inches for the range of 20Hz to 200kHz.

Accuracy of Cut-off Frequency Calibration

±10% with "Response" switch in "max-flat" (Butterworth) position; less accurate in "Low Q" position. Relative to mid-band level, the filter output is down 3db at cutoff in "max-flat" position, and approximately 12db in "Low Q" position.

Bandwidth

Continuously variable within the cutoff frequency limits of 20Hz and 200kHz. For minimum pass-band (Butterworth response) the two cutoffs are set to the same frequency, resulting in an insertion loss of 6db at that frequency, with 3db points at factors of .8 below it and 1.25 above it.

Response Characteristics

Choice of 4 pole Butterworth (maximally flat response) for frequency domain operation and Low Q (damped response) for transient-free time domain operation, selected by means of a switch on rear of chassis.

Pass-Band Gain

Zero db ±1 db in pass band.

Input Characteristics, Impedance

Approximately 10 megohms in parallel with 50 pf. Maximum input amplitude: 5 volts rms up to 2MHz. Maximum dc component: 100 volts.

Output Characteristics, Impedance

Approximately 50 ohms. Maximum Voltage ± 7 volts peak. Maximum Current ± 5 ma peak. Internally generated hum and noise: Less than 200 microvolts. (Slightly higher for 400 Hz operation.)

Attenuation Slope

Nominal 24db per octave each side of pass-band.

Maximum Attenuation

Greater than 60 db.

Controls

Front panel; LOW CUT-OFF FREQUENCY dial and multiplier switch. HIGH CUT-OFF FREQUENCY dial and multiplier switch. POWER OFF-ON switch. Rear panel; RESPONSE switch, GROUND switch, 115/230V LINE switch.

Terminals

Front panel, two BNC connectors, one for INPUT and one for OUTPUT. Rear of chassis, two BNC connectors, one for input and one for output. An additional multipurpose binding post for CHASSIS GROUND is provided on the rear panel. An AC power receptacle with detachable line cord is also provided.

Power Requirements

105-125 or 210-250 volts, single phase; 50-400 Hz, 10 watts. Hum and noise are increased by a factor of approximately two for 400Hz operation.

Fuse Protection

1/8 ampere slow-blow for 115 volts, 1/16 ampere slow-blow for 230 volts.

Dimensions and Weights

Model	Overall I	erall Dimensions (inches)			Weight (lbs.)
3500	8 1/2 wide	3 1/2 high	13 deep	9 net	14 shipping

1.3 FILTER CHARACTERISTICS

Bandwidth Adjustment

The flexibility of adjustment of bandwidth is illustrated in Figure 2. Band-pass operation in the MAXimally FLAT or Butterworth mode for two different band-widths is illustrated by curves A and B. Curve B shows the minimum pass-band width obtained by setting the two cutoff frequencies equal. In this condition the insertion loss is 6 db, and the -3 db cutoff frequencies occur at 0.8 and 1.25 times the mid-band frequency. The minimum pass-band for a 0 db insertion loss is shown by curve A with the cutoffs set at 0.5 and 2 times the mid-band frequency.



Figure 2. Normalized Frequency

Transient Response

The frequency response characteristic of this Filter closely approximates a fourthorder Butterworth with maximal flatness, ideal for filtering in the frequency domain. For pulse or transient signal filtering, a response switch is provided to change the frequency response to Low Q, optimum for transient-free filtering. Figure 3 shows a comparison of the Filter output response in these modes to a square wave input signal.



Figure 3. Square Wave Response

Cutoff Response

The attenuation characteristics of the Filter are shown in Figure 4. With the response switch in the MAXimally FLAT or Butterworth mode, the gain, as shown by the solid curve, is virtually flat until the -3db cutoff frequency. At approximately two times the cutoff frequency the attenuation rate coincides with the 24 db per octave straight line asymptote. In the Simple RC mode, optimum for transient-free filtering, the dotted line shows that the gain is down approximately 12 db at cutoff and reaches 24 db per octave attenuation rate at five times the cutoff frequency. Beyond this frequency the filter attenuation rate and maximum attenuation, in either mode, are identical.



Figure 4. Normalized Attenuation Characteristics

Phase Response

The phase angle at any frequency is the sum of the angles due to the high-pass and low-pass sections of the Filter. Figure 5 gives the phase characteristic for either section in degrees lead (+) or lag (-), as a function of the ratio of the operating frequency f to low cut-off frequency $f_{\rm L}$ or high-cutoff frequency $f_{\rm H}$.

The solid curve is for the maximally flat or Butterworth mode and the dotted curve is for Low Q.





Example

Determine the phase shift through the filter, in the maximally flat or Butterworth mode with the low cutoff (f_L) at 200 Hz, the high cutoff (f_H) at 600 Hz and an input frequency (f) at 300 Hz.

Phase shift due to low cutoff (f_{T})

$$\frac{f}{f_{\rm L}} = \frac{300}{200} = 1.5$$

from Figure 6 $1.5 = +110^{\circ}$

Phase shift due to high cutoff (f_{I})

$$\frac{f}{f_H} = \frac{300}{600} = .5$$

from Figure 6 $.5 = -80^{\circ}$

Total phase shift

 $= +110^{\circ} - 80^{\circ} = +30^{\circ}$



Filter, 3500

OPERATION

2.1 INTRODUCTION

The Filter is adjusted and checked carefully before shipment to insure that it meets all specifications. It is then aged and again tested to be sure that it is ready for use. The Filter is shipped complete, and after unpacking, is ready to be turned on and used.

Unpack the Filter carefully and inspect it for damage that may have occurred during shipment. Check the case for damage, and check for loose sub-assemblies and parts. Check all front panel controls for freedom of operation. The recommended operating procedure is described below.

The rms voltage of the input signal should not exceed 5 volts. The dc component of the input signal should not exceed 100 volts.

2.2 FRONT PANEL CONTROLS

The front panel controls consist of two identical frequency dials and associated multiplier switches used to set cut-off frequencies, a power on-off switch, and an indicator light.

Each frequency dial is calibrated with a single logarithmic scale reading directly in cycles per second from 19 to 210. The dials are two inches in diameter with an effective scale length of approximately six inches per band, giving total effective scale length of approximately 24 inches for the 20Hz to 200kHz frequency range. The left-hand dial (LOW CUT-OFF FREQUENCY) and band multiplier switch select the low cut-off frequency, and the right-hand dial (HIGH CUT-OFF FREQUENCY) and multiplier switch select the high cut-off frequency.

Each of the two multiplier switches has four positions, covering the frequency ranges as shown in Section 1.2.

2.3 REAR PANEL CONTROLS

The rear panel controls consist of a RESPONSE switch, a GROUND switch, and a 115/230V LINE switch. The RESPONSE switch is used to select either a Butterworth (max-flat) or a Low Q response. The GROUND switch is provided to disconnect the signal ground from the chassis. The LINE switch is used when changing from 115V to 230V AC operation.

2.4 OPERATION

To operate the Filter, proceed as follows:

- a. Make appropriate power connections as described in Section 2.6.
- b. Make appropriate connections to INPUT and OUTPUT terminals of filter.
- c. Set cut-off frequencies by means of the band multiplier switches (CUT-OFF FREQUENCY) and the frequency dials.
- d. Turn POWER switch to ON.

NOTE

The left-hand band multiplier switch and frequency dial are used to select the low cut-off frequency and the right-hand controls select the high cut-off frequency.

The minimum pass-band is obtained by setting the high cut-off frequency equal to the low cut-off frequency.

2.5 TERMINALS

<u>INPUT</u> - A BNC type connector is provided on the left side of the front panel. A parallel BNC coaxial connector is located on the rear of the chassis.

<u>OUTPUT</u> - A BNC type connector is provided on the right side of the front panel. A parallel BNC coaxial connector is located on the rear of the chassis.

<u>CHASSIS GROUND</u> - An additional combination-type binding post is provided on the rear panel.

AC INPUT - A power receptacle with detachable line cord is located on the rear panel.

2.6 LINE VOLTAGE AND FUSES

The Filter may be operated from an AC power source of either 105-125 volts, 50-400 Hz, or 210-250 volts, 50-400 Hz. A 115/230V LINE switch, located on the rear panel, selects the filter's mode of operation. When the AC line is 115V, move the LINE switch to the 115V position. In this mode, a 1/8 ampere slo-blo fuse must be used. When the filter is to be operated from 230 VAC, move the LINE switch to the 230V position, and replace the fuse with a 1/16 ampere slo-blo type.

CIRCUIT DESCRIPTION

3.1 INTRODUCTION

As shown below in the simplified block diagram, Figure 7, the filter consists of an input amplifier, for isolation; a four pole low-pass section (high cutoff frequency), with four R. C. filter networks which are adjustable by means of a gauged potentionmeter assembly and bandswitch; and a four pole high pass section (low cutoff frequency), with four R. C. filter networks and a similar ganged potentionmeter assembly and bandswitch. Both cutoff frequencies are tuned continuously within each decade by the potentionmeter assemblies. The capacitors are tuned in decade steps by the bandswitch.



Figure 7. Simplified Schematic Diagram

3.2 DETAILED DESCRIPTION

3.2.1 Input Amplifier

The input signal is capacitor coupled through C101 to the input amplifier consisting of Q101 and Q102. The input impedance determined by R101 is 10 megohms. The high input impedance of the F. E. T. Q101 is negligible. The input amplifier is provided to isolate the input signal and supply a low impedance driving source for the first R. C. network.

3.2.2 High Pass Section

The high pass section consists of a pair of two pole filters, each adjusted to provide the proper Butterworth response characteristics when cascaded. Buffer amplifiers are used to isolate the two pole R. C. networks. The Buffer Amplifier, consisting of Q201 and Q202, following the first 2 pole network provides isolation and drives the next R. C. network. Q203 furnishes feedback to the emitter follower stage for corner frequency peaking. The signal then enters another Buffer Amplifier stage consisting of Q204 and Q205, again providing isolation and a low impedance source to drive the next R. C. network. Q206 and Q207 perform as a buffer amplifier between the high-pass and low-pass sections with Q208 providing enough feedback to Q204 to produce the correct Butterworth response. With switch S901 in the grounded position, the feedback is reduced to produce the Low Q (damped response) for transit free time domain operation.

3.2.3 Low Pass Section

The low pass section also consists of a pair of two pole filters each adjusted to provide the proper Butterworth response when cascaded.

The pair of two pole R. C. networks are isolated from each other with a buffer amplifier which is made up of two emitter followers.

The output from the high-pass section is fed into the first two-pole R. C. network before the buffer amplifier consisting of O301 and Q302. A portion of the output from Q302 is fed back to the R. C. network via Q303 to obtain the desired characteristics from this two pole section. The buffer amplifier also provides a low impedance source for driving the next pair of R. C. filters. Q304 and Q305 provide isolation and a low impedance source to drive the output. A portion of the output from Q305 is fedback through amplifier Q306 to obtain the proper Butterworth response characteristics. With switch S901 in the grounded position the feedback is reduced to a low Q (damped response) for transit free time domain operation. The output from Q305 passes through C303 and R411 to the output terminals.

3.2.4 RC/Butterworth Response

To prevent ringing and overshoot, caused by fast rise-time pulses, the filter may be operated in the low Q position. S901 is provided to reduce the feedback to the second two pole filter in each section.

3.2.5 Power Supplies

A dual power supply is incorporated, providing plus and minus 15 volts. One full wave bridge rectifier (CR501, CR504, CR505, CR506) and filter capacitors C501 and C502 provide the necessary unregulated d-c voltage levels.

The + 15V supply consists of Q502 (used as a Zener Reference), amplifier Q503, and series regulator Q501. A change in the regulated output is fed through Q502 and CR502 to the emitter of Q503, and, attenuated in the divider R511 and R501, R506, to the base of Q503. The resulting change in Q503 current drives the base of series transistor Q501 in the proper direction to restore the regulated voltage to + 15V. The -15V supply works in the same manner.

Additional feedback is provided to both amplifiers via R505 and R508 to minimize power supply ripple.

INCOMING ACCEPTANCE AND INSPECTION

4.1 INTRODUCTION

The following procedure should be used to verify the Filter operation within specifications. These checks may be used for incoming inspection and periodic specification checks. Tests must be made with all covers in place. If the instrument is not operating within specifications refer to Section 5 before attempting any detailed maintenance.

4.2 TEST EQUIPMENT REQUIRED

The following test equipment is required to perform these adjustments:

- a. RC Oscillator, with frequency range .01Hz to 1MHz, frequency accuracy +0.5% to 100KHz, frequency response better than +.05db and distortion less than .02%, Krohn-Hite Model 4100A or equivalent.
- b. Oscilloscope, with DC to 50MHz bandwidth, vertical input sensitivity of lmv/cm, Tektronix type 544, with type 1A5 plug-in, or equivalent.
- c. AC Voltmeter, capable of measuring 100 microvolts to 10 volts RMS, Ballantine Model 314A or equivalent.
- d. DC Voltmeter, capable of measuring 1 millivolt to 20 volts, Fluke Model 8000A or equivalent.
- e. Variable auto-transformer for adjusting line voltage.

4.3 DIAL ACCURACY

a. Set high cutoff to 200KHz. Set response switch to max flat position. Set low cutoff dial to 20, 40, 100, 200 on each of the multiplier positions. At each point, set oscillator to frequency corresponding to dial and multiplier setting. With 1 volt input, output should read between 0.6V and 0.8V (-3db±1.5db) at all frequencies except 200KHz will read approximately 0.5 volts (-6db) due to interaction of high cutoff setting.

b. Repeat measurements with response switch in low Q position. Output reading should be approximately 0.25 volts (-12db) at all frequencies except 200 KHz. c. Set low cutoff to 20Hz. Set response switch to max flat position. Set high cut off dial to 20, 40, 100, 200 on each of the multiplier positions. At each point, set oscillator to frequency corresponding to dial and multiplier setting. With 1 volt input, output should read between 0.6V and 0.8V (-3db±1.5db) at all frequencies except 20 Hz. 20Hz will read approximately 0.5V (-6db) due to interaction of low cutoff frequency.

d. Repeat measurements with response switch in Low Q position. Output reading should be approximately 0.25V (-12db) at all frequencies except 20Hz.

4.4 ATTENUATION SLOPE

a. Set high cutoff to 200 KHz and response switch to max flat position. Set low cutoff dial to 60. On each low cutoff multiplier position set oscillator to one half the frequency indicated by the low cutoff dial and multiplier setting. Output should read -24db±3db from input at each frequency.

b. Set low cutoff to 20Hz. Set high cutoff dial to 60. On each high cutoff multiplier position, set oscillator to twice the frequency indicated by the high cutoff dial and multiplier setting. Output should read -24db±3db from input at each frequency.

4.5 PASS-BAND GAIN

Set low cutoff to 20Hz and high cutoff to 200KHz. Set oscillator to 1 volt. At 50 Hz, 500 Hz, 5 KHz and 50 KHz the output should be 1±.1 volt (0db±1db).

4.6 MAXIMUM ATTENUATION

a. Set both cutoff frequencies to 200KHz. Set oscillator input to filter at 5 volts, 20KHz. Output of filter should measure less than 5 millivolts (-60db).

b. Set both cutoff frequencies to 20KHz. Set input to filter to 5 volts, 200KHz. Output of filter should measure less than 5 millivolts (-60db).

4.7 OUTPUT CHARACTERISTICS

a. Maximum Voltage:

Set low cutoff to 20Hz and high cutoff to 200KHz. Set input frequency to lKHz and increase input voltage until clipping is observed on output. Output should measure greater than 14 volts peak to peak before clipping is observed.

b. Maximum Current:

Connect 50 ohm resistor across output. Adjust input to obtain 0.5 volts peak to peak across 50 ohm resistor. Output should show no observable distortion.

c. Impedance:

Set output to 0.1 volt rms open circuit. Connect 50 ohm resistor to output. Voltage should drop to 0.05 volts.

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4.8 HUM AND NOISE

Remove oscillator. Short input to filter. Output should measure less than 200 microvolts rms.

MAINTENANCE

5.1 INTRODUCTION

If the Filter is not functioning properly and requires service, the following procedure may facilitate locating the source of trouble. Access to the interior of the filter is accomplished by removing the four screws centered at the rear of each cover; sliding off the side covers will unlock the top and bottom covers.

The general layout of major components, test points, screwdriver controls and adjustments is shown in Figure 9. Detailed component layout of the printed circuit card, Figure 11, is located on foldout attached to the inside rear cover. Various check points and voltages are shown on the Schematic Diagram and are also marked on the printed circuit card.

Many troubles may easily be found by visual inspection. When a malfunction is detected, make a quick check of the unit for such things as broken wires, burnt or loose components, or similar conditions which could be a cause of trouble. Any trouble-shooting of the Filter will be greatly simplified if there is an understanding of the operation of the circuit. Before any detailed troubleshooting is attempted, reference should be made to Circuit Description, Section 3, to obtain this understanding.

5.2 POWER SUPPLY

If the filter does not seem to be working properly the two power supplies should be checked first. If the plus 15 and minus 15 volt supplies appear to be correct refer to signal tracing analysis, Section 4.3.

Any malfunction of the power supplies will generally cause a large error in the plus or minus 15 volt supplies. Small errors of the plus or minus supplies may be corrected by adjusting R506 and R509 respectively. If the minus 15 volt supply is correct and the plus 15 volt supply is incorrect, check the reference voltage from the emitter of Q503 to the collector of Q502. If this reference voltage is 8.4 \pm .5 and the plus 15 volt supply is high, the base to emitter voltage of Q503 will be reduced, decreasing its collector current lowering the emitter to base voltage and turning off Q501. This will increase the emitter to collector voltage of Q501, correcting the plus 15 volt supply. The failure will be found where this action is blocked. If the plus 15 volt supply is low, the current in Q503 will be increased, turning on Q501. If the supply voltage is low and Q503 and Q501 appear to be operating properly, the cause is most likely excessive current in the main filter section. An incorrect minus 15 volt supply may be traced in a similar manner.

5.3 SIGNAL TRACING ANALYSIS

If the power supplies appear to be correct but the Filter is not working, the following signal tracing analysis should locate the area of malfunction:

Set response switch to low Q position. Set both the low and high cutoff frequencies to IKHz. Connect a IKHz 5 volt rms sine wave signal to the input terminals. If the test signal does not appear correctly at the output, the area of the malfunction may be localized by determining where in the Filter the signal first deviates from normal.

Figure 8 shows various test points with their correct signal levels. If a test point is found whose signal level differs appreciably from the correct value, the circuitry immediately preceding that test point should be carefully checked.

5.4 TUNING CIRCUITS

If signal tracing shows one of the tuning circuits to be faulty, it should be determined if the trouble is in the resistive or capacitive element. If the trouble is in a capacitive element associated with the lowest or highest multiplier range, the malfunction will appear only on these positions. Any other defective tuning capacitors will introduce an error in adjacent bands. If there is a problem in a resistant element, the trouble will be of a general nature and will show up on all multiplier bands.

The range-determining capacitors associated with the band multiplier switches S701 and S702 are specially selected for close capacitance tolerance. All capacitor

	CORRECT
	SIGNAL LEVEL
TEST POINTS	(RMS VOLTS)
1	5.0
2	4.9
3	2.8
4	2.8
5	2.6
6	1.6
7	1.6
8	1.3
10	1.3
13	. 43
14	. 70
15	.67
16	. 18
17	. 31
18	. 30
20	. 14



values fall within $\pm 5\%$ of the specified value, but in order to maintain accurate frequency calibration over the entire dial range and also between decade ranges, the capacitors are matched within $\pm 2\%$ of each other and generally within $\pm 2\%$ in decade ratios.

The values of capacitance used on the highest band is selected to compensate for stray capacitance and are therefore not completely in decade ratios of those used on the lower bands.

For replacement purposes, a capacitor within $\pm 1\%$ of the specified value can be used with negligible effect on the overall calibration accuracy. If more than one capacitor on a particular range is to be changed, it is recommended that several other capacitors on the switch be carefully measured on a capacitance bridge to determine the average percentage deviation from the nominal value. Any capacitors except those used on the two highest frequency ranges may be measured to determine this tolerance. Replacement can then be made with capacitors of the exact value, and calibration will not be impaired.

Each of the variable resistance elements consists of four potentiometers ganged together with a gear assembly. Each potentiometer has series and shunt trims to insure proper tracking. The trims and the angular orientation of the potentiometers are carefully adjusted at the factory. If it becomes necessary to change one of these potentiometers in the field, it should be replaced only with a unit supplied by the factory complete with proper trims. The angular orientation should then be carefully adjusted following the procedure supplied with the parts.

Filter, 3500



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CALIBRATION AND ADJUSTMENT

6.1 INTRODUCTION

Before attempting any adjustments the procedure in Section 4 should be followed to determine if adjustments are necessary. The following procedure is provided for the purpose of facilitating the adjustment and calibration of the filter in the field, and adherence to this procedure should restore the filter to its original specifications. If any difficulties are encountered, please refer to Maintenance, Section 5. If any questions arise which are not covered by this procedure, please contact our factory service department. The location of all major components, modular subassemblies, test points, screw driver controls and adjustments are shown in Figure 9.

Access to the interior of the filter is accomplished easily by removing the four screws centered at the rear of each cover; sliding off the side covers will unlock the top and bottom covers.

6.2 TEST EQUIPMENT REQUIRED

AS LISTED IN SECTION 4.2.

6.3 INITIAL SETUP

- a. Set low cutoff dial to 60, multiplier to x10.
- b. Set high cutoff dial to 200, multiplier to x1K.

6.4 POWER SUPPLY

- a. Short filter input. Connect d-c voltmeter between signal ground and plus 15 volts. (positive end, C505)
- b. Adjust R506 for 15+0.2 volts.
- c. Connect d-c voltmeter between signal ground and minus 15 volts. (negative end of C506)
- d. Adjust R509 for 15+0.2 volts.
- e. Remove short.

6.5 LOW-CUTOFF SECTION RESPONSE

- a. Connect oscillator output to filter input.
- b. Set oscillator to 6KHz and adjust amplitude for 1 volt at filter input.
- c. Connect AC voltmeter to point "10".
- d. Adjust R226 for reading of 1V, +.02V
- e. Set oscillator to 600Hz.
- f. Adjust R225 for a reading of .7 volts at point "10".

6.6 LOW-CUTOFF DIAL SETTING

- a. Set oscillator frequency to 3 KHz.
- b. Adjust voltage for 1 volt at point "10".
- c. Set oscillator to 300 Hz.
- d. Adjust low cutoff dial for . 063 volts (-24db from 1 volt) at point "10".
- e. If necessary, loosen dial set screws and set dial at 60.

6.7 LOW CUTOFF X1K MULTIPLIER CALIBRATION

6.7.1 Step 1

- a. Set low cutoff dial to 20, multiplier to xlK.
- b. Set oscillator to 100KHz and connect AC voltmeter to point "4".
- c. Adjust voltage at point "4" for 1V rms.
- d. Switch oscillator to 5KHz.
- e. Adjust C707 for . 06 volts (-24.5db from 1 volt) at point "4".
- f. Repeat steps b through f until no additional adjustment is required.

6.7.2 Step 2

- a. Set oscillator to 100KHz and connect AC voltmeter to point "10".
- b. Adjust voltage at point "10" for 1 volt rms.
- c. Switch oscillator to 10KHz.
- d. Adjust C717 for .063 volts (-24db from 1 volt) at point "10".
- e. Repeat steps a through e until no additional adjustment is required.

6.8 200KHZ CALIBRATION

- a. Set low cutoff dial to 200, multiplier to xlK.
- b. Set oscillator to 600 KHz.
- c. Adjust oscillator for 1 volt at point "10".
- d. Switch oscillator to 200KHz.
- e. Trim C741 for 0.7±.05 volts at point "10".

6.9 HIGH CUTOFF DIAL SETTING

- a. Set low cutoff dial to 20, multiplier to xl.
- b. Set high cutoff dial to 60, multiplier to x10.
- c. Set oscillator frequency to 100 Hz.
- d. Adjust oscillator voltage for 1 volt at filter output.
- e. Switch oscillator to 1.2 KHz.
- f. Adjust high cutoff dial for .063 volts (-24 db from 1 volt) at output.
- g. If necessary, loosen dial set screws and set dial at 60.

6.10 HIGH CUTOFF X1K MULTIPLIER CALIBRATION

- a. Set high cutoff dial to 60, multiplier to x1K.
- b. Set oscillator to 6 KHz.

- c. Adjust oscillator voltage for 1 volt at filter output.
- d. Switch oscillator to 48KHz.
- e. Adjust C727 for a reading of . 94 volts at filter output.
- f. Switch oscillator to 60 KHz.
- g. Adjust C737 for a reading of 0.7+.05 volts at filter output.
- h. Repeat steps d through g until no further adjustment is required.



			R	SISTORS		
Symbol	Description	Mir.	Part No.	Symbol R500	Description	Mfr. Port No.
R101 #102 #103 R104 #105 R106 R107 R109 R109 R109 R109 R201 R202 R204 R203 R204 R205 R204 R205 R204 R205 R204 R205 R204 R205 R204 R205 R204 R205 R204 R205 R206 R209 R211 R211 R211 R211 R211 R215 R215 R215 R216 R217 R218 R217 R218 R219 R219 R219 R220 R220 R220 R220 R220 R211 R217 R218 R219 R219 R220 R220 R220 R220 R220 R220 R210 R210 R210 R210 R205 R206 R206 R208 R209 R211 R212 R217 R218 R217 R218 R219 R219 R220 R220 R220 R220 R220 R220 R210 R210 R210 R210 R210 R210 R210 R210 R210 R210 R210 R210 R205 R206 R208 R208 R210 R211 R212 R214 R217 R218 R217 R226 R220 R220 R200 R200 R200 R200 R200 R200 R200 R210 R210 R217 R218 R217 R218 R227 R226 R220 R220 R220 R220 R220 R220 R220 R210 R217 R218 R220 R222 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R220 R200 R300 R300 R300 R300 R300 R300 R300 R300 R300 R300 R300 R311	10.M. 10% 1/4W 1M. 10% 1/4W 100 10% 1/4W 12. 10% 1/4W 14. 10% 1/4W 470 20% 1/4W 510 5% 1/4W 6.8K 10% 1/4W 470 20% 1/4W 470 20% 1/4W 470 20% 1/4W 470 20% 1/4W 1.4K 5% 1/4W 240 5% 1/4W 240 5% 1/4W 240 5% 1/4W 1.4K 5% 1/4W 1.4K 5% 1/4W 1.4K 5% 1/4W 100 20% 1/4W 470 20% 1/4W 3.3K 10% 1/4W 470 20% 1/4W 1.4W 100 10% 1/4W 470 20% 1/4W 100 10% 1/4W 470 20% 1/4W 100 10% 1/4W 470 20% 1/4W	AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	CB1061 CB1051 CB1011 CB1011 CB1021 CB4712 CB4712 CB6821 CB6821 CB6712 CB6821 CB6712 CB6821 CB6712 CB6712 CB6722 CB6831 CB1012 CB6712 CB6722 CB1012 CB6722 CB1012 CB6722 CB6831 CB1011 CB1021 CB6712 CB6721 CB772 CB6721 CB772 CB6721 CB6721 CB772 CB6721 CB6721 CB6721 CB772 CB6721 CB772 CB772 CB6721 CB772 CB6721 CB6722 CB772 CB	R312 R312 R312 R314 R314 R316 R316 R317 R316 R316 R316 R316 R316 R316 R316 R316	1% 10% 1/4W 1,5K 10% 1/4W 3,9K 5% 1/4W 100 20% 1/4W 470 20% 1/4W 68K 5% 1/4W 3,9K 10% 1/4W 3,9K 10% 1/4W 100 20% 1/4W 100 10% 1/4W 100 10% 1/4W 10% 10% 1/4W 5K POT 5K POT 5K 10% 1/4W 5.6K 10% 1/4W 100 20% 1/4W 10% 10% 1/4W 10% 10% 1/4W 10% 10% 1/4W 10% 10% 1/4W	AB CB1921 AB CB1921 AB CB1921 AB CB1912 AB CB1912 AB CB4712 AB CB4712 AB CB4712 AB CB4712 AB CB1012 AB CB1012 AB CB1012 AB CB1012 AB CB1021 AB CB1921 AB CB1021 AB CB1021 AB CB1921 AB
	4/0 20/0 1/4/1			PACITORS	1000 1078 1740	Au Catori
Symbol C101	Description	Mfr. ERT	Part No. 8131-100-651-104M	Symbol C713	Description	Mfr. Part No.
C102 C103 C104 C201 C202 C203 C204 C205 C301 C302 C303 C501 C302 C503 C504 C505 C505 C505 C505 C505 C505 C505	c20pf T0% S00v 1000pf 20% S00v 100pf 10% S00v S00mf S0V S00mf S00mf S0V 4mf 20% S0V 10% 10mf 10% 100v .02amf 10% S00v .01mf +1% 200v .3% .01mf +1%	ELM SP ELM ELM ELM ELM ELM ELM ELM ELM SP SP SP SP SP SP CD CD TRW TRW TRW TRW TRW TRW	DMI9C621K C0238901E102M C0238901E102M C0238901E102M DMI9C101K DMI9C101K DMI9C101K DMI5C101K DMI5C101K T501N022GTIA1P 62D43063 62D43063 62D43063 62D43063 62D43063 1960105X0035D8 1960105X0035D8 1960105X0035D8 1960105X0035D8 1960105X0035D8 1960105X0035D8 X663F X663F X663F	C714 C715 C716 C717 C721 C722 C723 C724 C725 C726 C726 C727 C731 C732 C733 C734 C733 C734 C735 C736 C737 C736 C737 C736 C737 C736 C736	. Imf +1% 200V -3% .01mf +1% 200V -3% 1000pf 5% 500V B2pf 100% 50% 500V 4-40pf TRIMMAER 10mf +1% 50V -3% .1mf +1% 200V -3% .01mf +1% 200V -3% .01mf +1% 200V -3% 1000pf 5% 500V 62pf 10% 500V 62pf 10% 500V -3% .01mf +1% 200V -3% .01mf +1% 200V -3% .01mf +1% 200V -3% .01mf +1% 200V -3% .01mf +1% 50V -3% .01mf +1% 50V -3% .01mf +1% 500V -3% .01mf +1% 500V -3% .01mf +1% 500V -3% .01mf +1% 500V -3% .01mf +1% 500V -3% .01mf +1% 500V -3% .01mf +1% 500V .01mf +1% 500V .000V	TRW X663F TRW X663F ELM CM19C102J ELM T50310 TRW X663F ELM C19C102J ELM DM15C510K ELM T50310 ELM T50210 ELM T50210 ASP 9212-68910
				, DIODES, MISC.		
Symbol	Description	Mfr.	Port No.	Symbol	Description	Mfr. Part No.
Q101 Q202 Q203 Q204 Q205 Q204 Q205 Q206 Q206 Q207 Q208 Q301 Q303 Q304 Q305 Q306 Q306 Q301	2N4302 MP56518 MP56515 MP56515 MP56515 MP56515 MP56518 2N4302 MP55518 MP56516 MP56516 MP56515 MP56515 MP56515 MP56515 2N4234	AME MOT MOT MOT MOT MOT MOT MOT MOT MOT MOT	2N4302 MPS6518 MPS6518 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515 MPS6515	L201 L301 L302 L303 P601 P603 P604 P605 P606 P606 P606 F901	FERRITE BEAD 10Hy 10% 1/4W 10Hy 10% 1/4W 250K 10% 2W 25K 10% 2W 25K 10% 2V 90K 10% 2V 90K 10% 2V 25K 10% 2V 90K 10% 2V 25K 10% 2V 10% 2V 10% 2V 10% 2V 10% 2V 10% 2V 10% 10% 10% 2V 10% 10% 10% 2V 10% 10% 10% 2V 10% 10% 2V 25% 10% 10% 2V 25% 10% 10% 2	STK S7-0181 DLV 1537-12 DLV 1537-12 DLV 1537-12 DLV 1537-12 Ab J95728 Ab J95727 Ab J95727 Ab J95728 Ab J95727 Ab J95728 Ab J95727 Ab J95728 Ab J95727 BUS MDL-1/8A BUS MDL-1/16A GI HV5025
Q502 Q503 Q504	MPS3640 MPS6515 MPS6518	MOT MOT MOT	MPS3640 MPS6515 MPS6518	וסול	RECEPTACLE, POWER	SWC EAC-301
Q505 Q506	2N5189 MP52540	RCA MOT	2N5189 MP53640	\$701 \$702	SWITCH, ROTARY SWITCH, ROTARY	КН В-2657/С КН В-2657/С
CR401 CR501 CR502 CR503 CR504	1N4149 IN4502 MZ2361 MZ2361 IN4002	TR MSC MOT MOT MSC	IN4149 IN4002 MZ2361 MZ2361 IN4002	5901 5902 5903 5904	SWITCH, SLIDE SWITCH, SLIDE SWITCH, SLIDE SWITCH, TOGGLE TRANSFORMER, POWER	CW G-126 CW GF-123 SWC 46256LFR CK UI1

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A.ML (A.J. (B.J.S. (C.D. (C.C. (C1.2.) 5010) 32.4 14.00 68:19) 72.7 72.9 7	Har Borley Cc. Instructions. Januar Argino. Cale 1 Dublier Schelt With Lic. Person Electronic Homorocom.	Milwoukee, Wisc. Mt, View, Colif. Dubois, Pa. St. Louis, Mo. Newark, N. J. Watertowe, Mass. Philadelphia, Pa. East Aurora, N. Y. Comptoo, Colif.	ELM ERT MOT MSC RCA SP STK TR TRW	(72136) (72982) (04713) (49671) (56289) (78488- (03877) (84411)	Electromotive Mfg. Erie Technological Matarola Semiconductor Radio Corp. of America Sprague Electric Co. Stackpole Carbon Co. Transition Electronics. Transition Electronics.	Willimantic, Conn Erie, Pa. Phaenix, Ariz. Culver City, Calif Harrison, N. J. North Adams, Mas St. Mary's, Pa. Wakefield, Mass. Ogallada, Nebs.



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