DC POWER SUPPLY STB SERIES, MODEL 6111A SERIAL NUMBER PREFIX 6E

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### SAFETY SUMMARY

The following general safety precautions must be observed during all phases of operation, service, and repair of this instrument. Failure to comply with these precautions or with specific warnings elsewhere in this manual violates safety standards of design, manufacture, and intended use of the instrument. Hewlett-Packard Company assumes no liability for the customer's failure to comply with these requirements.

### **BEFORE APPLYING POWER.**

Verify that the product is set to match the available line voltage and the correct fuse is installed.

### GROUND THE INSTRUMENT.

This product is a Safety Class 1 instrument (provided with a protective earth terminal). To minimize shock hazard, the instrument chassis and cabinet must be connected to an electrical ground. The instrument must be connected to the acpower supply mains through a three-conductor power cable, with the third wire firmly connected to an electrical ground (safety ground) at the power outlet. For instruments designed to be hard-wired to the ac power lines (supply mains), connect the protective earth terminal to a protective conductor before any other connection is made. Any interruption of the protective (grounding) conductor or disconnection of the protective earth terminal will cause a potential shock hazard that could result in personal injury. If the instrument is to be energized via an external autotransformer for voltage reduction, be certain that the autotransformer common terminal is connected to the neutral (earthed pole) of the ac power lines (supply mains).

### INPUT POWER MUST BE SWITCH CONNECTED.

For instruments without a built-in line switch, the input power lines must contain a switch or another adequate means for disconnecting the instrument from the ac power lines (supply mains).

### DO NOT OPERATE IN AN EXPLOSIVE ATMOSPHERE.

Do not operate the instrument in the presence of flammable gases or fumes.

### **KEEP AWAY FROM LIVE CIRCUITS.**

Operating personnel must not remove instrument covers, Component replacement and internal adjustments must be made by qualified service personnel. Do not replace components with power cable connected. Under certain conditions, dangerous voltages may exist even with the power cable removed. To avoid injuries, always disconnect power, discharge circuits and remove external voltage sources before touching components.

### DO NOT SERVICE OR ADJUST ALONE.

Do not attempt internal service or adjustment unless another person, capable of rendering first aid and resuscitation, is present.

### DO NOT EXCEED INPUT RATINGS.

This instrument may be equipped with a line filter to reduce electromagnetic interference and must be connected to a properly grounded receptacle to minimize electric shock hazard. Operation at line voltages or frequencies in excess of those stated on the data plate may cause leakage currents in excess of 5.0 mA peak.

### SAFETY SYMBOLS.



Instruction manual symbol: the product will be marked with this symbol when it is necessary for the user to refer to the instruction manual (refer to Table of Contents).



Indicates hazardous voltages.



Indicate earth (ground) terminal.



The WARNING sign denotes a hazard. It calls attention to a procedure, practice, or the like, which, if not correctly performed or adhered to, could result in personal injury. Do not proceed beyond a WARNING sign until the indicated conditions are fully understood and met.



The CAUTION sign denotes a hazard. It calls attention to an operating procedure, or the like, which, if not correctly performed or adhered to, could result in damage to or destruction of part or all of the product. Do not proceed beyond a CAUTION sign until the indicated conditions are fully understood and met.

### DO NOT SUBSTITUTE PARTS OR MODIFY INSTRUMENT.

Because of the danger of introducing additional hazards, do not install substitute parts or perform any unauthorized modification to the instrument. Return the instrument to a Hewlett-Packard Sales and Service Office for service and repair to ensure that safety features are maintained.

Instruments which appear damaged or defective should be made inoperative and secured against unintended operation until they can be repaired by qualified service personnel.



Figure 1-1. DC Power Supply, Model 6111A

### SECTION I GENERAL INFORMATION

### 1-1 DESCRIPTION

The STB Series of power supplies is designed 1-2 for applications requiring extreme stability, regulation, and insensitivity to ambient temperature variations. The supply is completely transistorized (allsilicon) and is suitable for either bench or relay rack operation. The accurate programming coefficient allows the supply to be used as a 0.1% calibrator, or as a voltage reference source. It is a Constant Voltage / Current Limiting supply that will furnish full rated output voltage at the maximum rated output current or can be continuously adjusted throughout the output range. The front panel CUR-RENT controls can be used to establish the output current limit (overload or short circuit) when the supply is used as a constant voltage source and the VOLTAGE controls can be used to establish the voltage limit (ceiling) when the supply is used as a constant current source.

1-3 The power supply has both front and rear terminals. Either the positive or negative output terminal may be grounded or the power supply can be operated floating at up to a maximum of 300 volts off ground.

1-4 A single meter is used to measure either output voltage or output current in one of two ranges. The voltage or current ranges are selected by a METER switch on the front panel.

1-5 The programming terminals located at the rear of the unit allow ease in adapting to the many operational capabilities of the power supply. A brief description of these capabilities is given below:

a. Remote Programming

The power supply may be programmed from a remote location by means of an external voltage source or resistance.

b. Remote Sensing

The degradation in regulation which would occur at the load because of the voltage drop in the load leads can be reduced by using the power supply in the remote sensing mode of operation.

c. Series and Auto-Series Operation

Power Supplies may be used in series when a higher output voltage is required in the voltage mode of operation or when greater voltage compliance is required in the constant current mode of operation. Auto-Series operation permits one knob control of the total output voltage from a "master" supply.

d. Parallel Operation

The power supply may be operated in parallel with a similar unit when greater output current capability is required.

e. Auto-Tracking

The power supply may be used as a "master" supply, having control over one (or more) "slave" supplies that furnish various voltages for a system.

### 1-6 <u>SPECIFICATIONS</u>

1-7 Detailed Specifications for the power supply are given in Table 1-1.

1-8 OPTIONS

1-9 Options are factory modifications of a standard instrument that are requested by the customer. A typical option is replacing the front panel voltage and current controls with ten-turn voltage and current decadial controls. The following options are available on the instrument covered by this manual. Where applicable, detailed coverage of options is included throughout the manual.

### Option No. Description

06

Overvoltage Protection "Crowbar": A completely separate circuit for protecting delicate loads against power supply failure or operator error. This independent device monitors the output voltage and within 10µsec impose a virtual short-circuit (crowbar) across the power supply output if the preset overvoltage margin is exceeded. When Option 06 is requested by the customer, Model 6916A is attached to the rear of the power supply at the factory.

Overvoltage Margin: 1 to 4 volts, screwdriver adjustable.

<u>Power Requirement:</u> 15ma continuous drain from power supply being protected. Size: Add 5 inches to power supply depth dimension.

Weight: Add 2 lbs. net.

### NOTE

Detailed coverage of Option 06 is included in an addendum entitled, Model 6916A Overvoltage Protector. The addendum is included at the rear of manuals that support power supplies that have been modified for Option 06.

28 Rewire for 230V Input: Supply as normally shipped is wired for 115VAC input. Option 28 consists of reconnecting the input transformer for 230VAC operation.

### 1-10 ACCESSORIES

1-11 The accessories listed in the following may be ordered with the power supply or separately from the local Hewlett-Packard field sales office (refer to list at rear of manual for addresses).

### Part No. Description

- C05 8" Black Handle that can be attached to side of supply.
- 14513A Rack Kit for mounting one  $3\frac{1}{2}$ "-high supply (Refer to Section II for details).
- 14515A Rack Kit for mounting one  $5\frac{1}{4}$ "-high supply (Refer to Section II for details).

Description

14523A	Rack Kit for mounting two $3\frac{1}{2}$ "-high
	supplies (Refer to Section II for details)

14525A Rack Kit for mounting two  $5\frac{1}{4}$ "-high supplies (Refer to Section II for details).

### 1-12 INSTRUMENT IDENTIFICATION

1-13 Hewlett-Packard power supplies are identified by a three-part serial number tag. The first part is the power supply model number. The second part is the serial number prefix, which consists of a number-letter combination that denotes the date of a significant design change. The number designates the year, and the letter A through I designates the month, January through December respectively. The third part is the power supply serial number.

1-14 If the serial number prefix on your power supply does not agree with the prefix on the title page of this manual, change sheets are included to update the manual. Where applicable, backdating information is given in an appendix at the rear of the manual.

### 1-15 ORDERING ADDITIONAL MANUALS

1-16 One manual is shipped with each power supply. Additional manuals may be purchased from your local Hewlett-Packard field office (see list at rear of this manual for addresses). Specify the model number, serial number prefix, and  $\hat{\psi}$  Stock Number provided on the title page. Table 1-1. Specifications

### INPUT:

105-125/210-250VAC, single phase, 48-63 Hz (cps), 0.5A, 52W.

### OUTPUT:

0-20 volts at 0-1 ampere.

### LOAD REGULATION:

Front terminals: Less than 0.001% plus  $200\mu v$ . Rear terminals: Less than 0.001% plus  $100\mu v$ . For an output current change from no load to full load.

### LINE REGULATION:

Less than 0.001% output change for any line voltage change within the input rating.

### RIPPLE AND NOISE:

At any line voltage and under any load condition within rating.

Less than  $100\mu\nu$  peak-to-peak. Less than  $40\mu\nu$  rms.

### TEMPERATURE COEFFICIENT:

After 30 minutes warm-up

Front panel control or remote programming: Less than 0.001% plus  $10\mu\nu$  per degree Centigrade.

### STABILITY:

Total drift after 30 minutes warm-up and with less than  $\pm 3^{\circ}C$  ambient temperature variation:

Front panel control or remote programming: Less than 0.01% plus  $100\mu\nu$  for 8 hours. Less than 0.012% plus  $120\mu\nu$  for one month.

### TEMPERATURE RANGES:

Operating: 0 to 50°C. Storage: -20 to +85°C.

### OUTPUT IMPEDANCE:

Less than 0.002 ohms from DC to 100 Hz. Less than 0.02 ohms from 100 Hz to 1 KHz. Less than 0.5 ohms from 1 KHz to 100 KHz. Less than 3 ohms from 100 KHz to 1 MHz.

### TRANSIENT RECOVERY TIME:

Less than 50 microseconds for output recovery to within 10 millivolts of the nominal output voltage following a full load current change. Less than 100 microseconds for output recovery to within load regulation specification.

### OVERLOAD PROTECTION:

A continuously variable current limit circuit protects the power supply for all overloads including a direct short placed across the output terminals.

### METER:

Front panel meter and switch select 0-2.5V/ o-25V and 0-120ma/0-1. 2A scales.

### OUTPUT CONTROLS:

An in-line 5-digit (thumbwheel) voltage programmer permits control of the output voltage with an accuracy of 0.1% plus 1mv of the output voltage. Resolution is  $100\mu\nu$ . A single turn front panel pot permits the current limit setting to be varied continuously from zero to a value slightly in excess of the full current rating.

### OUTPUT TERMINALS:

Three "five-way" output posts are provided on the front panel and an output barrier strip is located on the rear of the chassis. All power supply output terminals are isolated from the chassis and either the positive or negative terminal may be connected to the chassis through a separate ground terminal located on the output terminal strip.

### ERROR SENSING:

Error sensing is automatically accomplished at the front terminals if the load is attached to the front terminals or at the rear terminals if the load is attached to the rear terminals. Provision is also included on the rear terminal strip for remote error sensing.

### REMOTE PROGRAMMING:

Remote programming of the output voltage is made available at the rear terminals. The programming coefficient is 1000 ohms per volt with an accuracy of 0.1% plus 1 millivolt. The current limit may also be set remotely by means of a resistance, 1000 ohms corresponding approximately to full output current.

### COOLING:

Convection cooling is employed. The supply has no moving parts.

### SIZE:

5-1/4" H x 8-1/2" W x 12-5/8" D. Two units can be mounted side by side to take up the same space as a standard 5-1/4" x 19" relay rack mounting.

WEIGHT: 11 lbs. net, 15 lbs. shipping.

FINISH: Light gray front panel with dark gray case.

### POWER CORD:

A 3-wire, 5-foot power cord is provided with each unit.

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### 2-1 INITIAL INSPECTION

2-2 Before shipment, this instrument was inspected and found to be free of mechanical and electrical defects. As soon as the instrument is unpacked, inspect for any damage that may have occurred in transit. Save all packing materials until the inspection is completed. If damage is found, proceed as described in the Claim for Damage in Shipment section of the Warranty at the rear of this manual.

### 2-3 MECHANICAL CHECK

2-4 This check confirms that there are no broken knobs or connectors, that the cabinet and panel surfaces are free of dents and scratches, and that the meters are not scratched or cracked.

### 2-5 ELECTRICAL CHECK

2-6 The instrument should be checked against its electrical specifications. Section V includes an "in-cabinet" performance check to verify proper instrument operation.

### 2-7 INSTALLATION DATA

2-8 The instrument is shipped ready for bench operation. It is only necessary to connect the instrument to a source of power and it is ready for operation.

### 2-9 LOCATION

2-10 This instrument is air cooled. Sufficient space should be provided around the instrument to permit free flow of cooling air along the sides and to the rear. It should be used in an area where the ambient temperature does not exceed 50°C (122°F).

### 2-11 POWER REQUIREMENTS

2-12 This power supply may be operated from either a 115 or 230 volt, 48-63 cps power source. The unit, as shipped from the factory, is wired for 115V operation.

2-13 The input power required when operating at full load from a 115 volt, 60 cycle power source is 45 watts and 0.5 amperes.

### 2-14 230 VOLT OPERATION

2-15 Normally, the windings of the input transformer are connected in parallel for operation from a 115 volt source. To convert the power supply for operation from a 230 volt source, the power trans-former windings must be connected in series. The windings are connected in series as follows: (Refer to Figure 2-1)



Figure 2-1. Input Transformer Primary Connections

a. Unplug the line cord and remove the top and bottom covers from the case. (This is done by removing the four screws which hold each cover to the side frames.)

b. With a sharp knife or razor blade, cut the printed wiring between test points 45 and 46 and also between 47 and 48 on the printed circuit board. These are shown on the overall schematic and are labeled on the printed circuit board.

c. Connect a jumper wire between 46 and 47.

d. Replace the fuse with a  $\frac{1}{2}$  ampere 230 volt fuse. Replace covers and operate unit normally.

### 2-16 POWER CABLE

2-17 To protect operating personnel, the National Electrical Manufacturers Association (NEMA) recommends that the instrument panel and cabinet be grounded. This instrument is equipped with a three conductor power cable. The third conductor is the ground conductor and when the cable is plugged into an appropriate receptacle, the instrument is grounded. The offset pin on the power cable threeprong connector is the ground connection.

2-18 To preserve the protection feature when operating the instrument from a two-contact outlet, use a three-prong to two-prong adaptor and connect the green lead on the adaptor to ground.



Figure 2-2. Rack Mounting, Two Units

### 2-19 RACK MOUNTING

2-20 This instrument may be rack mounted in a standard 19 inch rack panel either alongside a similar unit or by itself. Figures 2-2 and 2-3 show how both types of installations are accomplished.

2-21 To mount two units side-by-side, proceed as follows:

a. Remove the four screws from the front panels of both units.

b. Slide rack mounting ears between the front panel and case of each unit.

c. Slide combining strip between the front panels and cases of the two units.

d. After fastening rear portions of units together using the bolt, nut, and spacer, replace panel screws.

2-22 To mount a single unit in the rack panel, proceed as follows:

a. Bolt rack mounting ears, combining straps, and angle brackets to each side of center spacing panels. Angle brackets are placed behind combining straps as shown in Figure 2-3.

b. Remove four screws from front panel of unit.

c. Slide combining strips between front

panel and case of unit.

d. Bolt angle brackets to front sides of case and replace front panel screws.

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Figure 2-3. Rack Mounting, One Unit

### 2-23 REPACKAGING FOR SHIPMENT

2-24 To insure safe shipment of the instrument, it is recommended that the package designed for the instrument be used. The original packaging material is reusable. If it is not available, contact your local Hewlett-Packard field office to obtain the materials. This office will also furnish the address of the nearest service office to which the instrument can be shipped. Be sure to attach a tag to the instrument which specifies the owner, model number, full serial number, and service required, or a brief description of the trouble.

### SECTION III OPERATING INSTRUCTIONS

### 3-1 OPERATING CONTROLS AND INDICATORS

3-2 The front panel controls and indicators, together with the normal turn-on sequence, are shown in Figure 3-1.



- 1. PUSH LINE SWITCH TO TURN ON SUPPLY AND OBSERVE THAT LIGHT GOES ON.
- 2. SET METER SWITCH TO DESIRED VOLTAGE RANGE.
- ADJUST VOLTAGE CONTROLS UNTIL DESIRED OUTPUT VOLTAGE IS INDICATED ON METER.
- A SHORT CIRCUIT OUTPUT TERMINALS AND SET METER SWITCH TO DESIRED CURRENT RANGE
- 5. ADJUST CURRENT CONTROL FOR DESIRED OUTPUT CURRENT.
- REMOVE SHORT AND CONNECT LOAD TO OUTPUT TERMINALS (FRONT OR REAR).
- 7. POWER IS REMOVED BY PUSHING THE LINE SWITCH.

Figure 3-1. Front Panel Controls and Indicators

### 3-3 OPERATING MODES

The power supply is designed so that its mode 3-4 of operation can be selected by making strapping connections between particular terminals on the terminal strip at the rear of the power supply. The terminal designations are stenciled in white on the power supply above their respective terminals. Althrough the strapping patterns illustrated in this section show the negative terminal grounded, the operator can ground either terminal or operate the power supply up to 300 vdc off ground (floating). The following paragraphs describe the procedures for utilizing the various operational capabilities of the power supply. A more theoretical description is contained in a power supply Application Manual and in various Tech. Letters published by the Harrison Division. Copies of these can be obtained from your local Hewlett-Packard field office.

### 3-5 NORMAL OPERATING MODE

3-6 The power supply is normally shipped with its rear terminal strapping connections arranged for Constant Voltage / Current Limiting, local sensing, local programming, single unit mode of operation. This strapping pattern is illustrated in Figure 3-2. The operator selects either a constant voltage or current limited output using the front panel controls (local programming, no strapping changes are necessary).



### Figure 3-2. Normal Strapping Pattern

### 3-7 CONSTANT VOLTAGE

3-8 To select a constant voltage output, proceed as follows:

a. Turn-on power supply and adjust VOLTAGE controls for desired output voltage (output terminals open).

b. Short output terminals and adjust CUR-RENT controls for maximum output current allowable (current limit), as determined by load conditions. If a load change causes the current limit to be exceeded, the power supply will automatically crossover to constant current output at the preset current limit and the output voltage will drop proportionately. In setting the current limit, allowance must be made for high peak current which can cause unwanted cross-over. (Refer to Paragraph 3-43.)

### 3-9 CURRENT LIMIT

3-10 To select a current limit output, proceed as follows:

a. Short output terminals and adjust CUR-RENT controls for desired output current.

b. Open output terminals and adjust VOLT-AGE controls for maximum output voltage allowable (voltage limit), as determined by load conditions. If a load change causes the voltage limit to be exceeded, the power supply will automatically crossover to constant voltage output at the preset voltage limit and the output current will drop proportionately. In setting the voltage limit, allowance must be made for high peak voltages which can cause unwanted crossover. (Refer to Paragraph 3-43.)

### 3-11 CONNECTING LOAD

3-12 Each load should be connected to the power supply output terminals using separate pairs of connecting wires. This will minimize mutual coupling effects between loads and will retain full advantage of the low output impedance of the power supply. Each pair of connecting wires should be as short as possible and twisted or shielded to reduce noise pickup. (If shield is used, connect one end to power supply ground terminal and leave the other end unconnected.)

3-13 If load considerations require that the output power distribution terminals be remotely located from the power supply, then the power supply output terminals should be connected to the remote distribution terminals via a pair of twisted or shielded wires and each load separately connected to the remote distribution terminals. For this case, remote sensing should be used (Paragraph 3-27).

### 3-14 OPERATION OF SUPPLY BEYOND RATED OUTPUT

3-15 The shaded area on the front panel meter face indicates the amount of output voltage or current that is available in excess of the normal rated output. Although the supply can be operated in this shaded region without being damaged, it cannot be guaranteed to meet all of its performance specifications. However, if the line voltage is maintained above 115 Vac, the supply will probably operate within its specifications.

### 3-16 OPTIONAL OPERATING MODES

### 3-17 REMOTE PROGRAMMING, CONSTANT VOLTAGE

3-18 The constant voltage output of the power supply can be programmed (controlled) from a remote location if required. Either a resistance or voltage source can be used for the programming device. The wires connecting the programming terminals of the supply to the remote programming device should be twisted or shielded to reduce noise pick-up. The VOLTAGE controls on the front panel are disabled according to the following procedures.

3-19 <u>Resistance Programming (Figure 3-3)</u>. In this mode, the output voltage will vary at a rate determined by the programming coefficient--1000 ohms per volt (i.e. the output voltage will increase 1 volt for each 1000 ohms added in series with programming terminals). The programming coefficient is determined by the programming current. This current is adjusted to within 0.1% of 1ma at the factory. If greater programming accuracy is required, it may be achieved by changing resistor R16.



Figure 3-3. Remote Resistance Programming (Constant Voltage)

3-20 The output voltage of the power supply should be zero volts  $\pm 1$  millivolt when zero ohms is connected across the programming terminals. If a zero ohm voltage closer than this is required, it may be achieved by changing resistor R14 as described in Paragraph 5-48.

3-21 To maintain the stability and temperature coefficient of the power supply, use programming resistors that have stable, low noise, and low temperature characteristics (less than 5 ppm per degree Centigrade). A switch can be used in conjunction with various resistance values in order to obtain discrete output voltages. The switch should have make-before-break contacts to avoid momentarily opening the programming terminals during the switching interval.

3-22 <u>Voltage Programming (Figure 3-4)</u>. Employ the strapping pattern shown on Figure 3-4 for voltage programming. In this mode, the output voltage will vary in a 1 to 1 ratio with the programming voltage (reference voltage) and the load on the programming voltage source will not exceed 0.5 microampere.



Figure 3-4. Remote Voltage Programming (Constant Voltage)

3-23 The impedance ( $R_x$ ) looking into the external programming voltage source should be approximately 6000 ohms if the temperature and stability specifications of the power supply are to be maintained.

### 3-24 REMOTE RESISTANCE PROGRAMMING, CUR-RENT LIMIT (See Figure 3-5)

3-25 The output current will vary roughly in proportion to the programming resistor. Full current output is obtained with approximately 1000 ohms; however, the exact current setting should be checked by shorting the output terminals and reading the current with the programming resistor in place.



### Figure 3-5. Remote Resistance Programming (Current Limit)

3-26 Use stable, low noise, low temperature coefficient (less than 5 ppm/OC) programming resistors to maintain the power supply temperature coefficient and stability specifications. A switch may be used to set discrete values of output current. A makebefore-break type of switch should be used since the output current will exceed the maximum rating of the power supply if the switch contacts open during the switching interval.

### CAUTION

If the programming terminals (Al and A9) should open at any time during this mode, the output current will rise to a value that may damage the power supply and/or the load. To avoid this possibility, connect a  $1K_{\Lambda}$  resistor across the programming terminals and in parallel with a remote programming resistor. Like the programming resistor, the  $1K_{\Lambda}$  resistor should be of the low noise, low temperature coefficient type.

### 3-27 REMOTE SENSING (See Figure 3-6)

3-28 Remote sensing is used to maintain good regulation at the load and reduce the degradation of regulation which would occur due to the voltage drop in the leads between the power supply and the load. Remote sensing is accomplished by utilizing the strapping pattern shown in Figure 3-6. The power supply should be turned off before changing strapping patterns. The leads from the +S terminals to the load will carry approximately 1 milliampere of current, and it is not required that these leads be as heavy as the load leads. However, they must be twisted or shielded to minimize noise pick-up.



### Figure 3-6. Remote Sensing

### CAUTION

Observe polarity when connecting the sensing leads to the load.

3-29 Note that it is desirable to minimize the drop in the load leads and it is recommended that the drop not exceed 1 volt per lead if the power supply is to meet its DC specifications. If a larger drop must be tolerated, please consult a Hewlett-Packard field representative.

3-30 The procedure just described will result in a low DC output impedance at the load. If a low AC impedance is required, it is recommended that the following precautions be taken:

a. Disconnect output capacitor C3, by disconnecting the strap between A7 and (+). b. Connect a capacitor having similar characteristics (approximately same capacitance, same voltage rating orgreater, and having good high frequency characteristics) across the load using short leads.

3-31 Although the strapping patterns shown in Figures 3-3 through 3-5 employ local sensing, note that it is possible to operate a power supply simultaneously in the remote sensing and Constant Voltage/Current Limit remote programming modes.

### NOTE

It is necessary to readjust the current limit when the instrument is operated in the remote sensing mode.

### 3-32 SERIES OPERATION

3-33 <u>Normal Series Connections (Figure 3-7)</u>. Two or more power supplies can be operated in series to obtain a higher voltage than that available from a single supply. When this connection is used, the output voltage is the sum of the voltages of the individual supplies. Each of the individual supplies must be adjusted in order to obtain the total output voltage. The power supply contains a protective diode connected internally across the output which protects the supply if one power supply is turned off while its series partner(s) is on.



Figure 3-7. Top: Normal Series; Bottom: Auto-Series, Two Units

3-34 Auto-Series Connections (Figure 3-8). The Auto-Series comfiguration is used when it is desir able to have the output voltage of each of the series connected supplies vary in accordance with the setting of a control unit. The control unit is called the master: the controlled units are called slaves. At maximum output voltage, the voltage of the slaves is determined by the setting of the front panel VOLTAGE control on the master. The master supply must be the most positive supply of the series. The output CURRENT controls of all series units are operative and the current limit is equal to the lowest control setting. If any output CURRENT controls are set too low, automatic crossover to constant current operation will occur and the output voltage will drop. Remote sensing and programming can be used; however, the strapping arrangements shown in the applicable figures show local sensing and programming.



Figure 3-8. Auto-Series, Three Units

3-35 In order to maintain the temperature coefficient and stability specifications of the power supply, the external resistors ( $R_X$ ) shown in Figure 3-8 should be stable, low noise, low temperature coefficient (less than 5 ppm per degree Centigrade) resistors. The value of each resistor is dependant on the desired output voltage ratings of the master and slave supplies. The value of  $R_X$  is this voltage divided by the voltage programming current of the supply, 1ma ( $1/K_p$  where  $K_p$  is the voltage programming coefficient).

### 3-36 PARALLEL OPERATION (Figure 3-9).

3-37 Two or more power supplies can be connected in parallel to obtain a total output current greater than that available from one power supply. The total output current is the sum of the output currents of the individual power supplies. The output CUR-RENT controls of each power supply can be separately set. The output voltage controls of one power supply should be set to the desired output voltage; the other power supply should be set for a slightly larger output voltage. The supply set to the lower output voltage will act as a constant voltage source; the supply set to the higher output will act as a constant current source, dropping its output voltage until it equals that of the other supply.



Figure 3-9. Normal Parallel

### 3-38 AUTO TRACKING OPERATION (See Figure 3-10.)

3-39 This connection is used when it is necessary to provide several voltages, all referred to a common bus, which vary in proportion to the setting of one master instrument. The following constraints must be observed when using this connection.

a. The master unit must be a positive voltage source. When several positive sources are used, the master must be the largest voltage unit.

b. The external resistors should be stable, low noise, low temperature coefficient resistors if the instruments are to maintain their temperature coefficient and stability specifications.

3-40 The resistor values are determined as follows: Referring to Figure 3-10 for two units.

 $\frac{R_{A}}{R_{B}} = \frac{V \text{ Master } - V \text{ Slave}}{V \text{ Slave}}$ 

Choosing 10 milliamperes as a reasonable maximum current in the resistors  $R_A = 100$  (V master - V slave) and  $R_B = 100$  (V slave).

3-41 For several units connected in auto tracking refer to Figure 3-10. RA and RB are determined as before.  $R_{\rm C}$  = 100 (V master - V slave<sub>2</sub>),  $R_{\rm D}$  = 100 (V slave<sub>2</sub>), etc.





### 3-42 SPECIAL OPERATING CONSIDERATIONS

### 3-43 PULSE LOADING

3-44 The power supply will automatically crossover from constant voltage to constant current operation, or the reverse, in response to an increase (over the preset limit) in the output current or voltage, respectively. Although the preset limit may be set higher than the average output current or voltage, high peak currents or voltages (as occur in pulse loading) may exceed the preset limit and cause crossover to occur. If this crossover limiting is not desired, set the preset limit for the peak requirement and not the average.

### 3-45 OUTPUT CAPACITANCE

3-46 There is a capacitor (internal) across the output terminals of the power supply. This capacitor helps to supply high-current pulses of short duration during constant voltage operation. Any capacitance added externally will improve the pulse current capability, but will decrease the safety provided by the constant current circuit. A high-current pulse may damage load components before the average output current is large enough to cause the constant current circuit to operate.

3-47 The effects of the output capacitor during constant <u>current</u> operation are as follows:

a. The output impedance of the power supply decreases with increasing frequency.

b. The recovery time of the output voltage is longer for load resistance changes.

c. A large surge current causing a high power dissipation in the load occurs when the load resistance is reduced rapidly.

### 3-48 REVERSE VOLTAGE LOADING

3-49 A diode is connected across the output terminals. Under normal operating conditions, the diode is reverse biased (anode connected to negative terminal). If a reverse voltage is applied to the output terminals (positive voltage applied to negative terminal), the diode will conduct, shunting current across the output terminals and limiting the voltage to the forward voltage drop of the diode. This diode protects the series transistors and the output electrolytic capacitors.

### 3-50 REVERSE CURRENT LOADING

3-51 Active loads connected to the power supply may actually deliver a reverse current to the power supply during a portion of it's operating cycle. An external source cannot be allowed to pump current into the supply without loss of regulation and possible damage to the output capacitor. To avoid these effects, it is necessary to preload the supply with a dummy load resistor so that the power supply delivers current through the entire operating cycle of the load device.

### 3-52 MULTIPLE LOADS

3-53 It is imperative that each load taken from the power supply have two separate leads brought back to the power supply output terminals if full advantage is to be taken of the low output impedance of the power supply and if mutual coupling effects between loads are to be avoided.

### SECTION IV PRINCIPLES OF OPERATION



Figure 4-1. Overall Block Diagram

### 4-1 OVERALL BLOCK DIAGRAM DISCUSSION

4-2 The power supply, figure 4-1, consists of a power transformer, rectifier and filter, series regulator, error amplifier and driver, constant voltage input circuit, current limiting circuit, reference regulator circuit, bias supply, meter circuit, and an oven control circuit.

The ac input line voltage is reduced to the 4 - 3proper level and coupled to the rectifier and filter. The rectifier-filter converts the ac input to raw dc which is fed to the positive terminal via the regulator and current sampling resistor network. The regulator, part of the feedback loop, is made to alter it's conduction to maintain a constant output voltage or limit the output current. The voltage developed across the current sampling resistor network is the input to the current limiting circuit. If the output current that passes through the sampling network exceeds a certain predetermined level, the current limiting circuit applies a feedback signal to the series regulator which alters the regulator's conduction so that the output current does not exceed the predetermined current limit.

4 - 4The constant voltage input circuit obtains it's input by sampling the output voltage of the supply. Any changes in output voltage are detected in the constant voltage input circuit, amplified by the error amplifier and driver, and applied to the series regulator in the correct phase and amplitude to counteract the change in output voltage. The reference regulator circuit provides stable reference voltages which are used by the constant voltage input circuit and the current limiting circuit for comparison purposes. The bias supply furnishes voltages which are used throughout the instrument for biasing purposes. The meter circuit provides indications of output voltage or current in either operating mode.

4-5 An oven houses the temperature sensitive components in the supply to provide a low temperature coefficient which results in excellent stability. The oven control circuit maintains the oven temperature at 65°C.



Figure 4-2. Simplified Schematic

### 4-6 SIMPLIFIED SCHEMATIC

4-7 A simplified schematic of the power supply is shown in Figure 4-2. It illustrates the operating controls; the ON-off switch, and the voltage programming controls (R11 and R20). Figure 4-2 also shows the internal sources of bias and reference voltages and their nominal magnitudes with an input of 115 Vac. 4-8 Diode CR32, connected across the output terminals of the power supply, is a protective device which prevents internal damage that might occur if a reverse voltage were applied across the output terminals. Output capacitor, C23, is also connected across the output terminals when the normal strapping pattern shown on Figure 4-2 is employed. Note that this capacitor can be removed if an increase in the programming speed is desired. 4-9

DETAILED CIRCUIT ANALYSIS (Refer to Overall Schematic at Rear of Manual.)

### 4-10 SERIES REGULATOR

4-11 The series regulator consists of transistor stage Q11. The regulator serves as a series control element by altering it's conduction so that the output voltage and the current limit is never exceeded. The conduction of Q11 is controlled by the feedback voltage obtained from driver Q10.

### 4-12 CONSTANT VOLTAGE INPUT CIRCUIT

4-13 This circuit consists of the programming resistors, coarse voltage adjustment R20, fine voltage adjustment R11, and differential amplifiers Q1, Q2-Q3, and Q7-Q8. Q1 consists of two transistors having closely matched characteristics in a single transistor package. This package insures that both transistors will operate at essentially the same temperature, minimizing drift due to thermal differentials. Q1, Q2, and Q3 are enclosed in a constant-temperature oven to further minimize the effects of changing ambient temperature.

4-14 The constant voltage input circuit continuously compares a fixed reference voltage with a portion of the output voltage and, if a difference exists, produces an error voltage whose amplitude and phase is proportional to the difference. The error output is fed back to the series regulator, through the error and driver amplifiers. The error voltage changes the conduction of the series regulator which, in turn, alters the output voltage so that the difference between the two input voltages applied to the differential amplifier is reduced to zero. The above action maintains the output voltage constant.

4-15 The base of QIA is connected to the junction of the programming resistors and the current pullout resistor (R18 or R19) through a current limiting resistor, R1. Note that when internal programming is used, R19 is the current pullout resistor, having similar temperature characteristics as the front panel voltage control. In remote programming, R18 is the current pullout, having as low a temperature coefficient as possible. Diodes CR1 and CR2 limit voltage excursions on the base of QIA. RI limits the current through the programming resistors under the condition of rapid voltage turndown. Capacitor C4 shunts the programming resistor to increase the high frequency gain of the amplifier. The programming current is determined primarily by the reference voltage and the pullout resistor, R18 or R19. R17 in series with the pullout resistor serves as a mimming adjustment of the programming current. A variable current injected at the junction of the

programming and pullout resistors through R15 allows fine trimming of the programming current.

4-16 The base of Q1B is connected to ground through R2. Variable currents can be injected at this point through R13 which serves to compensate for fixed voltage offsets in Q1, and through R11 which is the fine voltage adjustment.

4-17 Negative feedback is coupled from the output of differential amplifier Q7-Q8 to the input of Q1 by network R30 and C6. This feedback provides high frequency roll off in the loop gain to stabilize the feedback loop.

### 4-18 DRIVER AND ERROR AMPLIFIER

4-19 The driver and error emplifier circuit raises the level of the error signal from the constant voltage input circuit a sufficient amount to drive the series regulator. Common emitter amplifier Q10 also receives a current limiting input when CR8 becomes forward biased.

### 4-20 CURRENT LIMIT CIRCUIT

4-21 The output current flows through R23 producing a voltage drop of one volt for 500 ma output current. Current limit control, R25 is attached to R23 and goes positive as the output current increases. When this positive voltage is great enough to overcome the negative voltage resulting from the current limit control setting, Q5 is turned on. This action causes test point 21 to fall to about zero volts, forward biasing CR8 and carrying the base of Q10 sufficiently negative to turn it off, thus turning off the series regulator. R27 and CR4 provide a -0.7V bias for the emmitter of Q5.

### 4-22 OVEN CONTROL CIRCUIT

4-23 The oven temperature is sensed by thermistor R57. If the temperature is too low, the resistance of R57 will be high enough to bias the emitter of unijunction transistor Q16 sufficiently positive for it to act as a free-running pulse generator. These pulses are coupled through C23 and R62 to the gate of the Silicon-Controlled Rectifier CR31. The first pulse in any half-cycle of line voltage will cause CR31 to conduct and remain conducting to the end of that half-cycle. When CR31 is conducting, current flows through the oven heater winding raising the temperature. When the temperature is high enough, R57 will have decreased sufficiently to lower the emitter bias of Q16, stopping its output pulses and leaving CR31 off.

### 4-24 REFERENCE CIRCUIT

4-25 The reference circuit is a feedback power supply similar to the main supply. It provides stable reference voltages which are used throughout the unit. The reference voltages are all derived from raw dc obtained from the full wave rectifier (CR24 and CR25) and filter capacitor C16. The  $\pm 6.2$  and -9.4 voltages, which are used in the constant voltage input circuit for comparison purposes, are developed across temperature compensated Zener diodes VR1 and VR2. Resistor R49 limits the current through the Zener diodes to establish an optimum bias level.

4-26 The reference circuit is a closed loop feedback regulator which acts to maintain the voltage at point 16 at 12.4 volts regardless of line voltage variation. Any difference between the zener reference diode VR1 and one-half of the 12.4 volt bus as sampled by R47 and R48 is amplified by Q14 and and Q15 connected as a differential amplifier. The error is further amplified by Q13 and is applied to the base of series regulator Q12 which controls the output voltage of the reference circuit.

4-27 Zener diode VR2 is added in series with the reference outputs to provide a -9.4 volt bias output. The main reference voltage is the -6.2 volt zener VR1. The 12.4 volt output is used as a stable bias source. Diode CR19 provides initial start-up bias for the reference circuit when the power supply is first turned on.

### 4-28 METER CIRCUIT

4-29 The meter circuit provides continuous indications of output voltage or current on a single multiple range meter. The meter can be used either as a voltmeter or an ammeter depending upon the position of METER switch S2 on the front panel of the supply. This switch also selects one of two meter ranges on each scale. The meter circuit consists of METER switch S2, various multiplying resistors and the meter movement.

4-30 With METER switch S2 set to either voltage position 1 or 2 (Figure 4-3A), the meter is connected in series with R21, R69, R66, R22, and R42 across the output of the supply. Resistor R66 calibrates the meter for full scale deflection to compensate for slight resistance variations inherent in different meter movements. Thermistor R22 compensates for the change in meter resistance as a function of temperature, and R42 lipearizes the resistance slope of R22 to match the meter resistance slope.

4-31 Voltage Adjust potentiometer R67 shunts a small amount of meter current and is adjusted for proper full scale meter deflection in the voltage

S2 SWITCH POSITIONS

MODEL	6101A	6102A	6106A	6111A	6112A	6113A	6116A
1	2.5V	5V	12V	2.5V	sv	2.5V	12V
2	25 <b>V</b>	50V	120V	25V	50V	2 5 V	120V
3	1.2A	.6A	•2.5A	1.2A	, 6A	2.5A	.25A
4	.12A	.06A	.025A	.12A	.06A	. 2 5A	.025A



A. VOLTAGE MONITORING



B. CURRENT MONITORING

Figure 4-3. Meter Circuit, Simplified Schematic

ranges. METER switch S2C shunts R69 in position 1 (the low voltage range). Thus, in the low voltage range the meter receives 10 times the amount of current that it receives in the high voltage range, for the same power supply output.

4-32 With METER switch S2 set to either current position 3 or 4 (Figure 4-3B), the meter is connected across the current sampling resistor R23. Current calibrate potentiometer R65 is adjusted for proper full scale meter deflection in the current ranges. METER switch S2A shunts R64 in position 4 (the low current range).

4-33 The meter is manufactured with a foolproof movement, that is, it can withstand a current overload of more than 10 times the maximum rated without injury.

### SECTION V MAINTENANCE

### 5-1 INTRODUCTION

Upon receipt of the power supply, the per-5 - 2formance check (Paragraph 5-10) should be made. This check is suitable for incoming inspection. If a fault is detected in the power supply while making the performance check or during normal operation, proceed to the troubleshooting procedures (Paragraph 5-27). After troubleshooting and repair (Paragraph 5-37), perform any necessary adjustments and calibrations (Paragraph 5-39). Before returning the power supply to normal operation, repeat the performance check to ensure that the fault has been properly corrected and that no other faults exist. Before doing any maintenance checks, turn-on power supply, allow a half-hour warm-up, and read the general information regarding measurement techniques (Paragraph 5-3).

### 5-3 GENERAL MEASUREMENT TECHNIQUES

5-4 The measuring device must be connected across the sensing leads of the supply or as close to the output terminals as possible when measuring the output impedance, transient response, regulation, or ripple of the power supply in order to achieve valid measurements. A measurement made across the load includes the impedance of the leads to the load and such lead lengths can easily have an impedance several orders of magnitude greater than the supply impedance, thus invalidating the measurement.



Figure 5-1. Front Panel Terminal Connections

5-5 The monitoring device should be connected to the rear +S and -S terminals (see Figure 3-2) or as shown in Figure 5-1. The performance characteristics should never be measured on the front terminals if the load is connected across the rear terminals. Note that when measurements are made at the front terminals, the monitoring leads are connected at A, not B, as shown in Figure 5-1. Failure to connect the measuring device at A will result in a measurement that includes the resistance of the leads between the output terminals and the point of connection.

5-6 For output current measurements, the current sampling resistor should be a four-terminal resistor. The four terminals are connected as shown in Figure 5-2. In addition, the resitor should be of the low noise, low temperature coefficient (less than 30 ppm/ $^{\rm O}$ C) type and should be used at no more than 5% of its rated power so that its temperature rise will be minimized.



Figure 5-2. Output Current Measurement Technique

5-7 When using an oscilloscope, ground one terminal of the power supply and then ground the case of the oscilloscope to this same point. Make certain that the case is not also grounded by some other means (power line). Connect both oscilloscope input leads to the power supply ground terminal and check that the oscilloscope is not exhibiting a ripple or transient due to ground loops, pick-up, or other means.

### 5-8 TEST EQUIPMENT REQUIRED

5-9 Table 5-1 lists the test equipment required to perform the various procedures described in this Section.

5-1

Table 5-1. Test Equipment Required		Table	5-1.	Test	Equipment	Required
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ndersonningenommen einversteren och som eine som	Table 5-1. 1est i	Equipment Required	y
Туре	Required Characteristics	Use	Recommended Model
Differential Sensitivity: 1 mv full scale Voltmeter (min.). Input impedance: 10 megohms (min.).		Measure DC voltages; calibration procedures	🖗 3420 (See Note)
Variable Range: 90-130 volts. Var Voltage Equipped with voltmeter Transformer accurate within 1 volt.		Vary AC input	
AC Voltmeter	Accuracy: 2%. Sensitivity: 1 mv full scale deflection (min.).	Measure AC voltages and ripple	⊕ 403 B
Oscilloscope	Sensitivity: 100μv/cm. Differential input.	Display transient response waveforms	40 A plus 1400A plug in.
Oscillator	Range: 5 cps to 600 Kc. Accuracy: 2%	Impedance checks	章 200 CD
DC Voltmeter	Accuracy: 1%. Input resistance: 20,000 ohms/volt (min.).	Measure DC voltages	@ 412 A
Repetitive Load Switch	Rate: 60 — 400 Hz, 2µsec rise and fall time.	Measure transient response	See Figure 5-7
Resistive Loads	Values: See Paragraph 5–14 and Figure 5–4. ±5%, 75 watts.	Power supply load resistors	
Current Sampling Resistor	Value: See Figure 5-4. 1%, 40 watts, 20ppm, 4-Terminal.	Measure current; calibrate meter	
Resistor	1Ka ±1%, 2 watt non-inductive	Measure impedance	und divid their blan and with the black black over state did able year over
Resistor	100 ohms, ±5%, 10 watt.	Measure impedance	
Resistor	Value: See Paragraph 5-49. ±0,1%, 1⁄2 watt.	Calibrate programming current	
Capacitor	500µf, 50wvdc	Measure impedance.	
Decade Resistance Box	Range: 0-500K. Accuracy: 0.1% plus 1 ohm Make-before-break contacts.	Measure programming coefficients.	

### 5-10 PERFORMANCE TEST

5-11 The following test can be used as an incoming inspection check and appropriate portions of the test can be repeated either to check the operation of the instrument after repairs or for periodic maintenance tests. The tests are performed using a 115-VAC 60 cps., single phase input power source. If the correct result is not obtained for a particular check, do not adjust any controls; proceed to trouble shooting (Paragraph 5-27).

### NOTE

A satisfactory substitute for a differential voltmeter is to arrange a reference voltage source and null detector as shown in Figure 5-3. The reference voltage source is adjusted so that the voltage difference between the supply being measured and the reference voltage will have the required resolution for the measurement being made. The voltage difference will be a function of the null detector that is used. Examples of satisfactory null detectors are:  $\oint$  419 A null detector, a DC coupled oscilloscope utilizing differential input, or a 50 mv meter movement with a 100 division scale. For the latter, a 2 mv change in voltage will result in a meter deflection of four divisions.





### CAUTION

Care must be exercised when using an electronic null detector in which one input terminal is grounded to avoid ground loops and circulating currents.

### 5-12 RATED OUTPUT AND METER ACCURACY

5-13 Voltage, Proceed as follows:

a. Connect load resistor across rear output terminals of supply for full load output. Resistor value to be as follows: <u>Model No.</u> 6101A 6102A 6106A 6111A 6112A Resistance  $20_{\Omega}$   $80_{\Omega}$   $500_{\Omega}$   $20_{\Omega}$   $80_{\Omega}$ <u>Model No.</u> 6113A 6116A Resistance  $5_{\Omega}$   $500_{\Omega}$ 

b. Connect differential voltmeter across +S and -S terminals of supply observing correct polarity.

c. Set METER switch to highest voltage range and turn on supply.

d. Adjust VOLTAGE controls until front panel meter indicates exactly the maximum rated output voltage.

e. Differential voltmeter should indicate maximum rated output voltage within  $\pm 2\%$ .

5-14 Current. Proceed as follows:

a. Connect test setup shown in Figure 5-4.

b. Turn CURRENT controls fully clockwise.

c. Set METER switch to highest current range and turn on supply.

d. Adjust VOLTAGE controls until front panel meter indicates exactly the maximum rated output current.

e. Differential voltmeter should read 1.0  $\pm$  0.02 Vdc.



Figure 5-4. Output Current, Test Setup

5-15 LOAD REGULATION (Front Terminals)

5-16 To check constant voltage load regulation, proceed as follows:

a. Connect test setup as shown in Figure 5-5.

b. Turn CURRENT controls fully clockwise.

c. Set METER switch to highest current range and turn on supply.

d. Adjust VOLTAGE controls until front panel meter indicates exactly the maximum rated output voltage.

e. Read and record voltage indicated on differential voltmeter.

f. Disconnect load resistors.

g. Reading on differential voltmeter should not vary from reading recorded in step e by more than the following:

Model No.	6101A	6102A	6106A	6111A
Variation (mvdc)	0.8	0.75	1.2	0.8
Model No.	6112A	6113A	6116A	
Variation (mvdc)	0.75	1.2	1.2	

5-17 LINE REGULATION (Front Terminals)

5-18 To check the line regulation, proceed as follows:

a. Connect variable auto transformer between input power source and power supply power input.

b. Turn CURRENT controls fully clockwise.

c. Connect test setup shown in Figure 5-5.



Figure 5-5. Load Regulation, Test Setup

d. Adjust variable auto transformer for 105 VAC input.

e. Set METER switch to highest voltage range and turn on supply.

f. Adjust VOLTAGE controls until front panel meter indicates exactly the maximum rated output voltage.

g. Read and record voltage indicated on differential voltmeter.

h. Adjust variable auto transformer for 125 VAC input.

i. Reading on differential voltmeter should not vary from reading recorded in step g by more than the following:

Model No.	6101A	6102A	6106A	6111A
Variation (mvdc)	0.2	0.4	1	0.2
Model No.	6112A	6113A	6116A	
Variation (mvdc)	0.4	0.1	1	

### 5-19 RIPPLE AND NOISE

5-20 To check theripple and noise, proceed as follows:

a. Retain test setup used for previous line regulation test except connect oscilloscope across output terminals as shown in Figure 5-6.

b. Adjust variable auto transformer for 125 VAC input.

c. Set METER switch to highest current range.

d. Turn CURRENT controls fully clockwise and adjust VOLTAGE controls until front panel meter indicates exactly the maximum rated output voltage.

e. Oscilloscope should indicate  $100\mu V$  peak-to-peak or less.



Figure 5-6. Ripple and Noise, Test Setup

5-4

### 5-21 TRANSIENT RECOVERY TIME

5-22 TQ check the transient recovery time proceed as follows:

a. Connect test setup shown in Figure 5-7.

b. Turn CURRENT controls fully clockwise.

c. Set METER switch to highest current range and turn on supply.

d. Adjust VOLTAGE controls until front panel meter indicates exactly the maximum rated output voltage.

e. Close line switch on repetitive load switch setup.

f. Adjust 25K potentiometer until a stable display is obtained on oscilloscope. Waveform should be within the tolerances shown in Figure 5-8 (output should return to within 10 mv of original value in less than 50 microseconds).



	RESISTANCE (OHMS)			
MODEL NO.	RX	Ry		
6101A	1	19		
6102A	2	76		
6106A	5	495		
6111A	1	19		
6112A	2	78		
6113A	5	4.5		
6116A	5	495		



### NOTE

If the unloading waveform is unobtainable, use a smaller value capacitor in the contact protection network illustrated in Figure 5-7.





### 5-23 OUTPUT IMPEDANCE

5-24 To check the output impedance, proceed as follows:

a. Connect test setup as shown in Figure 5-9.



Figure 5-9. Output Impedance, Test Setup

b. Set METER switch to highest voltage range, turn CURRENT controls fully clockwise, and turn on supply.

c. Adjust VOLTAGE controls until front panel meter reads 20 volts (10 volts for Model 6113A supplies).

d. Set AMPLITUDE control on Oscillator to 10 volts ( $E_{in}$ ), and FREQUENCY control to 10 cps.

e. Record voltage across output terminals of the power supply (E\_0) as indicated on AC voltmeter.

f. Calculate the output impedance by the following formula:

$$Z_{out} = \frac{E_0 R}{E_{in} - E_0}$$

E<sub>0</sub> = rms voltage across power supply output terminals.

R = 1000  $E_{t=} = 10 \text{ volts}$ 

5-5

g. The output impedance ( $Z_{\text{Out}}$ ) should be less than 0.002 ohm.

h. Using formula of step f, calculate output impedance at frequencies of 100cps, 1Kc, and 500Kc. Values should be less than 0.02 ohm, 0.5 ohm, and 3 ohms, respectively.

### 5-25 CURRENT LIMIT

5-26 To check the current limit circuit, proceed as follows:

a. Set the METER switch to the highest voltage range.

b. Turn the VOLTAGE controls fully clock-wise.

c. Turn the CURRENT control fully counterclockwise.

d. The voltage should reduce to zero.

e. Connect a short circuit across the output terminals.

f. Set the METER switch to the highest current range.

g. Turn the CURRENT control fully clockwise.

 ${\rm h}$  . The current should increase to, but not exceed the following:

Model	6101A	6102A	6106A	6111A
Current Limit (A)	1.05	0.52	0.21	1.05
Model	6112A	6113A	6116A	
Current Limit (A)	0.52	2.1	0.21	

### 5-27 TROUBLESHOOTING

5-28 Components within Hewlett-Packard power supplies are conservatively operated to provide maximum reliability. In spite of this, parts within a supply may fail. Usually the instrument must be immediately repaired with a minimum of "down time" and a systematic approach as outlined in succeeding paragraphs can greatly simplify and speed up the repair.

5-29 TROUBLE ANALYSIS

5-30 <u>General</u>. Before attempting to trouble shoot this instrument, ensure that the fault is with the instrument and not with an associated circuit.

The performance test (Paragraph 5-10) enables this to be determined without having to remove the instrument from the cabinet.

5-31 Once it is determined that the power supply is at fault, check for obvious troubles such as open fuse, a defective power cable, or an input power failure. Next, remove the top and bottom covers (each held by four retaining screws) and inspect for open connections, charred components, etc. If the trouble source cannot be detected by visual inspection, follow the detailed procedure outlined in succeeding paragraphs. Once the defective component has been located (by means of visual inspection or trouble analysis) correct it and re-conduct the performance test. If a component is replaced, refer to the repair and replacement, and adjustment and calibration paragraphs in this section.

5-32 A good understanding of the principles of operation is a helpful aid in trouble shooting, and it is recommended that the reader review Section IV of the manual before attempting to trouble shoot the unit in detail. Once the principles of operation are understood, logical application of this knowledge used in conjunction with the normal voltage readings shown on the schematic and the additional procedures given in the following paragraphs should suffice to isolate a fault to a component or small group of components. The normal voltages shown on the schematic are positioned adjacent to the applicable test points (identified by encircled numbers on the schematic and printed wiring boards). Additional test procedures that will aid in isolating troubles are as follows:

a. Reference circuit check (Paragraph 5-34). This circuit provides ciritcal operating voltages for the supply and faults in the circuit could affect the overall operation in many ways.

b. Feedback loop checks (Paragraph 5-35).

c. Procedures for isolating common troubles (Paragraph 5-36).

5-33 The test points referred to throughout the following procedures are identified on the schematic diagram by encircled numbers.

Table :	5-2.	Reference	Circuit	Troubleshooting
---------	------	-----------	---------	-----------------

Step	Meter Common	Meter Positive	Normal Indication	If Indication Abnormal, Take This Action	
1	+ S	30	6,2 ± 0,3vdc	Check 12.4 volt bias or VR1	
2	34	+S	9.4 $\pm$ 0.4vdc	Check 12.4 volt bias or VR2	
3	+S	16	12.4 ± 1.0vdc	Check Q12-Q15, CR24, CR25, C16, T1	

### 5-34 Reference Circuit.

a. Make an ohmmeter check to be certain that neither the positive nor negative output terminal is grounded.

b. Turn front-panel VOLTAGE and CURRENT controls fully clockwise (maximum).

c. Turn-on power supply (no load connected).

d. Proceed as instructed in Table 5-2.

5-35 <u>Feedback Circuit</u>. Generally, malfunction of the feedback circuit is indicated by high or low output voltages. If one of these situations occurs, disconnect the load and proceed as instructed in Table 5-3 or Table 5-4.

Step	Measure (-) (+)	Response	Probable Cause
	Voltage between +S and A5.	a. +0.6V b. 0V or negative	a. Open strap between A8 and -S. R20 open. b. Proceed to Step 2.
2	Voltage between 13 and 14.	<ul> <li>a. More negative than -0.1V.</li> <li>b. Within ±0.1V of 0V.</li> <li>c. More positive than +0.1V.</li> </ul>	§
3	Voltage between +S and 25.	<ul><li>a. More negative than +0.5V,</li><li>b. More positive than +0.5V.</li></ul>	Q8, R23, R31, R33 open.
4	Voltage between +S and 27.	a. 0V to +0.2V. b. More positive than 0.2V.	a. Q10 or Q11 shorted. b. Q9 open, R35 shorted.

### Table 5-3. High Output Voltage Troubleshooting

Table 5-4. Low Output Voltage Troubleshooting

Step	Measure (-) (+)	Response	Probable Cause
1	Disable Q5 by disconnect- ing CR8.	a. Normal output voltage. b. Low output voltage.	<ul> <li>a. Current limit circuit faulty, check CR8,Q5, and R26 for short.</li> <li>b. Reconnect CR8 and proceed to Step 2.</li> </ul>
2	Voltage between +S and A5.	a. More negative than +0.1V. b. +0.1V to +0.8V.	a. C4 shorted, R17,R18 open. b. Proceed to Step 3.
3	Voltage between 13 and 14	a. More positive than +0.1V. b. More negative than -0.1V.	

4	Voltage between +S and 25.	<ul> <li>a. More positive than +0.6V.</li> <li>b. More negative than +0.5V.</li> <li>b. Proceed to Step 5.</li> </ul>
5	Voltage between +S and 27.	<ul> <li>a. More positive than 1V.</li> <li>b. More negative than 0V.</li> <li>c. Q10, Q11 open. R38 shorted.</li> <li>b. Q9, CR10, CR11, CR12,</li> <li>C9 shorted.</li> <li>CR13, CR14, CR15 open.</li> <li>R35 open.</li> </ul>

### Table 5-4. Low Output Voltage Troubleshooting (Continued)

\*Check Q9 and CR9 for damage

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Table 5-5. Commo	n Troubles
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Symptom	<ul> <li>Checks and Probable Causes</li> <li>a. Check operating setup for ground loops.</li> <li>b. If output floating, connect 1µf capacitor between output and ground.</li> <li>c. Ensure that supply is not crossing over to current limit mode under loaded conditions. Check for low voltage across C19.</li> </ul>		
High ripple			
Poor line regulation	a. Check reference circuit (Paragraph 5-34).		
Poor load regulation (Constant Voltage)	<ul> <li>a. Measurement technique. (Paragraph 5-15.)</li> <li>b. Check reference circuit (Paragraph 5-34).</li> <li>c. Ensure that supply is not going into current limit. Check current limit circuit.</li> </ul>		
Oscillates a. Constant Voltage Operation b. Current Limit Operation	a. C6,R30,C3,R9,C7,R34,C8, or C9 open b. C5,R29, or C9 open		
Poor Stability (Constant Voltage)	<ul> <li>a. Check ±6.2 Vdc reference voltages (Paragraph 5-34).</li> <li>b. Noisy programming resistor R20.</li> <li>c. CR1, CR2 leaky.</li> <li>d. Check R10, R11, VR1 for noise or drift.</li> <li>e. Stage Q1 defective.</li> </ul>		

5-36 <u>Common Troubles</u>. Table 5-5 lists the symptoms, checks, and probable causes for common troubles.

### 5-37 REPAIR AND REPLACEMENT

5-38 Before servicing a printed wiring board, refer to Figure 5-10. Section VI of this manual

contains a list of replaceable parts. Before replacing a semiconductor device, refer to Table 5-6 which lists the special characteristics of selected semiconductors. If the device to be replaced is not listed in Table 5-6, the standard manufacturers part number listed in Section VI is applicable. After replacing a semiconductor device, refer to Table 5-7 for checks and adjustments that may be necessary. Excessive heat or pressure can lift the copper strip from the board. Avoid damage by using a low power soldering iron (50 watts maximum) and following these instructions. Copper that lifts off the board should be cemented in place with a quick drying acetate base cement having good electrical insulating properties. A break in the copper should be repaired by soldering a short length of tinned copper wire across the break. Use only high quality rosin core solder when repairing etched circuit boards. NEVER USE PASTE FLUX. After soldering, clean off any excess flux and coat the repaired area with a high quality electrical varnish or lacquer. When replacing components with multiple mounting pins such as tube sockets, electrolytic capacitors, and potentiometers, it will be necessary to lift each pin slightly, working around the components several times until it is free. WARNING: If the specific instructions outlined in the steps below regarding etched circuit boards without eyelets are not followed, extensive damage to the etched circuit board will result. 2. Reheat solder in vacant eyelet and quickly 1. Apply heat sparingly to lead of component insert a small awl to clean inside of hole. to be replaced. If lead of component passes through an eyelet If hole does CONDUCTOR not have an in the circuit SIDE eyelet, inboard, apply heat on comsert awl or a #57 drill ponent side from conof board. If ductor side lead of comof board. ponent does not pass through an eyelet, apply heat to conductor side of board. 4. Hold part against board (avoid overheating) 3. Bend clean tinned lead on new part and and solder leads. carefully insert Apply heat to component leads on correct through eyelets or side of board holes in board. as explained a <u>currana</u> curran in step 1. In the event that either the circuit board has been damaged or the conventional method is impractical, use method shown below. This is especially applicable for circuit boards without eyelets. 1. Clip lead as shown below. 2. Bend protruding leads upward. Bend lead of new APPLY CLIP component SOLDER HERE around pro-truding lead. Apply solder **hanna**t using a pair of long nose pliers as a heat sink. This procedure is used in the field only as an alternate means of repair. It is not used within the factory.

Figure 5-10. Servicing Printed Wiring Boards

Reference Designator	Characteristics	①     ③     ③     Stock No.     ③	Suggested Replacement
Ql	Diff. Amp. NPN	1854-0221	2N4045
Q2, Q3, Q9, Q10, Q13-Q15	SS NPN Silicon	1854-0027	2N2714
CR1, CR2, CR4, CR8, CR9, CR16, CR31	Diode, Silicon	1901-0033	1N485B Sylvania
CR10, CR13 CR20	Diode, Sil, 2.4V @ 100 mA	1901-0460	1N4830 G.E.
CR19, CR23	Rect, Sil, Stabistor 200 mA, 10prv	1901-0461	1N4828 G.E.
CR24-CR29, CR30B, CR32-CR34	Rect, Silicon 500 mA, 200prv	1901-0026	1N3253 R.C.A.

### Table 5-6. Selected Semiconductor Characteristics

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Table 5-7. Checks and Adjustments After Replacement of Semiconductor Devices

Reference Function		Check	Adjust
Q1, Q2, Q3, Q7, Q8, Q9	Voltage error amplifier	Voltage load regulation Remote programming	R14
Q10, Q11	Series Regulator	Voltage load regulation	
Q5	Current Limit Amplifier	Current limit operation	
Q12,13,14, 15	Reference Circuit Amplifier	+6.2V line regulation	
Q16	Oven Control Pulse Generator	Oven temperature setting	R56
CR1, 2	Protection Diode	Voltage-load regulation	
		Voltage across each diode 0.6 to 0.85 volts	
CR8	Current Limit Coupling Diode	Current limit operation	
CR9	Overshoot suppressor diode	Turn-on overshoot	
CR16	Overshoot suppressor diode	Turn-on overshoot	
CR19	Reference Circuit Start-up diode	Reference circuit operation	
CR24, 25	Rectifier	Voltage on C16	
CR26,27,28	Rectifier	Voltage on C17	

CR29, 30, 33, 34	Rectifier	Voltage on C19	
CR31	Oven SCR	Oven Functioning	
CR32	Protection diode		
VR1	+6.2 Voltage Reference	Remote Programming Coefficient, zero crossing	R17,R16 R14
VR2	-9.4 Voltage Reference	Remote Prog. Coefficient zero crossing	R16 R14
MI, R64, or R66	-	Current meter cal. Voltage meter cal.	R65 R67

Table 5-7. Checks and Adjustments After Replacement of Semiconductor Devices (Continued)

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### 5-39 ADJUSTMENT AND CALIBRATION

5-40 Adjustment and calibration may be required after performance testing, troubleshooting, or repair and replacement. Perform only those adjustments that affect the operation of the faulty circuit and no others. Table 5-8 summarizes the adjustments and calibrations contained in the following paragraphs.

Adjustment or Calibration	Paragraph	Control Device
Meter Zero	5-41	Pointer
Voltmeter Tracking	5-43	R67
Ammeter Tracking	5-45	R65
Zero Volt Programming Accuracy	5-47	R6 or R8
Programming Current Level	5-49	R13

### 5-41 METER ZERO

5-42 Proceed as follows to zero meter:

a. Turn off instrument (after it has reached normal operating temperature) and allow 30 seconds for all capacitors to discharge.

b. Insert sharp pointed object (pen point or awl) into the small indentation near top of round black plastic disc located directly below meter face.

c. Rotate plastic disc clockwise (cw) until meter reads zero, then rotate ccw slightly in order to free adjustment screw from meter suspension. If pointer moves, repeat steps b and c.

### 5-43 VOLTMETER TRACKING

5-44 To calibrate voltmeter tracking, proceed as follows:

a. Connect differential voltmeter across supply, observing correct polarity.

b. Set METER switch to highest voltage range and turn on supply. Adjust VOLTAGE control until differential voltmeter reads exactly the maximum rated output voltage.

c. Adjust R67 until front panel meter also indicates maximum rated output voltage.

### 5-45 AMMETER TRACKING

5-46 To calibrate ammeter tracking proceed as follows:

a. Connect test setup shown on Figure 5-4.b. Turn VOLTAGE control fully clockwise

and set METER switch to highest current range.

c. Turn on supply and adjust CURRENT controls until differential voltmeter reads 1.0 Vdc.

d. Adjust R65 until front panel meter indicates exactly the maximum rated output current.

5-47 CONSTANT VOLTAGE PROGRAMMING CUR-RENT

5-48 <u>Zero Volt Programming Accuracy</u>. To calibrate the zero volt programming accuracy, proceed as follows:

a. Connect differential voltmeter between +S and -S terminals.

b. Short voltage controls by connecting jumper between terminals A5 and -S.

c. Rotate CURRENT control fully clockwise and turn on supply.

d. Adjust zero crossing potentiometer R14 until the meter indicates zero volts.

5-49 <u>Programming Current Level</u>. To calibrate the constant voltage programming current level, proceed as follows:

a. Connect the supply under test for remote resistance programming as illustrated in Figure 3-3.

b. Connect a 0.1%, 2-watt programming resistor between terminals A4 and -S on rear barrier strip. Resistor value to be as follows:

Model	6101A	6102A	6106A	6111A
Resistance (ohms)	20K	40K	100K	20K
Model	6112A	6113A	6116A	
Resistance (ohms)	40K	10K	100K	

c. Connect a differential voltmeter between -S and +S and turn on the supply.

d. Adjust potentiometer R16 until differential voltmeter indicates the maximum rated output voltage of the supply. If the range of R16 is not sufficient to adjust the output voltage within tolerance proceed to step e.

e. Set potentiometer R16 to the center of its range.

f. Replace R17 with a resistance decade initially set for 300 ohms.

g. Adjust the resistance decade until the differential voltmeter indicates the maximum rated output voltage of the supply.

h. Replace the decade resistance with a resistor whose value is as close to the resistance decade as possible.

i. Readjust R16 until the differential voltmeter indicates the maximum rated output voltage of the supply.

### SECTION VI REPLACEABLE PARTS

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### 6-1 INTRODUCTION

6-2 This section contains information for ordering replacement parts. Table 6-4 lists parts in alphanumeric order by reference designators and provides the following information:

a. Reference Designators. Refer to Table 6-1.

b. Description. Refer to Table 6-2 for abbreviations.

c. Total Quantity (TQ). Given only the first time the part number is listed except in instruments containing many sub-modular assemblies, in which case the TQ appears the first time the part number is listed in each assembly.

d. Manufacturer's Part Number or Type.

e. Manufacturer's Federal Supply Code Number. Refer to Table 6-3 for manufacturer's name and address.

f. Hewlett-Packard Part Number.

g. Recommended Spare Parts Quantity (RS) for complete maintenance of one instrument during one year of isolated service.

h. Parts not identified by a reference designator are listed at the end of Table 6-4 under Mechanical and/or Miscellaneous. The former consists of parts belonging to and grouped by individual assemblies; the latter consists of all parts not immediately associated with an assembly.

### 6-3 ORDERING INFORMATION

6-4 To order a replacement part, address order or inquiry to your local Hewlett-Packard sales office (see lists at rear of this manual for addresses). Specify the following information for each part: Model, complete serial number, and any Option or special modification (J) numbers of the instrument; Hewlett-Packard part number; circuit reference designator; and description. To order a part not listed in Table 6-4, give a complete description of the part, its function, and its location.

Table 6-1. Reference Designators

A	= assembly	E = miscellaneous
B	= blower (fan)	electronic part
C	= capacitor	F = fuse
CB	= circuit breaker	J = jack, jumper
CR	= diode	K = relay
DS	= device, signal- ing (lamp)	L = inductor M = meter

Table 6-1. Reference Designators (Continued)

Р	= plug	V	= vacuum tube,
Q	= transistor		neon bulb,
R	= resistor		photocell, etc.
S	= switch	VR	= zener diode
Т	= transformer	Х	= socket
ΤB	= terminal block	Z	= integrated cir-
TS	= thermal switch		cuit or network
	,		

Table 6-2. Description Abbreviations

А	=	ampere	mfr		manufacturer
ac	=	alternating	mod.	Ξ	modular or
		current			modified
assy.	Ξ	assembly	mtg		mounting
bd	≕	board	n	Ξ	nano = 10 <sup>-9</sup>
bkt	=	bracket	NC	Ξ	normally closed
oС	=	degree	NO	=	normally open
		Centigrade	NP	=	nickel-plated
cd	=	card	n	Ξ	ohm
coef	=	coefficient	obd	=	order by
comp	=	composition			description
CRT	Ξ	cathode-ray	OD	=	outside
		tube			diameter
CT	=	center-tapped	р	=	$pico = 10^{-12}$
dc	=	direct current	P.C.		printed circuit
DPDT	=	double pole,	pot.	Ξ	potentiometer
		double throw	p-p	=	peak-to-peak
DPST	=	double pole,	ppm	=	parts per
		single throw			million
elect	=	electrolytic	pvr	=	peak reverse
encap	) ==	encapsulated			voltage
F	=	farad	rect	=	rectifier
٥F	=	degree	rms	=	root mean
		Farenheit			square
fxd	=	fixed	Si	≓	silicon
Ge	=	germanium	SPDT		single pole,
H	17	Henry			double throw
Hz	=	Hertz	SPST	Ξ	single pole,
IC	=	integrated			single throw
1		circuit	SS		small signal
ID		inside diameter	Т		slow-blow
incnd		incandescent	tan.		tantulum
k		kilo = $10^3$	Ti		titanium
m		milli = $10^{-3}$	V		volt
M	Ξ	mega = 10 <sup>6</sup>	var		variable
μ	=	micro = 10 <sup>-6</sup>	ww		wirewound
met.		metal	W	=	Watt
L			<u> </u>		

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Table 6-3. Code List of Manufacturers

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CODE NO.	MANUFACTURER ADDRESS
00629	EBY Sales Co., Inc. Jamaica, N.Y.
00656	Aerovox Corp. New Bedford, Mass.
00853	Sangamo Electric Co.
00000	S. Carolina Div. Pickens, S.C.
01121	Allen Bradley Co. Milwaukee, Wis.
01255	Litton Industries, Inc.
01200	Beverly Hills, Calif.
01281	TRW Semiconductors, Inc.
01001	Lawndale, Calif.
01295	Texas Instruments, Inc.
	Semiconductor-Components Div.
	Dallas, Texas
01686	RCL Electronics, Inc. Manchester, N. H.
01930	Amerock Corp. Rockford, Ill.
02107	Sparta Mfg. Co. Dover, Ohio
02114	Ferroxcube Corp. Saugerties, N.Y.
02606	Fenwal Laboratories Morton Grove, Ill.
02660	Amphenol Corp. Broadview, Ill.
02735	Radio Corp. of America, Solid State
	and Receiving Tube Div. Somerville, N.J.
03508	G.E. Semiconductor Products Dept.
	Syracuse, N.Y.
03797	Eldema Corp. Compton, Calif.
03877	Transitron Electronic Corp.
	Wakefield, Mass.
03888	Pyrofilm Resistor Co. Inc.
	Cedar Knolls, N.J.
04009	Arrow, Hart and Hegeman Electric Co.
	Hartford, Conn.
04072	ADC Electronics, Inc. Harbor City, Calif.
04213	Caddell & Burns Mfg. Co. Inc.
	Mineola, N.Y.
04404	*Hewlett-Packard Co. Palo Alto Div.
	Palo Alto, Calif.
04713	Motorola Semiconductor Prod. Inc.
0.7.000	Phoenix, Arizona
05277	Westinghouse Electric Corp.
00047	Semiconductor Dept. Youngwood, Pa.
05347	Ultronix, Inc. Grand Junction, Colo.
05820 06001	Wakefield Engr. Inc. Wakefield, Mass.
00001	General Elect. Co. Electronic Capacitor & Battery Dept. Irmo, S.C.
06004	Capacitor & Battery Dept. Irmo, S.C. Bassik Div. Stewart-Warner Corp.
00004	Bridgeport, Conn.
06486	IRC Div. of TRW Inc.
00100	Semiconductor Plant Lynn, Mass,
06540	Amatom Electronic Hardware Co. Inc.
00030	New Rochelle, N.Y.
06555	Beede Electrical Instrument Co.
00000	Penacook, N.H.
06666	General Devices Co. Inc.
00000	Indianapolis, Ind.
06751	Semcor Div. Components, Inc.
00101	Phoenix, Arizona
06776	Robinson Nugent, Inc. New Albany, Ind.
06812	Torrington Mfg. Co., West Div.
	Van Nuys, Calif.
07137	Transistor Electronics Corp.
57407	Minneapolis, Minn.
L	winneapoira, Willin,

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CODE	
NO.	MANUFACTURER ADDRESS
07138	Westinghouse Electric Corp. Electronic Tube Div. Elmira, N.Y.
07263	Fairchild Camera and Instrument Corp. Semiconductor Div.
07387 07397	Mountain View, Calif. Birtcher Corp., The Los Angeles, Calif. Sylvania Electric Prod. Inc.
07716	Sylvania Electronic Systems Western Div. Mountain View, Calif. IRC Div. of TRW Inc. Burlington Plant
07910	Burlington, Iowa Continental Device Corp.
07933	Hawthorne, Calif. Raytheon Co. Components Div. Semiconductor Operation Mountain View, Calif.
08484	Breeze Corporations, Inc. Union, N.J.
08530	Reliance Mica Corp. Brooklyn, N.Y. Sloan Company, The Sun Valley, Calif.
08717 08730	Sloan Company, The Sun Valley, Calif. Vemaline Products Co. Inc. Wyckoff, N.J.
08730	General Elect, Co. Minia-
	ture Lamp Dept. Cleveland, Ohio
08863	ture Lamp Dept. Cleveland, Ohio Nylomatic Corp. Norrisville, Pa. RCH Supply Co. Vernon, Calif.
08919	RCH Supply Co. Vernon, Calif. Airco Speer Electronic Components
09021 09182	Hewlett-Packard Co. New Jersey Div.
	Berkeley Heights, N.J.
09213	General Elect. Co. Semiconductor Prod. Dept. Buffalo, N.Y.
09214	Prod. Dept. Buffalo, N.Y. General Elect. Co, Semiconductor Prod. Dept. Auburn, N.Y.
09353	C & K Components Inc. Newton, Mass.
09922	Burndy Corp. Norwalk, Conn.
11115	Wagner Electric Corp. Tung-Sol Div. Bloomfield, N.J.
11236 11237	CTS of Berne, Inc. Berne, Ind. Chicago Telephone of Cal. Inc.
11502	So. Pasadena, Calif. IRC Div. of TRW Inc. Boone Plant
11711	Boone, N.C. General Instrument Corp Rectifier Div. Newark, N.I.
12136	Philadelphia Handle Co. Inc. Camden, N.J.
12615	U.S. Terminals, Inc. Cincinnati, Ohio
12617	Hamlin Inc. Lake Mills, Wisconsin
12697	Clarostat Mfg. Co. Inc. Dover, N. H.
13103	Thermalloy Co. Dallas, Texas
14493	*Hewlett-Packard Co. Loveland Div. Loveland, Colo.
14655	Cornell-Dubilier Electronics Div. Federal Pacific Electric Co.
14936	Newark, N.J. General Instrument Corp. Semicon- ductor Prod. Group Hicksville, N.Y.
15801	Fenwal Elect. Framingham, Mass.
16299	Corning Glass Works, Electronic
	Components Div. Raleigh, N.C.

\*Use Code 28480 assigned to Hewlett-Packard Co., Palo Alto, California

CODE NO.	MANUFACTURER ADDRESS
16758	Delco Radio Div. of General Motors Corp. Kokomo, Ind.
17545	Atlantic Semiconductors, Inc. Asbury Park, N.J.
17803	Fairchild Camera and Instrument Corp Semiconductor Div, Transducer Plant Mountain View, Calif.
17870	Daven Div. Thomas A. Edison Industries McGraw-Edison Co. Orange, N.J. Signetics Corp. Sunnyvale, Calif.
18324	Signetics Corp. Sunnyvale, Calif.
19315	Bendix Corp. The Navigation and Control Div. Teterboro, N.J.
19701	Electra/Midland Corp. Mineral Wells, Texas
21520	Fansteel Metallurgical Corp. No. Chicago, Ill.
22229	Union Carbide Corp. Electronics Div. Mountain View, Calif.
22753	UID Electronics Corp. Hollywood, Fla.
23936	Pamotor, Inc. Pampa, Texas
24446	General Electric Co. Schenectady, N.Y.
24455	General Electric Co. Lamp Div. of Con-
	sumer Prod. Group Nela Park, Cleveland, Ohio
24655	General Radio Co. West Concord, Mass.
24681	LTV Electrosystems Inc Memcor/Com-
26982	ponents Operations Huntington, Ind. Dynacool Mfg. Co. Inc. Saugerties, N.Y.
27014	National Semiconductor Corp.
	Santa Clara, Calif.
28480	Hewlett-Packard Co. Palo Alto, Calif.
28520	neyment wirg. CO. Rennworth, N.J.
28875	IMC Magnetics Corp. New Hampshire Div. Rochester, N.H.
31514	SAE Advance Packaging, Inc. Santa Ana, Calif.
31827	Budwig Mfg. Co. Ramona, Calif.
33173	G.E. Co. Tube Dept. Owensboro, Ky.
35434	Lectrohm, Inc. Chicago, Ill.
37942	P.R. Mallory & Co. Inc.
42190	Indianapolis, Ind. Muter Co. Chicago, Ill.
	New Departure-Hyatt Bearings Div.
11075	General Motors Corp. Sandusky, Ohio
$\begin{array}{c} 44655\\ 46384\end{array}$	Ohmite Manufacturing Co. Skokie, Ill. Penn Engr. and Mfg. Corp.
4.00.00.0	Doylestown, Pa.
47904	Polaroid Corp. Cambridge, Mass.
49956	Raytheon Co. Lexington, Mass.
55026	Simpson Electric Co. Div. of American Gage and Machine Co. Chicago, Ill.
56289	Sprague Electric Co. North Adams, Mass.
58474	Superior Electric Co. Bristol, Conn.
58849	Syntron Div. of FMC Corp. Homer City, Pa.
59730	Thomas and Betts Co. Philadelphia, Pa.
61637	Union Carbide Corp. New York, N.Y.
63743	Ward Leonard Electric Co.
007.50	Mt. Vernon, N.Y.

CODE MANUFACTURER NO. ADDRESS 70563 Amperite Co. Inc. Union City, N.J. 70901 Fort Washington, Pa. Beemer Engrg. Co. 70903 Belden Corp. Chicago, Ill. 71218 Bud Radio, Inc. Willoughby, Ohio 71279 Cambridge Thermionic Corp. Cambridge, Mass. 71400 Bussmann Mfg. Div, of McGraw & Edison Co. St. Louis, Mo. 71450 CTS Corp. Elkhart, Ind. 71468I. T. T. Cannon Electric Inc. Los Angeles, Calif. 71590 Globe-Union Inc. Centralab Div. Milwaukee, Wis. 71700 General Cable Corp. Cornish Wire Co. Div. Williamstown, Mass. 71707 Coto Coil Co. Inc. Providence, R.I. 71744 Chicago Miniature Lamp Works Chicago, Ill. 71785 Cinch Mfg. Co. and Howard B. Jones Div. Chicago, Ill. 71984 Dow Corning Corp. Midland, Mich. 72136 Electro Motive Mfg. Co. Inc. Willimantic, Conn. 72619 Dialight Corp. Brooklyn, N.Y. 72699 General Instrument Corp. Newark, N.J. 72765 Drake Mfg. Co. Harwood Heights, Ill. 72962 Elastic Stop Nut Div. of Amerace Esna Corp. Union, N.J. 72982 Erie Technological Products Inc. Erie, Pa. 73096 Hartford, Conn. Hart Mfg. Co. 73138 Beckman Instruments Inc. Helipot Div. Fullerton, Calif. 73168 Fenwal, Inc. Ashland, Mass. 73293 Hughes Aircraft Co. Electron Dynamics Div. Torrance, Calif. 73445 Amperex Electronic Corp. Hicksville, N.Y. 73506 Bradley Semiconductor Corp. New Haven, Conn. 73559 Carling Electric, Inc. Hartford, Conn. 73734 Federal Screw Products, Inc. Chicago, Ill. 74193 Heinemann Electric Co. Trenton, N.J. 74545 Hubbell Harvey Inc. Bridgeport, Conn. 74868 Amphenol Corp. Amphenol RF Div. Danbury, Conn. 74970 E.F. Johnson Co. Waseca, Minn. 75042 IRC Div. of TRW, Inc. Philadelphia, Pa. 75183 \*Howard B. Jones Div. of Cinch Mfg. Corp. New York, N.Y. 75376 Kurz and Kasch, Inc. Dayton, Ohio 75382 Kilka Electric Corp. Mt. Vernon, N.Y. 75915 Littlefuse, Inc. Des Plaines, Ill. 76381 Minnesota Mining and Mfg. Co. St. Paul, Minn. 76385 Minor Rubber Co. Inc. Bloomfield, N.J. 76487 James Millen Mfg. Co. Inc. Malden, Mass. 76493 I.W. Miller Co. Compton, Calif.

Table 6-3. Code List of Manufacturers (Continued)

\*Use Code 71785 assigned to Cinch Mfg. Co., Chicago, Ill.

Table 6-3.	Code List	of Manufacturers	(Continued)
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CODE NO.	MANUFACTURER ADDRESS
76530 76854	Cinch City of Industry, Calif. Oak Mfg, Co. Div. of Oak
77068	Electro/Netics Corp. Crystal Lake, Ill. Bendix Corp., Electrodynamics Div. No. Hollywood, Calif.
77122 77147	Palnut Co. Mountainside, N.J. Patton-MacGuyer Co. Providence, R.I.
77221	Phaostron Instrument and Electronic Co. South Pasadena, Calif.
77252	Philadelphia Steel and Wire Corp. Philadelphia, Pa.
77342 77630	American Machine and Foundry Co. Potter and Brumfield Div. Princeton, Ind. TRW Electronic Components Div.
77764	Camden, N.J. Resistance Products Co. Harrisburg, Pa.
78189	Illinois Tool Works Inc. Shakeproof Div. Elgin, Ill.
78452 78488 78526	Everlock Chicago, Inc. Chicago, Ill. Stackpole Carbon Co. St. Marys, Pa. Stanwyck Winding Div. San Fernando
78553	Electric Mfg. Co. Inc. Newburgh, N.Y. Tinnerman Products, Inc. Cleveland, Ohio
78584 79136	Stewart Stamping Corp.Yonkers, N.Y.Waldes Kohinoor, Inc.L.I.C., N.Y.Whitehead Metals Inc.New York, N.Y.
79307 79727	Continental-Wirt Electronics Corp.
79963 80031	Philadelphia, Pa. Zierick Mfg. Co, Mt. Kisco, N.Y. Mepco Div. of Sessions Clock Co.
80294 81042	Morristown, N.J. Bourns, Inc. Riverside, Calif. Howard Industries Div. of Msl Ind. Inc.
81073 81483	Racine, Wisc. Grayhill, Inc. La Grange, Ill. International Rectifier Corp. El Segundo, Calif.
81751 82099	Columbus Electronics Corp. Yonkers, N.Y. Goodyear Sundries & Mechanical Co. Inc. New York, N.Y.
82142	Airco Speer Electronic Components Du Bois, Pa.
82219	Sylvania Electric Products Inc. Electronic Tube Div. Receiving Tube Operations Emporium, Pa.
82389	Switchcraft, Inc. Chicago, Ill.
82647	Metals and Controls Inc. Control Products Group Attleboro, Mass.
82866	Research Products Corp. Madison, Wis,
82877 82893	Rotron Inc. Woodstock, N.Y. Vector Electronic Co. Glendale, Calif.
83058 83186	Carr Fastener Co. Cambridge, Mass. Victory Engineering Corp.
83298	Springfield, N.J. Bendix Corp.Electric Power Div. Eatontown, N.J.
83330	Herman H. Smith, Inc. Brooklyn, N.Y.
83385	Central Screw Co. Chicago, Ill.
83501	Gavitt Wire and Cable Div. of Amerace Esna Corp. Brookfield, Mass.

CODE NO.	MANUFACTURER ADDRESS
83508	Grant Pulley and Hardware Co. West Nyack, N.Y.
83594	Burroughs Corp. Electronic
83835 83877	Components Div. Plainfield, N.J. U.S. Radium Corp. Morristown, N.J. Yardeny Laboratories, Inc. New York, N.Y.
84171 84411 86684	Arco Electronics, Inc. Great Neck, N.Y. TRW Capacitor Div. Ogallala, Neb. RCA Corp. Electronic Components
86838 87034	Rummel Fibre Co. Newark, N.J. Marco & Oak Industries a Div. of Oak Electro/netics Corp. Anaheim, Calif.
87216 87585	Philco Corp. Lansdale Div. Lansdale, Pa. Stockwell Rubber Co. Inc. Philadelphia, Pa.
87929 88140	Tower-Olschan Corp. Bridgeport, Conn. Cutler-Hammer Inc. Power Distribution and Control Div. Lincoln Plant Lincoln, Ill.
88245	Litton Precision Products Inc, USECO
90634 90763 91345	Div. Litton Industries Van Nuys, Calif. Gulton Industries Inc. Metuchen, N.J. United-Car Inc. Chicago, Ill. Miller Dial and Nameplate Co.
91343 91418	Radio Materials Co. Augat, Inc. El Monte, Calif. Chicago, Ill. Attleboro, Mass.
91506	Augat, Inc. Attleboro, Mass.
91637 91662	Dale Electronics, Inc. Columbus, Neb. Elco Corp. Willow Grove, Pa.
91929	Honeywell Inc. Div. Micro Switch Freeport, Ill.
92825 93332	Whitso, Inc. Schiller Pk., Ill. Sylvania Electric Prod. Inc. Semi-
93410	conductor Prod. Div. Woburn, Mass. Essex Wire Corp. Stemco
94144	Controls Div. Mansfield, Ohio Raytheon Co. Components Div. Ind. Components Oper. Quincy, Mass.
94154	
94222 95263	Southco Inc. Lester, Pa.
95354 95712	
95987	Devices Div. Franklin, Ind.
95987 96791	Weckesser Co. Inc. Chicago, Ill. Amphenol Corp. Amphenol Controls Div. Janesville, Wis.
97464	Industrial Retaining Ring Co. Irvington, N.J.
97702	IN Migron, N.J. IMC Magnetics Corp. Eastern Div. Westbury, N.Y.
98291 98410	
98978	International Electronic Research Corp. Burbank, Calif.
99934	Renbrandt, Inc. Boston, Mass.

Reference Designator	Description C	Quantity	Mfr. Part # or Type	Mfr.	Mfr. Code	ft Stock No.	RS
<u></u>	find alogt the Stude	1	150D105X9035A2	Sprague	56289	0180-0291	1
C1	fxd, elect 1µf 35vdc fxd, film 0.1µf 200vdc	1	192P10492	Sprague	56289	0160-0168	1
C2	fxd, film $.033\mu$ f 200vdc	3	192P33392	Sprague	56289	0160-0163	1
C3,13,21	•	1	260P10592S3	Sprague	56289	0160-2579	1
C4	fxd, film 1µf 200vdc	1		Sprague	56289	0160-2453	1
C5	fxd, film . 22µf 80vdc	2	192P2249R8 192P10292	Sprague	56289	0160-0153	1
C6,8	fxd, film .001µf 200vdc			Sprague	56289	0160-0166	1
C7	fxd, film .068µf 200vdc	1	192P68392	Sprague	56289	0160-0157	1
C9	fxd, film.0047µf 200vdc	1	192P47292		56289	0180-0049	1
C10,14	fxd, elect 20µf 50vdc	2	30D206G050DC4	Sprague	30203	0100-0049	Т
C11,12,						_	
15,22	NOT ASSIGNED				- 09182	- 0180-0332	1
C16	fxd, elect 325µf 35vdc	1	D34656	HLAB		0180-1893	1
C17,23	fxd, elect 1450µf 45vdc	2	D39532	HLAB	09182	0100-1033	T
C18B,25	fxd, ceramic .02µf 600vdc			11 <sup>11</sup>		0150 0004	1
	Dis 6	-	ED02	Erie	72982	0150-0024	1
C19	fxd, elect 1500µf 40vdc	1	D38733	HLAB	09182	0180-1894	
C20	fxd, film .0022 $\mu$ f 200vdc	1	192P22292	Sprague	56289	0160-0154	1
C24	fxd, film 1µf 200vdc	1	118P10592S3	Sprague	56289	0160-2465	1
CR1,2,4, 8,9.16 CR3,5-7,	Diode si. 250MW 200prv	6		HLAB	09182	1901-0033	6
11,12,14, 15,17,18,							
21,22	NOT ASSIGNED	-	-		-	-	2
CR10,13,20		3		HLAB	09182	1901-0460	3
CR19,23	Rect. si. 200ma 10prv	2		HLAB	09182	1901-0461	2
CR24-28,32 CR29,30B,	Rect. si. 500MA 200prv	6	1N3253	R.C.A.	02735	1901-0389	6
33,34	Rect. si. 1A 200prv	4	1N5059	G.E.	03508	1901-0327	4
CR30A	NOT USED		-	-	_	-	
CR31	SCR 1.6A 50prv	1	C6F	G. E.	03508	1884-0033	THE REAL PROPERTY IN THE REAL PROPERTY INTO THE REAL PR
DS1	Lamp neon part of Slass'y	Ref		HLAB	09182	2140-0244	1
Fl	Fuse cartridge 1A@250V 3A	G 1	312001	Littlefuse	75915	2110-0001	5
L1,2	Coil	2		HLAB	09182	9100-1854	1
01	Diff. Amp. NPN (oven ass'	'y) 1		HLAB	09182	1854-0021	1
Q1	SS NPN si. (oven ass'y)	2		HLAB	09182	1854-0027	2
Q2,3		-	_	-	<u>-</u>	~	-
Q4,6	NOT ASSIGNED	1	2N3390	G.E.	03508	1854-0202	1
Q5	SS NPN si.	2	2N2907A	Sprague	56289	1853-0099	2
Q7,8	SS PNP si.	24	ZINZJU/M	opragao	00200		
Q9,10,	(1) DINAI	5		HLAB	09182	1854-0027	5
13-15	SS NPN si.	1		HLAB	09182	1854-0225	1
Q11	Power NPN si.	1	10262	R.C.A.	02735	1853-0041	1
Q12	SS PNP si.		40362 2N2646	G. E.	03508	1855-0010	1
Q16	Uni Junction si.	1	2N2646				
R1,2	fxd, ww lKn $\pm 5\%$ 3w	2	242E1025	Sprague	56289	0813-0001	1
R3	fxd, met. film 221Ka±1% 1/		Type CEA T-O	I. R. C.	07716	0757-0473	1
R4	fxd, met. film $27.4$ Ka $\pm 1\%$		Туре СЕА Т-О	I.R.C.	07716	0757-0452	1
R5,6	fxd, met. film $432$ Ka $\pm 1\%$ l	/8w 2	Туре СЕА Т-О	I.R.C.	07716	0757-0480	2
R7,8	fxd, met. film $43K_{f} \pm 1\% 1/4$		Type CEA T-O	I.R.C.	07716	0698-5090	2
R9	fxd, comp 120 $_{n}$ ±5% 1/2w	1	EB-1215	A. B.	01121	0686-1215	1

Reference Designator	Description Qua	antity_	Mfr. Part # or Type	Mfr.	Mfr. Code	fi Stock No.	RS
R10,12,19	NOT USED	-	<b>⊷</b>	_	_	<u>-</u>	<u>-</u>
R11,20,							
51,58	NOT ASSIGNED	-	-	-	-		-
R13,15	fxd, met.film 1 MEG ±1% 1/4w	2	Туре СЕВ Т-О	I. R. C.	07716	0757-0344	1
R14,16	var. ww $15K_{n} \pm 5\% 1W @ 50^{\circ}C$	2	Model 100	I.R.C.	07716	2100-0896	1
R17	fxd, ww 297 ±1% 1/4w	1		HLAB	09182	0811-1929	1
R18	fxd, ww 5.9K ±1% 0±5%ppm/ <sup>O</sup>	C1		HLAB	09182	0811-1978	1
R21	fxd, met. film 2K ±1% 1/8w	1	Type CEA T-O	I.R.C.	07716	0757-0283	1
R22	Thermistor $64n \pm 10\%$	1	LB16J1	Fenwal	15801	0837-0023	1
R23	fxd, ww $\ln \pm .5\%$ 8w	1	Type T-7A	R.C.L.	01686	0811-2133	1
R24	fxd, comp 7.5Kn $\pm 5\%$ 1/2w	1	EB-7525	A. B.	01121	0686-7525	1 1
R25	var. ww $1K_{n} \pm 5\%$	1	mp1005	HLAB	09182	2100-1847	1
R26,32,43 R27,28,33,	fxd, comp $10K_{A} \pm 5\% 1/2w$	3	EB1035	A.B.	01121	0686-1035	
60	fxd, comp $1K_{h} \pm 5\% 1/2w$	4	EB1025	A. B.	01121	0686-1025	1
R29	fxd, comp $100_{n} \pm 5\% 1/2w$	1	EB-1015	A. B.	01121	0686-1015	1
R30	fxd, comp 5.1Kn $\pm 5\%$ 1/2w	1	EB-5125	A. B.	01121	0686-5125	1
R31	fxd, comp $3.9$ Kn $\pm 5\% 1/2$ w	1	EB-3925	A. B.	01121	0686-3925	1
R34	fxd, comp $390_{\text{A}} \pm 5\% 1/2w$	1	EB-3915	A. B.	01121	0686-3915	1
R35,59	fxd, comp $680n \pm 5\% 1/2w$	2	EB-6815	A.B.	01121	0686-6815	1
R36,61	fxd, comp $2K_n \pm 5\% 1/2w$	2	EB-2025	A. B.	01121	0686-2025	1
R37	fxd, comp $10n \pm 5\% 1/2w$	1	EB-1005	A. B.	01121	0686-1005	1
R38,45	fxd, comp $1.5K_h \pm 5\% l/2w$	2	EB-1525	A. B.	01121	0686-1525	1
R39	fxd, met. ox $300 \pm 5\%$ 2w	1	Type C425	Corning	16299	0698-3630	1
R40	fxd, ww 400 $n \pm 5\%$ 5w	1	Type 5XM	W.L.	63743	0811-1857	1 1
R41	fxd, comp $200_{n} \pm 5\% 1/2w$	1	EB-2015	A.B.	01121	0686-2015	
R42	fxd, met. film $42.2 \pm 1\% 1/8w$		Type CEA T-O	I.R.C.	07716	0757-0316	1 1
R44	fxd, comp 4.3Ka $\pm 5\%$ 1/2w	1	EB-4325	A. B.	01121	0686-4325 0686-2725	1
R46,53	fxd, comp $2.7$ Kn $\pm 5\%$ $1/2$ w	2	EB-2725	A.B.	01121		1
R47,48	fxd, met. film 1.5Kn ±1% 1/8v		Туре СЕА Т-О	I.R.C.	07716	0757-0427 0811-1935	1
R49	fxd, ww 714 $_{A}$ ±1% 1/4w	1	100	HLAB	09182	0811-1758	1
R50	fxd, ww $.24n \pm 5\%$	1	Type BWH	I.R.C.	07716 01121	0686-2425	1
R52	fxd, comp 2. 4Ka $\pm 5\%$ 1/2w	1	EB-2425	A.B.	63743	0811-1860	1
R54	fxd, ww $600_{A} \pm 5\%$ 5w	1	Type 5XM	W.L. A.B.	01121	0686-3335	1
R55	fxd, comp $33K_{h} \pm 5\% 1/2w$	1	EB-3335	А. В. А. В.	01121	0000 0000	1
R56,66 R57	fxd, compSELECTIVE ±5% 1/2 Thermister 100Kn ±10%		Type EB			0007 0000	
	(oven ass'y)	1	51TG4	Gulton	90634	0837-0026	1
R62	fxd, comp 220n ±5% 1/2w	1	EB-2215	A.B.	01121	0686-2215	1
R63	fxd, ww.51 ±5%	1	Type BWH	I.R.C.	07716	0811-0929	1
R64	fxd, met. film 1.21K ±1% 1/8		Type CEA T-O	I.R.C.	07716	0757 - 0274	1 1
R65	var. ww 10n	1	Type 110-F4	C. T. S.	11236	2100-1822 2100-0391	1
R67	var. ww lK	1	Type 110-F4	C.T.S.	11236	0686-5615	1
R68	fxd, comp 560±5% 1/2w	1	EB-5615	A.B.	01121	0698-4484	Ţ
R69	fxd, met. film 19.1K ±1% 1/8v	ν£	Туре СЕА Т-О	I.R.C.	07716		_
S1	Switch, pilot lt. (red) ON/OF	F 1	54-61681 - 26 AlH		87034	3101-0100	1
S2	Meter switch, wafer	1		HLAB	09182	3100-1900	1
S3	Thumbwheel switch	1	See parts listed b				1
R200*	var. ww 10n	1		HLAB	09182	2100-1887	1
R201-209*			Type E-20	R.C.L.	01686	0811-1958	2
R211-219*			Type E-20	R. C. L.	01686	0811-1968	2
R221-229*			Type E-20	R. C. L.	01686	0811-1976	2
R231*	fxd, ww10Kn ±0.1% 1/2w 5pp		Type E-30	R.C.L.	01686	0811-1994	<u>1</u>
S201-204*	Rotary switch 10 pos.SPKEL-	-F 4		HLAB	09182	3100-1902	1

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Reference			Mfr. Part #		Mfr.	<i>₩</i>	
Designator	Description Que	ntity	or Type	Mfr.	Code	Stock No.	RS
~ ^	Mine has a suite from time of	31					
\$3	Thumbwheel switch (continued			HLAB	09182	5060-6104	1
	*PC Board ass'y, potentiomete			HLAB	09182	5020-5508	1
	*PC Board ass'y, thumbwheel	4 4		HLAB	09182	4040-0047	ī
	*Thumbwheel stamping	1		HLAB	09182	4040-0048	î
	*Thumbwheel stamping			HLAB	09182	4040-0044	1
	*Thumbwheel mtg. bkt.	5			09182	4040-0045	1
	*Thumbwheel mtg. bkt. mod #1			HLAB	09182	5080-7107	1
	*Thumbwheel mtg. bkt. mod #2			HLAB	09182	5080-7108	î
	*Thumbwheel mtg. bkt. mod#:			HLAB	09182	5020-5517	î
	*Strap-locking, 1/16" Delrin	2			09182	4040-0049	1
	*Gear and shaft	4		HLAB	09164	4040~0049	ř
Tl	Power transformer	1		HLAB	09182	9100-2127	1
VR1	Zener 6.2V ±5% 250mw						
• • • •	(oven ass'y)	1	1 N 8 2 5	Transitron	03877	1902-0777	1
VR2	Diode, zener 9.4V 500mw	1	1N2163	U.S.Semcor	06751	1902-0762	1
	Side chassis - right	1		HLAB	09182	5000-6093	
	Side chassis - left	1		HLAB	09182	5000-6094	
	Panel - front	1		HLAB	09182	5000-6095	
		1		HLAB	09182	5000-6096	
	Trim strip	1		HLAB	09182	5000-6097	
	Chassis - rear	2		HLAB	09182	5000-6061	
	Cover	1		HLAB	09182	5020-5540	
	Guard - angle	1		HLAB	09182	5000-6070	
	Can - outer	1		HLAB	09182	5000-6071	
	Can - inner			HLAB	09182	5060-6125	
	Ass'y - oven	Ref	T) 1 \ 1 \ 4 \	HLAB	09182	1510-0040	1
	5 Way binding post (maroon)	1	DF21Mn	Superior	58474	1510-0039	1
	5 Way binding post (black)	2	DF21BC	Whitehead		1400-0330	-
	Cable clamp 1/4 I.D.	1	T4-4	Beldon	70903	8120-0050	1
	Line cord plug PH151 7 1/2 ft.		KH 4096 SR-5P-1	Heyco	28520	0400-0013	ĩ
	Strain relief bushing	1	SK-SF-1		09182	0370-0084	1
	Knob 1/4 insert pointer	2	400 10 11010	HLAB	71785	0360-1143	1
	Jumper	5	422-13-11013	Cinch HLAB	09182	0360-1234	1
	Barrier strip	1	1050	Stockwell		0403-0088	1
	Rubber bumper	4	MB50	Stockwell		0403-0086	1
	Rubber bumper	3	4072			4040-0295	1
	Bezel 1/6 MOD	1		HLAB	09182	4040-0200	4
	Meter 2 1/4" size DUAL scal				00103	1120-1226	n
	0-24V 0-1.2A	1		HLAB	09182	1460-0720	1
	Spring'	4		HLAB	09182	0510-0275	1
	Fastener	8	C8091632-24B			0340-0174	2
	Mica insulator	1	734	Reliance	08530		ן נ
	Insulator, transistor pin	2		HLAB	09182	0340~0166	1
	Insulator	2		HLAB	09182	0340-0168	1

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OPTION 06:					,
Overvoltage "Crowbar"					
Protector Model 6916A	1	-	HLAB	09182	Model 6916A

### APPENDIX A

2-3 - L

### Option 11, Overvoltage Protection "Crowbar"

### DESCRIPTION:

This option is installed in DC Power Supplies, 6101A, 6102A, 6106A, 6111A, 6112A, 6113A, and 6116A, and tested at the factory. It consists of a printed circuit board, screwdriver-type front panel potentiometer, and four wires that are soldered to the main power supply board.

The crowbar monitors the output voltage of the power supply and fires an SCR that shorts the output when it exceeds the preset trip voltage. The trip voltage is determined by the setting of the CROWBAR ADJUST control on the front panel. The trip voltage range is as follows:

Model	6101A	6102A	6106A	6111A	6112A	6113A	6116A
Trip Voltage Range	3.2-23V	3.2-44V	20-110V	3.2-23V	3.2-44V	3.2-13V	20 <b>-</b> 110V

To prevent transients from falsely tripping the crowbar, the trip voltage must be set higher than the power supply output voltage by the following margin: 7% of the output voltage +1V. The margin represents the minimum crowbar trip setting for a given output voltage; the trip voltage can always be set higher than this margin.

### **OPERATION:**

- 1. Turn the CROWBAR ADJUST fully clockwise to set the trip voltage to maximum.
- 2. Set the power supply VOLTAGE control for the desired crowbar trip voltage. To prevent false crowbar tripping, the trip voltage should exceed the desired output voltage by 7% of the output voltage +1V.
- 3. Slowly turn the CROWBAR ADJUST counterclockwise until the crowbar trips, and the output falls to a small positive voltage (about 1.8V or less).
- 4. The crowbar will remain activated and the output shorted until the supply is turned off. To reset the crowbar, turn the supply off, then on.

REF. DESIG.	DESCRIPTION	TQ	MFR. PART NO.	MFR. CODE	HP PART NO.	ŔS
C1 C2	fxd, elect 1μF 50Vdc fxd, mica 510μF 500Vdc	1 1	30D105G050BA2 RCM15E511J	56289 04062	0180-0108 0140-0047	1 1
CR1-3 CR4	Diode, Si. 200mA 200prv SCR 7.4A 100prv	3 1	C20A	09182 03508	1901-0033 1884-0031	3 1
Q1,2	SS NPN Si.	2	2N3417	03508	1854-0087	2
R1 R2 R3 R4 R5 R6 R7 R8 T1 VR1 VR2	fxd, met. film $10_{n} \pm 1\%1/8W$ fxd, comp $1.3K \pm 5\% 1W$ fxd, met. film $1.21K_{n} \pm 1\% 1/8W$ fxd, met. film $7.5K_{n} \pm 1\% 1/8W$ var. ww $10K_{n} \pm 5\%$ (CROWBAR ADJ.) fxd, ww $1K_{n} \pm 5\%$ 3W fxd, comp $22_{n} \pm 5\% \frac{1}{2}W$ fxd, met. film $510_{n} \pm 1\% \frac{1}{4}W$ Transformer, Pulse Diode, zener $6.19V \pm 5\%$ Diode, zener $2.37V \pm 5\%$	1 1 1 1 1 1 1 1 1 1	Type CEA T-O GB-1325 Type CEA T-O Type CEA T-O 242E1025 EB-2205 Type CEB T-O	07716 01121 07716 07716 09182 56289 01121 07716 09182 09182 09182	0757-0346 0689-1325 0757-0274 0757-0440 2100-1854 0813-0001 0686-2205 0698-5145 5080-7122 1902-0049 1902-3002	1 1 1 1 1 1 1
	MISCELLANEOUS Heat Sink, CR4 Insulator, CR4 Mica Washer, CR4 Cable Clamp Bushing, Potentiometer (R5) Nut, Hex (R5) Label, Information, (CROWBAR ADJUST) Modified Front Panel, Includes Components Printed Circuit Board Assembly, Includes Components	1 1 1 1 1 1 1 1	T4-4	09182 09182 09182 79307 09182 09182 09182 09182 09182	5000-6229 0340-0462 2190-0709 1400-0330 1410-0052 2950-0034 7124-0389 06111-60005 06101-60021	

Table A-1. Replaceable Parts



1) V

Figure A-1. Model 6101A and 6111A Overvoltage Protection Crowbar



oven control circuit to ensure a ripple specification of  $100 \mu V$ peak-to-peak. This change reduces the magnetic radiation induced in the On the schematic, change the oven control circuit as shown below. the following changes: In the replaceable parts table and on the schematic, make In Table A-1, change the HP Part No. of CR4 to 1884-0032. In the parts list make the following changes: In Table 1-1, Load Regulation should read: the current limit to be set to  $110 \pm 2\%$  of rated current. (multiprogrammer remote programming) operation; to allow The above changes have been made to allow for Option 040 R58 is added as follows: Page - 2 -Manual HP Part No. 06111-90001 CR23: Change to HP Part No. 1901-0033 and connect Change the HP Part No. of rubber bumper 0403-0088 to R62: Change to 1k, 5%, 1/2W, HP Part No. 0686-1025. R60: Delete. Change the HP Part No. of S2 to 3100-1911 Front Terminals: Less than 0.001% plus  $700\mu$ V. in shunt with L2 as shown below. 0403-0002 TO 828 -CR3 R62 825 R5B 224 CHANGE 9: ERRATA: **CR23** 70 9,4V REF. Q|6 5

Cover Chassis, Right Side Chassis, Left Side Heat Sink Trim Strip Front Panel, Lettered DESCRIPTION STANDARD 06111-60006 5000-9424 5000-9489 5000-9430 5060-7966 5000-9429 old parts. 06111-60003 **OPTION A85** HP PART NO **OPTION X95** 5060-6124 5000-6061 5000-6199 5000-6093 5000-6094

# ERRATA:

number of extra manuals depends on the number of Option 910's ordered." ordering Option 910 when ordering your instrument. The December 1, 1975, extra manuals may be obtained by Add the following notice to paragraph 1-16: "Effective

is 2140-0244. switch 3101-1248, which is used in those supplies that include Change 4. The HP Part No. of the type A1H lamp Add to the parts list the replacement lamp for illuminated

binding post, HP Part No. 1510-0115 (qty. 1). binding post, HP Part No. 1510-0114 (qty. 2); and red posts listed on page 6-7 of the parts list and add: black with better designed insulation. Delete the two types of The front panel binding posts have been changed to a type

HP Part No. 4040-0414. The blue-gray meter bezel has been replaced by a black one,

Add the following to the parts list: corrugated packing carton. HP Part No. 9211-0615; and two floater pads, 9220-1418.

pericuit by Change 8) to 2100-3252. The resistor has not been changed; just its part no. Change the part number of R58 (added to the current limit has.

## CHANGE 10:

Change zener diode VR2 to 9V, 0.005% T.C., HP Part No. 1902-0785. Note that the old zener diode (1902-0763) should not be used for replacement at any time.

## ERRATA:

In Table 1-1, change the Transient Recovery Time Specification to read as follows:

in output current equal to the current rating of the supply, when the input line voltage is at 115Vac or 230 Vac. within 50mV of the nominal output voltage following a change Less than 50µ sec is required for output voltage recovery to

replace complete fuseholder and nut with new fuseholder parts. Do not replace new parts with If old fuseholder must be replaced for any reason, for fuseholder nut from 2950-0038 to 2110-0569 holder carrier 2100-0565. Change the HP Part No. 1400-0084 to fuseholder body 2100-0564 and fuse 1978, change the HP Part No. for fuseholder from For all instruments delivered on or after July 1,

## Page -3-Manual Changes/Model 6111A Manual HP Part No. 06111-90001

Terminal lug, qty 2 : 0360-0042 Lockwasher, qty 2: 2190- 0079 Nut, qty 1 : 2500-0001 Black binding post, qty 1 ± 1510-0107 Terminal lug, qty 1 ± 0360-1190 Nut, qty 3 : 2950-0144 Red binding post, qty 2 : 1510-0091 hardware to the following: binding posts, control knobs, and associated In the parts list, change the HP Part No. for the CHANGE 11:

Knob, pointer, qty 2:0370-1099 Resistor, var 1k, R67, qty 1:2100-3281 Lockwasher, qty 12: 2190-0016

## CHANGE 12

(as shown), the other breaks the ACC line. two switch sections, one which breaks the AC line In the replaceable parts list, change Switch S1 to the schematic diagram change Switch S1 to show (added in Change 4 ) to HP Part No. 0360-0015. On HP Part No. 3101-2287 and change Terminal Strip

# In the replaceable parts list change the description of S1 to:

ON/OFF. On page 3-1 figure 3-1 change reference point 1 to: LINE SWITCH and change Note 1 to: Push Line switch to turn on supply.

## ERRATA.

schematic change the variable resistors R 14 and R 16 to  $20 k_\Omega ~ \frac{1}{2} w$  HP Part No. 2100-0558. In the replaceable parts list and on the In the replaceable parts list, change Q1 to HP P/N 1854-0221.

## CHANGE 13:

In the replaceable parts list change Terminal Strip (Added in Change 12) to HP Part No. 0360-0011.

## CHANGE 14:

5%, 2W, HP P/N 0812-0066, qty. 1. On page A-3, the Overvoltage Protection Crowbar In Appendix A, Table A-1, add R9 0.33 $\Omega$ , anode of CR4 and +OUT. schematic, add R9 in series with the

CHANGE 15:

add Corrugated Carton, HP P/N 9211-4859. In the replaceable parts list, page 6-7,

ERRATA:

-S terminals on the rear barrier block, and and ground the + output." differential oscilloscope across the +S and a.), "Connect oscilloscope across output terminals shown in figure 5-6" to "connect 9 9 page 5-4, paragraph 5-20, change in step

CHANGE 16:

str the Π the replaceable parts list, page 6-7, add ; following mechanical assembly; Barrier ; p Guard Assembly, HP P/N 5060-2862,qty 1.

### ERRATA:

change Barrier Strip to HP P/N 0360-2185. Τn the replaceable parts list, page 6-7,

3/30/84

### Model 6111A DC Power Supply Manual HP Part No. 06111-90001

Make all corrections in the manual according to errata below, then check the following table for your power supply serial number and enter any listed change(s) in the manual.

SEF	MAKE				
Prefix	Number	CHANGES			
All		Errata			
6E	0172-0211	1			
7A	0212-0656	1, 2			
7A	0657-0681	1, 2, 3			
7A	06820746	1, 2, 3, 4			
1B	0747-0856	1 thru 5			
1140A	0857-0936	1 thru 6			
1140A	0937-1061	1 thru 7			
1140A	1062-1586	1 thru 8			
1606A	1587-2096	1 thru 9			
1835A	2097-2416	1 thru 10			
1930A	2417 - 2456	1 thru 11			
1934A	2457-2906	1 thru 12			
2125A	<b>2907 –</b> 3286	1 thru 13			
2309A 2407A	3287-3446 344 <b>7-</b> 3466	1 thru 14 1 thru 15			
2407A 2411A	3467-up	1 thru 15 1 thru 16			
ERRATA:					

On the schematic at the rear of manual, add jumper between terminals A4 and A5 on rear terminal strip.

In the replaceable parts table, make the following changes: Q7, Q8: Change to 2N2907A, Sprague, 56289, HP Part No. 1853-0099, SS PNP Si.

R64: 3.6 Meg. ±5%, 1/2W, A. B., HP Part No. 0686-3655.

In Paragraph 4-23, third sentence, change "C23" to "CR23."

On Page 5-11, Table 5-8, make the following changes: Zero Volt Programming Accuracy: Change "R6 or R8" to R14.

Programming Current Level: Change "R13" to R16, R17.

### CHANGE 1:

On Page 5-10, Table 5-6, delete references Q2 and Q3 from the first column of table.

In the replaceable parts table, make the following change: Q2. Q3: Change type to 2N3391, HP Part No. 1854-0371, SS NPN Si., G. E. 03508.

On the schematic at the rear of the manual, delete the lead connecting terminal 13, in the main secondary of T1, to the junction between anodes of CR33 and CR34. Terminal 13 should now be open and the anodes of CR33 and CR34 should be left connected to the minus side of filter capacitor C19.

### CHANGE 2:

The serial number prefix of the instrument has been changed from "6E" to "7A".

In the replaceable parts table and on the schematic (if applicable) make the following changes:

- R201-R209: Change tolerance to  $\pm 0.1\%$  and temp. coeff. to  $10ppm/^{\circ}C$ .
- VR1: Change to HP Part No. 1902-1221, 6.2V, ±5%, 250mW zener, 1N821, Transitron 03877.

### CHANGE 3:

In the replaceable parts table and on the schematic diagram, make the following change:

CR13: Change to three discrete diodes, CR5, CR6, and CR7, each HP Part No. 1901-0327 (1N5059).

### CHANGE 4:

In the replaceable parts table, make the following changes: S1: Change to HP Part No. 3101-1248. Terminal Strip: Add, HP Part No. 0360-0401.

### CHANGE 5:

In the replaceable parts table and on the schematic, make the following changes:

Power Transformer T1: Change to HP Part No. 5080-7181. R51: Add,  $20\Omega$ , 1/2W, HP Part No. 0686-2005. R51 is added between C4 and -S terminal on schematic.

### CHANGE 6:

The serial prefix of this unit has been changed to 1140A. This is the only change.

### ERRATA:

Delete references to Option 06 on pages 1-1, 1-2, and 6-7. Option 06 has been superseded by Option 011. When supply is shipped with Option 011, Overvoltage Protection Crowbar installed, Appendix A, Figure A-1 is added to the schematic diagram.

### CHANGE 7:

The standard colors for this instrument are now mint gray (for front and rear panels) and olive gray (for all top, bottom, side, and other external surfaces). Option X95 designates use of the former color scheme of light gray and blue gray. Option A85 designates use of a light gray front panel with olive gray used for all other external surfaces. New part numbers are shown on back.

### CHANGE 8:

In the replaceable parts table and on the schematic, make the following changes:

R13: Change to 562kΩ, 1/8W, HP Part No. 0757-0483.

R24: Change to 5.1kΩ, ±5%, 1/2W, HP Part No. 0686-5125.

R58: Add R58, var, ww, 5kΩ, ±5%, HP Part No. 2100-0741.