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OS260 DUAL TRACE OSCILLOSCOPE

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Introduction

Section 1

The Gould Advance OS260 Oscilloscope is a 15MHz true dual trace instrument incorporating a split beam cathode ray tube with a 10cm x 8cm display.

It features two identical Y input channels with maximum sensitivities of 2mV/cm and bandwidths of d.c. -15MHz. The display modes are:- "CH1 or CH2" single trace; "dual trace" with completely separate amplifiers, giving an unambiguous bright display of fast waveforms; "X-Y" operation in which one input channel is utilised to give X deflection, and "external X" operation in which both Y channels can be used while X deflection is by an external signal.

Sweep speeds from 0.2sec/cm to 0.5μ s/cm are covered in 18 switched ranges with a variable control effective on all ranges. A X10 facility is incorporated, increasing the maximum effective sweep speed to 50ns/cm.

Switch selected trigger sources, a.c. or d.c. coupled, are internal from either channel or external via a front panel socket. A switched bright line trigger gives a trace on the screen in the absence of a trigger signal, or when the trigger level is outside the range of the input signal. A single shot circuit allows one sweep of the timebase after only an arm button is operated.



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Specification

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CRT

Rectangular dual beam tube with 8 x 10cm display Total Accelerating Voltage - 10kV Phosphor type - P31 (P7 to special order) Overlap of beams - 100% Graticule - External illuminated.

VERTICAL DEFLECTION

Two identical channels CH1 and CH2.

Bandwidth D.C. D.C. - 15MHz (3dB down) A.C. 2Hz - 15MHz (3dB down)

Rise Time 23ns

Sensitivity (switched) 5mV/cm to 20V/cm in 12 ranges

Accuracy ±5%

Variable Gain Continuously variable gain control increases sensitivity up to 2.5 times. Gives maximum sensitivity of 2mV/cm

Input Impedance 1MΩ/28pF

Input Coupling A.C. - Gnd - D.C.

Input Protection 400V d.c. + pk a.c.

Display Modes Single trace, CH1 or CH2 True Dual trace, CH1 and CH2

HORIZONTAL DEFLECTION

Timebase 0.5μ s/cm to 0.2s/cm in 18 ranges

Accuracy ±5%

Variable Speed Uncalibrated variable control gives continuous adjustment between ranges

X Expansion X10 pull switch gives fastest speed of 50ns/cm. Expansion accuracy $\pm 5\%$

TRIGGER

Variable trigger level control with option of bright line in the absence of a signal

Source Internal CH1 + or -Internal CH2 + or -External + or -External trigger input impedance 100kΩ/10pF

Trigger Coupling D.C. A.C. A.C. Fast

Sensitivity Internal: 3mm approx. 40Hz – 2MHz 1.5cm approx. at 8Hz and 15MHz (Bright line off) External: 1.5V approx. 40Hz – 2MHz 7.5V approx. at 8Hz and 15MHz (Bright line off)

Single Sweep A single sweep for photographic use is armed by a push button and initiated by the next trigger pulse.

X-Y

Two modes of X-Y operation are provided

 i) X-Y Channel 1 provides X deflection and Channel 2 provides Y deflection X bandwidth d.c. - 500kHz Phase Shift <3° at 20kHz

 ii) X-Y-Y An External X input (rear panel) is displayed against the two Y inputs giving two X-Y traces X bandwidth d.c. - 1.5MHz Phase Shift <3° at 200kHz

External X Sensitivity approx. 0.9V/cm (0.09V/cm with X expansion)

Input Impedance approx. $100k\Omega$

ADDITIONAL FACILITIES

Calibrator 1 Volt ±21/2% square wave at supply frequency

Ramp Output 0 to +10V from $4k\Omega$ approx.

Z mod Input 10V gives visible modulation 70V gives full blanking Input coupling -a.c.Input impedance $-22k\Omega$ approx.

SUPPLY

100V, 115V, 220V, 240V ± 10% 45 - 440Hz Consumption approx. 40VA.

OPERATING TEMPERATURE

 $0 - 50^{\circ}$ C. Full specification is met over the range $15-35^{\circ}$ C

DIMENSIONS and WEIGHT

HEIGHT	180mm
WIDTH	290mm
DEPTH	445mm
WEIGHT	8kg approx

ACCESSORIES SUPPLIED

Handbook Two X10 probes type PB13 One BNC-BNC lead PL43 One BNC-Clips lead PL44 Supply lead PL98

OPTIONAL ACCESSORIES

Probe PB12A passive probe kit with switched X1 and
X10 attenuatorsViewing Hood PN33425Rack Mount Kit PN37714Carrying CasePN32479Front Panel Cover PN34402TrolleysTR4 and TR6

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Operation

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3.1 SUPPLIES

The instrument is normally despatched from the factory with the supply range switch on the rear panel set to the 240V ($\pm 10\%$) range. Check that this is set correctly before connecting to the supply. Note that the correct fuse for the two high voltage ranges, 220V and 240V, is 500mA Slo-Blo (20mm) Advance Part No. 33685. If the 115V range is selected the fuse should be changed to a 1A Slo-Blo Advance Part No. 34790.

NOTE: Do not change the supply range switch with the instrument connected to the supply.

While the instrument does not rely on forced air circulation, it should not be operated with the natural convection cooling restricted, particularly at the rear of the instrument.

The instrument is switched on by turning the INTENSITY control clockwise, the associated neon indicator should light.

3.2 OBTAINING A TRACE

1. To obtain a trace

- (a) Set the CH1 shift control to approximately mid setting.
- (b) Set the CH2 shift control to OFF.
- (c) Set the X shift control to approximately mid setting.
- (d) Set the TRIG level control to normal position, i.e. not pulled out for BRIGHT LINE OFF.
- (e) Set the TIME/CM switch to 5μ s.
- (f) Adjust the INTENSITY control to obtain a display of the required brightness.
- (g) Centralise the display by adjusting the CH1 and X shift control.
- (h) Adjust the FOCUS control to obtain a sharply defined trace.

3.3 Y CHANNEL CONTROLS

- 1. Using one of the coaxial input signal leads (PL43 or PL44) connect a signal to the CH1 and CH2 input socket.
- 2. For
 - (a) Direct connection of the input signal, set the associated input slide switch to DC.
 - (b) Capacitive coupling of the input signal through an internal 0.1μ F 400V capacitor, set the slide switch to AC.

NOTE:

When examining low amplitude a.c. signals superimposed on a high d.c. level, the slide switch should be set to a.c. and the sensitivity of the Y amplifier increased as in (5). To minimise pick up at sensitive settings, it is essential to ensure that the ground lead connection is near to the signal point.

3. To locate the baseline, set the slide switch to GND. At this setting, the input signal is open circuit and the input of the amplifier is switched to ground. 4. To adjust the sensitivity, set the VOLTS/CM switch to a suitable setting. If necessary, adjust the concentric VARIABLE control.

NOTE:

The range of the VARIABLE control give a 2.5:1 increase in gain, $\pm 5\%$ when in the fully clockwise position. Except at the CAL setting, the VARIABLE control is uncalibrated. At the CAL setting, the calibration corresponds to the setting of the VOLTS/CM switch.

- 5. For vertical shift of the trace, adjust the Y shift controls (identified with vertical arrows). To switch off either channel, turn the relevant shift control fully anticlockwise until the switch operates.
- 6. If, under no signal conditions, trace movement is detected when the setting of the VOLTS/CM switch. is altered, reset the BAL preset control. Adjust this control to minimise vertical movement of the CH1 or CH2 traces at the CAL position of the fine gain, when the inputs are grounded and the attenuator switch is moved between the 0.5V/cm position and the 0.2V/cm position. This should be done after a warm up time of, say, 15 minutes or longer and should require only infrequent adjustment thereafter.

3.4 SINGLE TRACE OPERATION

- 1. For single trace operation on CH1, set
 - (a) The CH1 shift control away from the OFF setting.
 - (b) The CH2 shift control to Y2 OFF.
- For single trace operation on the CH2 channel, set

 (a) The CH2 shift control away from the OFF setting.
 - (b) The CH1 shift control to OFF.

3.5 DUAL TRACE OPERATION

In the dual trace condition each channel has its own complete amplifier chain ensuring a correct dual display even under single shot conditions.

For dual trace operation, set both shift controls away from the OFF positions so that two traces appear on the screen.

3.6 TIMEBASE AND X AMPLIFIER

The sweep speed of the internal timebase (i.e. the time scale of the horizontal axis) is determined by the setting of the TIME/CM switch. In addition to selection of the speed of the internal timebase, the switch has two functional settings. These are EXT X and X-Y, on both of these positions the internal timebase is inoperative. The gain of the internal X amplifier may be increased ten times by pulling out the PULL X10 control on the VARIABLE TIME/CM switch. This facility is available at all settings except X-Y of the TIME/CM switch. The facility effectively increases the sweep length from 10cm to 100cm and thus allows close examination of any

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portion of the trace. Any portion of the increased sweep length may be selected for viewing on the display by adjusting the X shift control.

- 1. To adjust the time scale of the horizontal axis:-
 - (a) Set the TIME/CM switch to a suitable setting.
 - (b) If necessary, the sweep can be slowed by adjustment of the concentric VARIABLE control.

NOTE:

The range of the VARIABLE control is approximately 3:1. Except on the CAL setting, the VARIABLE control is uncalibrated. At the CAL setting, the calibration corresponds to the setting of the TIME/CM switch.

- 2. If close examination of any portion of the trace is required, operate the PULL X10 control.
- 3. For horizontal shift of the trace, adjust the X shift control (identified by horizontal arrow). The control has a dual speed function. Initial operation provides coarse shift control, the return adjustment over a limited arc provides fine shift control.

3.7 X-Y MODE

The single trace X-Y display can be obtained via the two main input sockets.

- 1. Set the TIME/CM switch to X-Y.
- 2. Set the CH1 input slide switch to DC or AC.
- 3. Connect the external signal which is to be used for X deflection, to the X (CH1) socket.
- 4. Operate the CH2 channel as for single trace operation and use the CH1 VOLTS/CM switch to control the X deflection.

The CH1 shift control is inoperative.

3.8 EXTERNAL X MODE

For a dual trace X-Y display, the external signal can be applied directly to the X amplifier. Sensitivity is approximately 900mV/cm or 90mV/cm with X10 pulled. Band width is 1.5MHz.

- 1. Set the TIME/CM switch to EXT X.
- 2. Connect the external signal to the EXT X socket at the rear of the instrument.
- 3. Adjust the horizontal position with the X shift control.

3.9 TRIGGER

The timebase may be triggered from the positive or negative slope of the signal selected by the TRIG SELECT switch as follows:-

- (a) CH1 or CH2 signal (irrespective of which beam is displayed).
- (b) An external triggering source connected to the EXT TRIG socket.

The LEVEL control allows selection of the triggering point on the trigger waveform and hence determination of the start of the horizontal trace.

When the LEVEL control is pulled out to select BRIGHT LINE OFF, the timebase will only trigger when the input

signal passes through the selected level. When the LEVEL control is set outside the range of signal or when there is insufficient signal amplitude, the timebase will not run and the screen will remain blank.

The more convenient mode of operation for normal use is with the LEVEL control pushed in, when the timebase will free run in the absence of the correct trigger, and display a bright line or unsynchronised display until the level control is adjusted and/or the amplitude of the input signal is increased. This free run action in the absence of correct trigger, helps in locating the trace. If the timebase is required to free run continuously, the LEVEL control should be set to either end of its rotation. It is expected that the BRIGHT LINE OFF mode will be selected only when the instrument is to be used to display signals at low or high repetition rates.

The TRIG SELECT switch is used in conjunction with the AC/ACF/DC switch. This switch is effective at all settings of the TRIG SELECT switch. The operating facilities available at the three settings are as follows:-

- AC The a.c. coupled wideband mode used for most common trigger signals.
- ACF A filter is switched into circuit to reject low frequencies. High frequency triggering may be effected from complex waveforms such as a high frequency signal with a low frequency ripple content. The 3dB point is approx. 15kHz.
- DC The trigger signal is d.c. coupled enabling the timebase to be triggered from very low frequency waveforms or consistently triggered from variable mark/space waveforms.

The SINGLE SHOT facility is useful for photographic recording of displayed waveforms, or visual study of non-recurring traces.

When SINGLE SHOT is selected the timebase sweep will be inhibited. Pressing the ARM button will prime the trigger circuit and a l.e.d. lamp indicates this stage. The next trigger pulse to be received will initiate a single sweep of the timebase and the lamp will extinguish at completion of the sweep. Further operation of the push button will arm the trigger in the same way for subsequent sweeps.

Summarising, normal triggering control is effected as follows:-

- 1. Set NORMAL/SINGLE SHOT switch to NORMAL.
- 2. Set the TRIG SELECT switch to the required trigger signal and slope.
- 3. Set the ACF/AC/DC switch to the required setting.
- 4. Adjust the LEVEL control so that the trace starts
- at the required point on the waveform.

3.10 ADDITIONAL FACILITIES

(a) Scale

(ь)

Illumination of the graticule is provided. Adjustment of the intensity is by the front panel control. Cal.

This socket provides a d.c. coupled positive-going square wave of $1V \pm 2\%$ amplitude at line frequency for calibration checks. The square wave has a source

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impedance of $1k\Omega$ and a risetime of approximately $20\mu s$ suitable for probe adjustment.

(c) Ramp

This socket at the rear of the instrument provides a d.c. coupled positive-going timing ramp of approximately 10V amplitude generated by the timebase. Source impedance is $18k\Omega$.

(d) Z Mod.

The socket at the rear of the instrument allows an a.c. coupled signal to modulate the brightness. Coupling is by an internal 0.08μ F capacitor into approximately $22k\Omega$. Bandwidth is 100Hz-1MHz.

- 1. Sensitivity is approximately 10V pk-pk for visible modulation at normal brightness.
- 2. Full blanking requires a 70V negative-going pulse.

(e) Passive Probe

A X10 passive probe may be used to extend the voltage range and increase the input impedance of the Y amplifiers. The input resistance of a Y channel is $1M\Omega$ shunted by approximately 28pF. The effective capacity of the input lead must be added to this and the resultant impedance will sometimes load the signal source. Therefore it is advisable to use a 10M X10 probe. This reduces the input capacity and increases the input resistance, whilst reducing the sensitivity. The probe contains a shunt RC network in series with the input, and forms an attenuator with the input RC of the Y channel. To obtain a flat frequency response it is necessary to adjust the capacitance of the probe to match the input capacity of the Y channel as follows:-

- 1. In the Normal Mode, set the Y channel VOLTS/CM switch to 20mV/cm, and the TIME/CM switch to .2ms/cm.
- 2. Connect the probe to the CAL 1V socket.
- 3. Set the adjustable capacitor in the probe tip or termination with a small screwdriver for a level response with no overshoot or undershoot visible on the display.

(f) Camera

A camera may be fitted to the oscilloscope to record waveforms. This facility is particularly useful for the display of transient signals at slow or fast speed timebase setting. Suitable cameras utilising Polaroid or 35mm film may be obtained from D. Shackman & Sons, or Telford Products Ltd. Adaptors are available for attaching the camera to the oscilloscope. Almost any other oscilloscope camera may be used with the OS260 but a suitable adaptor must be obtained and should be discussed with the camera manufacturer.

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4.1 GENERAL

Referring to the block diagram (Fig. 1) signals applied to the CH1 and CH2 input sockets pass into their respective attenuators, preamplifiers and output amplifiers, to the two sets of cathode ray tube Y plates. The VOLTS/CM switch controls the gain of the preamplifier in the necessary 1 - 2 - 5 sequence to cover the ranges from the 5mV/ cm to 0.2V/cm. Above this $a \div 100$ attenuator is introduced before the amplifier.

Each signal is passed also to the trigger switch where selection of CH1 and CH2 or EXT. TRIG. source is made. The selected signal is AC, ACF or DC coupled to the trigger amplifier and then passed to the Schmitt trigger, where it is converted into fast negative-going pulses. The hold-off circuit acts as a gate which is normally open to allow a trigger pulse to set the timebase bistable. The bootstrap ramp generator then begins to generate its linear ramp, which after passing through the X amplifier is applied to the X plates of the cathode ray tube and drives the electron beam linearly across the tube face. A small portion of the signal from the ramp generator is fed back to the hold-off circuit, shutting the gate to prevent any further pulses from the Schmitt trigger from reaching the timebase bistable during the ramp period. When the ramp has reached the necessary maximum level, the timebase bistable is reset, and the ramp is quickly returned to its quiescent state. A time constant in the hold-off circuit now holds the gate closed to inhibit another ramp from being initiated for a short period, until the ramp timing capacitor is discharged fully. Thus

a ramp is generated at a rate set by the TIME/CM switch when the trigger signal reaches a predetermined level. This ramp sweeps the beam across the c.r.t. face, returns and waits for the next trigger point to be reached. The hold-off circuit is also controlled by the single shot circuit when this facility is used. The timebase bistable is connected to a blanking amplifier which drives the grid of the c.r.t. and whose function is to turn on the electron beam during the sweep and blank it off during the fly back and subsequent waiting period.

In the X-Y mode, the signal from the CH1 amplifier, normally used for trigger, is passed via the ramp generator, which acts as a voltage follower, to drive the X plates while the beam switch selects CH2 to drive the Y plates. The beam blanking signal is not used.

External X signal is applied to the ramp generator in that mode in a similar way to X-Y operation.

External Z modulation signal is a.c. coupled to the cathode ray tube cathode.

4.2 Y PREAMPLIFIERS

The attenuator and preamplifier in CH1 are identical to those in CH2. Accordingly only CH1 will be described. Referring to Fig. 4 the input signal is applied to the front panel socket, SKA, and then to the 3 position slide switch, S20, via R2. This switch selects a.c. or d.c. input coupling by including or by-passing C3 in the signal path. On the centre position of the switch, the input socket is disconnected and the input to the amplifier is connected to ground. Input sensitivity selection is performed in two





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stages; the six lowest ranges, 5-200 mV/cm, are obtained by switching the gain of the amplifier as described later. The 0.5-20V/cm ranges are provided by switching in a \div 100 attenuator section before the amplifier and repeating the gain switching. This attenuator is formed by R4 and R201 with C202 to set the h.f. response. C201 is adjusted to maintain the total input capacitance of the highest ranges equal to that of the lower ranges. Diodes, D201 and D202, limit the peak signal voltage at the amplifier input to approximately 8 volts and in conjunction with R7 protect the instrument against damage from inputs of up to 400 volts peak.

The input stage consists of half of a dual field effect transistor, TR201, connected as a source follower, driving the emitter follower, TR203. The collector emitter voltage of TR203 is maintained constant independent of input voltage at one base emitter voltage plus the voltage across R236 by the bootstrap transistor, TR205.

The signal at the emitter of TR203 is applied via the switched resistor network, R40/45, and the common base stage, TR204, to shunt feedback amplifier formed by TR206, R212 and R211. This can be regarded as a "virtual earth" amplifier with R211 as the feedback resistor and the R28 to R34 network as the input resistor. Thus, the overall gain of the stage is selected by S21b to provide the six basic input sensitivities of the instrument. The common base transistor, TR204, is interposed to balance the d.c. offset voltage introduced into the signal path by TR205. The base of TR204 is connected to the source of TR202, which is half of a dual field effect transistor with TR201. TR202 is biased by R209, R210 and the balance potentiometer R203. This is set so that with the input grounded the d.c. potentials of TR204 and TR203 emitters are identical and there is no resultant change of signal level as R40 etc. is switched in. Diode, D206, is fitted to protect TR204 from reverse base-emitter voltages. The output from the collector of TR206 is taken via R215 to the base of TR208, which, together with TR209, forms a long-tailed pair. Transistors, TR212 and TR207, are connected in a similar fashion to TR202 and TR206 and provide a balancing d.c. voltage at the base of TR209.

Movement of the displayed trace will occur when the variable sensitivity control R58, is operated unless the voltages at the emitters of TR208 and TR209 are equal (when the input is grounded) and this balance is set up using potentiometer, R218.

The mutual conductance of the long-tailed pair, TR208 and TR209, is determined in the variable range, by the series of R235, R233 and R58 and in the CAL position by R220. Fixed high frequency compensation is provided by C206, C205 and R234. The collector current of TR208 feeds into a load resistor on the timebase board to provide an internal trigger signal.

The signal voltage developed across R224 is added to the Y shift voltage derived from the potentiometer R52, and is buffered by the emitter follower, TR210, to drive the coaxial cable connection to the CH1 output amplifier. R228 and D209 provide a collector supply for TR210.

R223 is returned to the -20 volt supply through TR211 and provides the correct d.c. potential at the collector of TR209. When the shift control, R52, is turned anticlockwise, S27 closes, cutting off TR211 and effectively shifting the trace completely off the screen. When in the X-Y mode, TR211 is also turned off by -20 volts applied to pin 3 from the timebase assembly.

4.3 Y OUTPUT AMPLIFIERS (Fig. 6)

The two output amplifiers are identical, therefore only CH1 will be described.

The Y signal from the preamplifier is applied at pin 16 to the base of TR311, a common emitter amplifier. The emitter circuit includes potentiometer, R342, (to set the gain of the stage and hence the overall gain of the channel) and high frequency compensating network R345, C322 and C323. The signal from the collector of TR311 is passed through the emitter follower to the base of TR313, which with TR316, TR314 and TR315 forms the output cascode stage. TR313 and TR316, is a long tail pair, which converts the input signal voltage to differential output current; its gain is determined by emitter resistor, R352, with high frequency gain set by networks R351/ C324/C325, R393/C326 and R350/C327. The collector currents of TR313 and TR316 flow into the emitter of the grounded base transistors, TR314 and TR315, to develop the differential output voltage across the load resistors, R347/R357, to drive the c.r.t. deflection plates. Inductors, L1 and L2, and damping resistors, R383 and R384, are included to improve the high frequency response. The base of TR316 is biased by the zener diode, D302, and resistor network, R358 and R359.

4.4 TRIGGER CIRCUITS (Fig. 5)

The trigger signal via pins 25 and 23 from the preamplifier channels is developed across R104 and R105 which are the collector loads of TR228 and TR208 respectively. 1cm of Y deflection gives approximately 25mV across these loads.

R28 and R106 form an approximately 200:1 attenuator to external trigger signals. R107, R108 and R109, R110 are adjusted to offset the standing collector currents which flow in the CH1, CH2 trigger leads, thus maintaining the voltage across R104 and R105 near zero in the absence of Y signals. One of these signals, selected by S13aF, the trigger source and slope switch, is passed to S12, the trigger coupling switch, and from there to the base of TR101. There are three possible signal paths, AC coupled via C18, LF. rej. via C17 with R112 bypassing l.f. signals to ground (fco \simeq 15kHz) or DC coupling.

TR101, acting as an emitter follower, passes the trigger signal to the amplifier pair, TR102 and TR103, the potential derived from the level control, R10, being passed via emitter follower, TR104, to the base of TR103. Thus the amplified trigger signal appearing between the collectors of TR102 and TR103 contains a d.c. component determined by the setting of R10. The gain of this amplifier is determined by R113 and R114, and is approximately 4X. The output signals are passed via the reversing switch,

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S13aB, to the input of amplifier TR105/TR106. The collectors of TR102 and TR103 are connected to the bases of TR105 and TR106 respectively for positive slope, and reversed for negative slope. TR105/106 form a differential amplifier whose output on the collector of TR106, drives the Schmitt trigger circuit, TR107/TR108. The gain of amplifier TR104/106 is approximately 20 and the output d.c. voltage is adjusted with the common emitter resistor, R132.

The function of the trigger circuit, TR107/108, is to generate a fast negative edge at the collector of TR108, independent of the rate of change of the applied signal. The signal appearing on the collector load of TR107/R140, is coupled via the network, R143, C110 and R146, to the base of TR108, whose emitter is connected to the emitter of TR107 and the common emitter resistor, R145. The emitter coupling introduces positive feedback which results in a latching action.

4.5 TIMEBASE BISTABLE AND RAMP GENERATOR (Fig. 5)

The ramp generator comprises TR119, TR120 and TR121 as cascaded emitter follower stages, with bootstrap feedback action provided from the cathode of zener diode, D108. This feedback maintains constant voltage across the VARIABLE TIME control, R11, R172, R183 and the timing resistor selected by the TIME/CM switch. This constant voltage drop, independent of actual voltage level produces a constant current to charge linearly the timing capacitor, also selected by the TIME/CM switch. The VARIABLE TIME control provides fine adjustment of the timing current, and hence sweep time, by varying the feedback voltage applied to the timing resistor.

In the quiescent condition of the timebase bistable, TR114 is on, TR115 is off and clamp transistor, TR116, which shunts the timing capacitor, is saturated. A negative-going pulse from the Schmitt trigger is coupled via C112 and D105 to turn off TR114. TR115 turns on, thus turning off TR116. The clamp is removed, allowing the timing capacitor to charge, producing the linear ramp. As the emitter of TR121 rises, a feedback voltage (via D111, the emitter follower - TR126, D109, R169 and R148) biases off D105 to prevent any further pulses reaching the bistable. Connected to the junction of R148/R169 is the HOLD OFF capacitor which now charges positive. When the ramp reaches its final amplitude (a rise of approximately 10V) feedback from the junction of R184/R185 is applied to the base of TR114, turning it on. The bistable reverts to its initial state allowing TR116 to turn on, rapidly discharging the timing capacitor and returning the ramp to its quiescent level. The hold-off capacitor, which was charged to a positive voltage during the ramp, now discharges through R169 and R186 more slowly than the timing capacitor, until it is caught by D109. Only then is D105 biased for the next trigger pulse to initiate the next sweep.

An output is taken from the ramp generator via R176 to SKE the RAMP OUT socket on the rear panel.

4.6 BRIGHT LINE CIRCUIT (Fig. 5)

When sufficient trigger signal is available, the square wave from the collector of TR108 passes through R144/C113, where restoration by D102 produces a negative going signal with respect to the negative rail. This negative signal on the base of TR111 is integrated by R149/C116 to produce a d.c. bias sufficient to hold off TR112. In this condition the circuit has no effect on timebase operation. However, when the triggering signal falls below the required level, the Schmitt trigger ceases to operate, removing the signal from D102. The voltage on the emitter of TR111 rises to approximately one volt above the negative line, turning on TR112. R147 is now effectively connected between the negative rail and the cathode of D105. It further discharges the hold-off capacitor below the normal quiescent level to a point where D105 conducts, turning TR114 off and initiating a sweep. At the end of the ramp, the charge on the holdoff capacitor is again removed by R147/R169 and another ramp begins. These consecutive sweeps produce the bright line display. When the PULL BRIGHT LINE OFF control is operated, switch S10 closes, effectively shorting the base and emitter of TR112, holding it off; in this condition a ramp is only generated after the arrival of a trigger pulse.

4.7 SINGLE SHOT (Fig. 5)

The CMOS integrated circuit, IC101, provides the gating and set/reset bistable of the single shot circuit and is powered by a +15 volt supply derived from the +20 volt line by R137 and D104.

When S16 is in the NORMAL position, R150 is high forcing pin 11 low, therefore operation of the timebase bistable through R142 is not affected. When S16 is switched from NORMAL to SINGLE SHOT, the base of TR112 is connected to its emitter thus preventing operation of the bright line circuit. Also R150 is connected to OV, allowing the bistable formed by the gates on pins 8-13 to be reset (with pin 11 high) after each sweep of the timebase through the differentiator, C121 and R156. At the end of the current sweep, R142 is at +15V, back biasing D105 and preventing trigger pulses from the Schmitt trigger from triggering the timebase bistable.

C123, (pins 1, 2 of IC101) is charged to +15V through R93, R94 and R157. When the ARM button is pressed, C123 is discharged through R93, causing the output of the gate (pin 3 of IC101) to go high. The bistable is set by this positive transition, through the differentiating circuit, C124 and R150 to pin 13. R142 is now at 0V allowing the timebase bistable to be triggered once by the first trigger pulse through diode, D105.

The l.e.d. indicator, D11, is driven by TR117 through R158. The base of TR117 is switched by the NOR gate either from the bistable, through the input on pin 5, or in the NORMAL mode by S16 through pin 6.

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4.8 X OUTPUT AMPLIFIER (Fig. 5)

The ramp or X signal at the emitter of TR121 passes through R187 to the base of TR122, which with TR125 forms a long tail pair. D101 protects TR122 from reverse base emitter voltages possible when Ext. X is overloaded. Gain switching is carried out in the emitter circuit by selection of one of two resistance paths. In normal operation only R189 is in circuit, with the preset, R191, to set the X1 gain. In timebase mode, the PULL X10 switch, S11, can be operated in order to expand the trace length ten times introducing R188 with preset R191 to set the X10 gain. In the X-Y mode, contacts on the TIME/CM switch in parallel with S11, close to automatically select this higher gain setting. The dual X shift potentiometer, R17, gives coarse and fine control. The two sections are mechanically linked so that one section is directly driven and the other (fine) driven only when the backlash has been taken up. The signals on the collectors of TR122 and TR125 are applied to the differential output amplifier, TR123 and TR124. Signals from the collectors of these two transistors drive the horizontal deflection plates of the c.r.t. High frequency compensation is provided by C122.

4.9 X-Y MODE (Fig. 5)

In this mode signals are applied to both CH1 and CH2 input sockets. CH2 is routed to the Y deflection plates in the normal manner. CH1 is routed through the ramp generator which is now acting as a high impedance unity gain buffer, and into the X output stage. Signals entering CH1 pass through the attenuator and gain switching stage, as described previously. Signal current from TR208 on the Y preamplifier board (otherwise used for trigger), develops a voltage across R101 and R105 in series. This voltage is level shifted by R170/R163 and applied through the diode gate, D107, and S14bF to the base of TR119. In the X-Y mode, the timing resistors and capacitors are switched out of circuit, consequently TR119, TR120 and TR121 merely act as emitter followers which provide buffering between the level shift resistors and the X output amplifier.

When this mode is selected, a contact on the TIME/CM switch, S14aF, connects the cathode of D106 to the negative line. The current drawn through D106 and R153 turns of TR114 and consequently TR116 and removes blanking. (See section 4.13).

4.10 EXTERNAL X MODE (Fig. 5)

The Ext. X signal applied to Sk.G passes through the h f. stopper, R97, and is level shifted by the network, R85/R86/R87, and switched by S14aF to the base of TR119. The signal is thus amplified and applied to the X plates in the same way as in the X-Y mode. Protection from excessive inputs is provided by R87, D112 and D113. In the Ext. X mode TR109 is held non-conducting by R92 which is switched to -20V by S14aF, in all other modes TR109 is held conducting by a positive base bias through

R89 and effectively short circuits the Ext. X signal so that it cannot cause interference to the trace.

4.11 CALIBRATOR (Fig. 6)

The $1V \pm 2\%$ square wave at the CAL 1V socket, SKD, is produced by TR309, on the power supply board. Current for the base of this transistor is supplied via R334 and D318. The anode of D317 is connected to the junction of these components, its cathode being taken to one of the 22V windings. On positive excursions of the winding, D317 is biased off and the current through R334/D318 saturates TR309. During negative excursions D317 conducts, and the current in R334 passes through the transformer winding. In this condition D318 and TR309 are turned off. The result is a square wave at line frequency on the collector of TR309, with amplitude set by adjustment of R328. The CAL signal is attenuated to 1V by R330 and R331.

4.12 POWER SUPPLIES (Fig. 6)

All the power supplies for the instrument are derived from the transformer, T31. Two tapped primary windings are switched by S31 to allow for three supply voltage ranges and fuse, FS31, provides fault protection. The supply indicator neon, V32, is supplied via limiting resistor, R32, from the 115 volt tap on the transformer.

For the low voltage supplies two separate secondary windings supply bridge rectifiers, BR31 and BR32, mounted on the transformer and provide unregulated supplies of $\pm 200V$, $\pm 26V$ and $\pm 26V$ across the reservoir capacitors, C33B, C31 and C32 respectively. The $\pm 200V$ supply is further smoothed by R31 and C33A. The $\pm 26V$ and $\pm 26V$ supplies are fed to high performance integrated circuit regulators, IC301 and IC302 respectively, to provide stabilised lines of $\pm 20V$ and $\pm 20V$. These devices contain all the circuitry necessary for a conventional series regulator, together with current limiting and thermal shutdown facilities to protect the device against overloads arising from short circuits or component failures. Note that the $\pm 20V$ line is in fact provided by a 15V regulator, IC302, in conjunction with a zener diode, D203.

The two remaining secondary windings are associated with the cathode ray tube supplies. The 6.3V winding feeds the c.r.t. heater. The 1400V winding provides the -1500V and the +8.5kV supplies.

The 1500V supply is derived by the diode, D301, feeding the reservoir capacitors, C301, C302, C303 and C304. The voltage is smoothed by R305, C305, C306, C307 and C308, and applied to the c.r.t. network.

The +8.5kV c.r.t. anode supply is provided by quadrupling the 1800V a.c. supply in a separate encapsulated multiplier module.

Stabilisation of both e.h.t. lines against supply voltage variations is achieved as follows:-

One end of the 1800V winding feeds the rectifier diodes in the normal manner, the other end is connected to ground via a bridge rectifier, BR301. The alternating

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current in the winding passes through BR301, TR307, R324, TR308 and R349 as direct current which develops a d.c. voltage across C318 and C319. Overvoltage protection of these components is afforded by the chain of zener diodes, D314, D315 and D316. This d.c. voltage, controlled by the conduction of the cascode connected pair of transistors, TR307 and TR308, is effectively subtracted from the peak voltage available at the 'hot' end of the winding; thus by varying the conduction of TR308, the rectified high voltage supplies can be controlled.

The stabilising circuit operates at the negative peak of the waveform from the e.h.t. winding, when current flows from the low side of the winding through pin 42 and the bridge rectifier, BR301, to OV. Conduction in the bridge holds the negative side of C316, C317 etc. near OV. The voltage drops across R349 and R320 are small. Consequently for balanced working conditions potentials at the base of TR308, the emitter of TR306 and hence the base of TR306 must also be near to 0V. In fact the diode junction drops cancel in TR306, D313, TR308 and BR301. If the feedback current from the -1500V supply through R318 is not exactly cancelled by that defined by R315 and the preset control R314 from the +20V supply, the base potential of TR306 will differ from 0V. The conduction of TR308 and hence TR307 will vary the voltage across C318 and C319 to correct the -1500V supply level.

At this same peak of the supply cycle, current from the e.h.t. multiplier, via R903, flows in D312 defining the base potential of TR307 just above +20V so that TR307 operates in cascode from TR308. At other points of the cycle D313 and D312 are reverse biased and capacitors, C316, C317 and C318, retain the relative operating potentials of TR307 and TR308. When the positive peak output from the e.h.t. winding is reached, the same correction voltage across C318 and C319 is subtracted and first order stabilisation is applied to the +8.5kV p.d.a. supply. A small correction current from the unstabilised -26V supply is applied to the base of TR306 to null any remaining variation of e.h.t. supplies with supply variations.

Graticule illumination is provided by two bulbs which are supplied through R301 from the emitter follower, TR301. The lamp voltage is controlled by the front panel control, R39. Collector supply for TR301 is full wave rectified by separate diodes, D305 and D306.

4.13 BLANKING (Fig. 6)

The blanking circuit is powered by the voltage drop across the zener diode, D307, which is in series with the negative 1500V c.r.t. gun supply. The grid of the c.r.t. is returned to the junction of the collectors of two complementary transistors, TR303 and TR305. When the timebase is triggered, TR114 conducts turning off TR110 (timebase bistable, see Section 4.5) and a negative edge is applied via pin 30 to the two capacitors, C314 and C315. This turns off TR303 and turns on TR305 thus reducing the negative bias on the c.r.t. grid and increasing the intensity. Feedback through R313 turns off TR304 causing its collector to go negative which turns on TR305 harder, through D309. This speeds up the pulse on the c.r.t. grid and maintains the circuit in this condition until the blanking pulse from the timebase goes positive at the end of the sweep, when the circuit reverts to its blanked condition with TR303 on and TR305 off. The time constant of R303/C346 ensures that when the instrument is switched on it is in the bright trace condition. Blanking is not effective in the Ext. X or X-Y modes. External Z modulation is a.c. coupled through C320 and applied directly to the cathode of the c.r.t.

4.14 TUBE NETWORKS (Fig. 6)

Intensity is controlled by R38 and the range of this control by R319. As the cathode supply is stabilised by feedback through R318, adjusting the intensity changes the negative supply at the cathode of D301.

Focus and focus range is controlled by R34 and R325. With a split beam tube it is necessary when changing focus, to correct a small Y shift which occurs due to the construction of the c.r.t. The focus control is a twin gang potentiometer, the first section directly control the potential on the focus electrode and the second section changes the base and emitter voltages of the emitter follower, TR310. The required Y shift compensation is applied. R337 to CH1 and, in antiphase, through R381 to CH2. R323 causes the focus voltage to change slightly with changes in the intensity control, R38.

R307 adjusts the potential on the GEOM electrode and R311, buffered by the emitter follower, TR302, provides adjustment of the ASTIG electrode.

Trace rotation is adjustable by varying the current through coil, L31, by R306.

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5.1 GENERAL

Top and bottom views of the OS260 are shown in Figs. 2 and 3 respectively. Access to all preset components is possible when the upper and lower covers and the rear blow moulding have been removed. The top and bottom covers are removed by releasing the four latch fasteners by turning these one half turn, and the rear blow moulding by removing six screws.

If during fault finding a component needs replacing, it may be cut from the printed circuit board as close as possible to the component, leaving the wires protruding through to the component side of the board. The new component can then be soldered into position by attaching it to these protruding wires. This protects the copper track from damage.

If a fault on a printed circuit board cannot be cleared, it is recommended that the instrument is returned to the manufacturer for repair. When faults have been cleared it is recommended that the test procedure be implemented to ensure that the instrument confirms to the specification.

5.1.1 Supply Voltage Selection

Selection of 115, 220 or 240V operation is by the three position slide switch, S31, located on the rear panel of the instrument. Note that the POWER ON switch should be turned off before S31 is operated. 100 volt operation is available as an alternative to 115V by changing connections to the transformer primary. BEFORE CHANGES ARE MADE DISCONNECT THE INSTRUMENT FROM THE SUPPLY. Remove the instrument top cover, locate the supply transformer, T31, Fig. 2, and unsolder the two pink wires (on the 115V tap) and resolder onto the adjacent 100V tap. Unsolder the orange wire (on the other 115V tap) and resolder onto the root tap, located between the yellow and black wires. The voltage selection switch, S31, now has its voltages changed as follows:-

the 115V position becomes 100V the 220V position becomes 205V the 240V position becomes 225V.

5.1.2 Fuse Replacement

SWITCH OFF INSTRUMENT POWER SWITCH BEFORE CHANGING FUSE.

The supply line fuse, FS31, is mounted on the rear panel beneath the supply plug. The rating is 500mA Slo Blo (Pt. No. 33685) for 190-260 volt operation, and 1A Slo Blo (Pt. No. 34790) for 95-130 volt operation.

5.2 REMOVAL OF PRINTED CIRCUIT ASSEMBLIES

Removal procedures for each of the printed circuit board assemblies are outlined below. However, almost all the components in the instrument, with the exception of those in the early stages of the Y amplifiers, are accessible without recourse to board removal.

- 5.2.1 Y Preamplifier Sub-Assembly
- (a) Remove the three sockets from the rear of the assembly. Remove socket from pin 3 (green wire).
- (b) Remove two sockets, on coaxial cables, from the power supply board.
- (c) Remove the screw securing the rear of the assembly to the centre screen. Remove screw through side frame, at rear of assembly.
- (d) Remove all knobs from the front panel controls. (Prise off top covers of the knobs and loosen the collet securing nuts revealed.)
- (e) Remove fixing nuts from the attenuator switches.
- (f) The assembly can now be removed from the instrument.

5.2.2 Timebase and X Amplifier Sub-Assembly

- (a) Remove power socket, twin feeder socket, socket on pin 46, 47, single sockets on pin 11 (brown wire), and pin 8 (green wire).
- (b) Remove two sockets on coaxial cables, from Y preamplifier assembly.
- (c) Remove socket from pin 14 (yellow wire).
- (d) Remove four screws fixing the p.c.b. to instrument.
- (e) Remove all knobs from front panel controls. (Prise off top covers of the knobs and loosen the collet securing nuts revealed.)
- (f) Remove fixing nuts from the TIME/CM switch and trigger switch.
- (g) The assembly can now be removed from the instrument.

5.2.3 Power Supply and Y Output Printed Circuit Board

- (a) Remove socket from pin 14 on timebase p.c.b. (yellow wire).
- (b) Remove single wires from pin 29 (white wire), pin 50 (orange wire), pin 31 (brown wire), pin 32 (red wire), pin 33 (orange wire), pin 34 (yellow wire).
- (c) Remove the eight remaining socket assemblies.
- (d) Remove rear blow moulding from instrument.
- (e) Remove four screws fixing the p.c.b. to the side frame.
- (f) Remove three screws fixing heat sink to rear panel of the instrument.
- (g) The assembly can now be removed from the instrument.

5.2.4 C.R.T. Replacement

- (a) Remove rear moulding from the instrument.
- (b) Remove the tube base connector.
- (c) Remove the p.d.a. cap.
- (d) Remove the socket from pins 1 and 2 on the power supply p.c.b. (pink wires).
- (e) Remove the screw through the rear tube shield support bracket.
- (f) Remove two screws to separate the rear support bracket.
- (g) Slide the c.r.t. assembly rearwards and lift the front clear of the framework and remove forwards.

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5.3 FAULT FINDING

Before any fault location is attempted, it is suggested that all supply line voltages are checked with respect to 0V. These are given in Table 1, refer to Fig. 3.

Table 1

LINE	MEASURED VOLTAGE	MEASU RE- MENT POINT
+20V 20V +190V	+19 to +21V -19 to -21V +180 to +200V	Plug A on power board
-1450V	-1390 to -1550V	End of C320
PDA	+8000V	adjacent to D317 PDA cap

NOTE: The power supply input voltage should be approximately at the centre of the range for which the transformer taps are connected.

Table 2, indicating voltages at various circuit locations, may be used as a general guide and servicing aid. The front panel controls should be set as follows:

NORMAL/SINGLE SHOT switch to NORMAL INTENSITY, X SHIFT, CH2 SHIFT all at mid position CH1 SHIFT to OFF position CH1 and CH2 INPUT switches to ground position TRIG SELECT to CH1 +ve ACF, AC, DC to A.C. LEVEL to mid position, BRIGHT LINE on TIME/CM to X-Y

Adjust X and CH2 shift controls to bring spot to centre of screen.

Table 2 Circuit Voltages

Y – Preamplifier Sub-Assembly LOCATION	TYPICAL VOLTAGES
TR203, 204, 223, 224 Base TR203, 223 Collector TR206, 207, 226, 227 Collector	+1.3V +1.8V +7.5V
TR208, 228 Collector	+3.0V
Timebase Sub-Assembly	
LOCATION	TYPICAL VOLTAGES
TR101 Base	0 V
TR102, 103 Collector	+8.2V
TR102, 103 Emitter	+7.5V
TR106 Collector	+14V
TR107 Collector	+17V
TR108 Base	+13V
TR108 Collector	+20V
TR112 Collector	-20V
IC101 Pin 11	0V
TR115 Collector	+0.2V
TR121 Emitter	+4.2V
TR123, 124 Emitter	-6.8V
TR123, 124 Collector	+130V

Power Supply and Y Output	
LOCATION	TYPICAL VOLTAGES
TR306 Emitter	+1.8V
TR311 Collector	+1.3V
TR317 Collector	+4V
TR316, 322 Base	+8.5V
TR320, 321 Collector	+130V
TR314 Collector	+175V
TR315 Collector	+90V

5.4 CALIBRATION PROCEDURE

Calibration adjustments should be made only after a 15 minute warm up period following switch on. Refer to Figs. 2 and 3 for component locations.

- 5.4.1 Test Equipment
- (a) Multirange Test Meter, 0-2.5kV with sensitivity $> 20k\Omega/V$.
- (b) Variable Autotransformer output voltage 95-260V at 1A.
- (c) Sine/Square wave signal generator covering the range 10Hz-100kHz amplitude 20mV-5V.
- (d) Source of Time and Voltage Calibration signals, to cover the range 0.1μs-0.5s and 25mV-100V.
- (e) Squarewave Generator to provide 500kHz flat top square wave with amplitude adjustable between 25mV and 1 volt. Risetime to be less than 5ns.
- (f) Constant amplitude r.f. sinewave generator to cover the range 500kHz to 15MHz with a 50kHz reference frequency. Output amplitude 25mV to 5 volts pk-pk when terminated with 50Ω load. Amplitude accuracy over the frequency range to be within $\pm 3\%$.
- (g) 50Ω BNC through-termination.
- 5.4.2 Power Supply Voltages (Fig. 3)
- (a) Set the INTENSITY control to minimum.
- (b) Set the SUPPLY VOLTAGE switch on the rear panel to suit the available supply. Using the autotransformer, set the supply to the instrument to within ±1% of the selected nominal voltage.
- (c) Check that the POWER neon, V32, is lit and that the SCALE control varies the graticule illumination.
- (d) With the voltage selector switch set for 240V operation, connect the instrument to the a.c. supply via a variable autotransformer and set the voltage to 240V ± 1%. If the voltage selector switch is not set for 240V operation the tests should be carried out with the supply within 1% of the nominal voltage selected.

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(e) Adjust R314 (SET EHT) to give 240V d.c. between the +ve end of C318 and the -ve end of C319. Check the voltages listed in Table 1 are within the limits specified while the supply voltage is varied from 222-260 volts.

5.4.3 C.R.T. Controls (Fig. 3)

(a) Set the front panel controls as follows:-NORMAL/SINGLE SHOT switch to NORMAL

TIME/CM switch to X-Y INTENSITY to mid position FOCUS to mid position X SHIFT to mid position CH1 and CH2 VOLTS/CM switch to 20V/cm

Adjust X and CH2 shift to centre a spot on the screen. Adjust R311 (ASTIG) together with the INTENSITY and R325 (FOCUS RANGE) controls to obtain a sharp round spot.

- (b) Switch TIME/CM switch to 1ms/cm. Remove rear instrument cover (six screws), loosen bolt in magnet clamp round neck of the c.r.t. Rotate the ceramic magnet with a screwdriver, inserted into the square centre hole, until the intensity of the two traces is equal; reduce INTENSITY control and ensure that the equality holds down to low intensity. Repeat adjustment of FOCUS RANGE and ASTIG controls as described above.
- (c) Switch TIME/CM switch to 1ms/cm, turn X shift clockwise until the start of the trace is visible on the screen. Switch NORMAL/SINGLE SHOT switch to SINGLE SHOT. Turn front panel INTENSITY control fully clockwise. Turn R319 (INTENSITY RANGE) clockwise until the spot is visible and then turn anticlockwise until the spot is just extinguished.
- (d) Set the TIME/CM to 1ms/cm, and BRIGHT LINE on. Adjust R308 (TRACE ROTATE) to bring the trace exactly parallel with the horizontal axis of the graticule.
- (e) Set the CH2 shift to off, CH1 input switch to a.c., trigger selector to CH1 and apply to CH1 input socket a 20kHz sine wave, set to give approximately 8cm of Y deflection. Set the TIME/CM switch to 1ms/cm and adjust TRIGGER LEVEL control so that a raster is displayed. Adjust R307 (GEOM) for a compromise between horizontal and vertical pin cushion and barrel distortion. Reset R325 (FOCUS RANGE) and if necessary re-adjust R311 (ASTIG).
- 5.4.4 Y Calibration (Fig. 2)
- (a) With the input coupling switch in the GND position, and CH2 off, obtain a trace on CH1 by operating the CH1 shift control. Adjust the front panel BALance control, R203, so that there is no trace shift when changing from the 0.2V/cm range to the 0.5V/cm range. Adjust R218 (VAR. GAIN BAL) on the Y preamplifier board so that there is no shift when the CH1 variable sensitivity control is operated.
- (b) Repeat the preceding step for CH2 using R253 (BAL) and R268 (VAR. GAIN BAL).
- (c) Turn CH2 off and set CH1 shift control to the centre of its range. If the trace is more than ±3cm from the centre of the screen change the value of R392 to rectify this.
- (d) Repeat the preceding step for CH2, changing the value of R393 if necessary.
- (e) Apply a sinewave signal to each channel in turn and set the amplitude for 8cm pk-pk display. Check that the traces can be shifted completely off the

screen in each direction.

(f) Set both CH1 and CH2 attenuators to 0.2V/cm, both input switches to d.c., and the TIME/CM switch to 5ms/cm. Apply 1V from a calibrator to CH1, trigger on CH1, and adjust R342 (CH1 GAIN) for a 5cm display. Apply the same signal to CH2 input, trigger on CH2, and adjust R364 (CH2 GAIN) for a 5cm display.

5.4.5 Attenuator Compensation (Fig. 3)

Capacitors, C2 and C22, are selected such that the input capacitance is approximately 28pF.

To set the attenuator compensation, set the CH1 VOLTS/ CM switch to 0.5, the input coupling to d.c. and the TIME/CM to 0.5ms/cm. Connect a low impedance 3V, 1kHz square wave signal to the input and adjust C202 for a square top to the display. Repeat for CH2, adjusting C222.

To equalise the input capacitance on all ranges connect a 1kHz square wave signal either via a 10:1 probe or a $1M\Omega$ series resistor connected in parallel with a 10 to 40pF trimmer capacitor, mounted close to the input socket. Set the input amplitude for approximately 6cm of display and adjust the probe compensation or the trimmer for a square top to the display. Set the CH1 VOLTS/CM switch to 0.5 and adjust C201 to regain the flat top to the display. Repeat for CH2 adjusting C221.

5.4.6 Pulse Response and Bandwidth (Fig. 3)

Switch the CH1 attenuator to 5mV/cm and set TIME/CM to $1\mu s/cm$. Apply a 500kHz fast risetime square wave signal to CH1 input using a 50Ω termination at the input socket to prevent cable reflections. Adjust output from the generator to give a 6cm display. Adjust C324 to obtain a flat level top towards the leading edge of the square wave, and adjust C323 and R345 to obtain a square corner. Repeat for CH2 using C335, C334 and R367 respectively. Check that the pulse response is square on all ranges between 5mV/cm and 0.2V/cm, adjusting the generator for approximately 6cm amplitude on each range. Allow a maximum of 4% over or under shoot.

Check bandwidth by applying a 50kHz sine wave to CH1 input and adjust the generator to give a 6cm display. Increase the frequency until the amplitude drops to 4.2cm, this frequency should be greater than 15MHz. If bandwidth is lower than 15MHz the capacitor, C328, may be increased and the pulse response re-optimised as above. Repeat bandwidth check on CH2 adjusting the value of C340 if necessary.

- 5.4.7 Timebase Calibration (Fig. 2)
- (a) Set TIME/CM control to 1ms/cm and pull the PULL X10 XAMP control. Apply 1ms time markers to CH1, adjusting Y sensitivity to give approximately 3cm amplitude, triggering with bright line off (TRIGGER LEVEL control pulled out). Adjust R190 (X10 GAIN) on the timebase board for exactly 10cm between markers.
- (b) Set PULL X10 XAMP (pushed in) and adjust R191 (X1 GAIN) on timebase board for 1cm between

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markers.

- (c) With 1ms markers still applied, vary the supply voltage to the instrument by ±10% from the nominal value and check that there is less than ±1% change in timebase calibration.
- (d) Set TIME/CM to 10µs/cm and apply 10µs markers. Adjust the trimmer, C10, (SET 1µs/cm) on the timebase range switch for 1cm between markers.
- (e) With the PULL X10 XAMP control at X1, check all the timebase ranges from 1μ s/cm to 0.5s/cm with the appropriate markers, to within $\pm 5\%$.
- (f) Check that the trace length is greater than 11cm on all timebase ranges.
- (g) Check that the variable time control reduces the speed by greater than 2.5:1.

5.4.8 Trigger Balance (Fig. 2)

- (a) With the NORMAL/SINGLE SHOT switch in the NORMAL position and no trigger signals applied, check that the timebase free runs with the BRIGHT LINE on and does not free run with the BRIGHT LINE off.
- (b) Apply a 1kHz sine wave to CH1 and adjust amplitude to give approximately 6cm display. Adjust R132 (TRIG BAL) on the timebase board so that there is no vertical shift in the trigger point when moving the trigger source control between CH1 + and -. Check that the TRIGGER LEVEL is midway through its range when the timebase is triggering at the zero crossing point in the displayed waveform.
- (c) With the signal applied to CH1 input, adjust R108 (CH1 DC BAL) on the timebase board so that there is no change in trigger point when the trigger coupling switch is moved from AC to DC. Repeat this adjustment with R116 (CH2 DC BAL) for CH2.
- (d) Check that the ACF position of the trigger coupling switch is functional.
- (e) Apply a 1kHz square wave input signal and reduce the amplitude to 3mm. Check that stable triggering can be obtained on both + and - slope positions for both input channels.
- (f) Set the trigger source selector to EXT and apply a 1.5 volt, 1kHz square wave to the EXT TRIG input. Check that stable triggering can be obtained on both + and - slope settings with the BRIGHT LINE either on or off.
- (g) Apply a 15MHz sine wave to CH1 and adjust amplitude for 1.5cm of display on the 20mV/cm attenuator range. Check that steady triggering can be

obtained with the BRIGHT LINE switched off. Switch the attenuator to 0.1V/cm to give 2.5mm display and reduce the input frequency to 2MHz. Check for stable triggering and repeat both tests on CH2.

(h) Switch NORMAL/SINGLE SHOT to SINGLE SHOT and check for correct operation of the single shot facility. Press the ARM button and check that the l.e.d. lamp lights. Apply a trigger signal and check that a single trace occurs after which the lamp extinguishes.

5.4.9 Internal Calibrator (Fig. 3)

Set CH1 attenuator to .2V/cm. Apply a $1V \pm 1\%$ square wave calibration signal (approximately 50Hz) to CH1 input and note the exact deflection. Remove the 1V square wave and apply the internal calibrator to CH1 input. Adjust R328 (SET CAL) to give the deflection previously noted.

5.4.10 X-Y Operation

- (a) Apply a 1kHz sine wave signal to the CH2 input socket and set TIME/CM to 1ms. Adjust the generator to give 5cm amplitude and apply this signal also to the CH1 input. Set the TIME/CM switch to X-Y and position the trace with the X shift control so that the X deflection is equal about the vertical centre line. Increase the frequency gradually to 20kHz and ensure that, if the 45° line gradually changes to an ellipse, the spacing of the lines on the vertical axis does not exceed 2.5mm over the frequency range.
- (b) Set the CH2 input switch to GROUND and apply a 50kHz sine wave to the X(CH1) input socket. Adjust the amplitude to give a horizontal line 10cm long. Increase frequency until trace reduces to 7cm and ensure that this frequency is greater than 500kHz.

5.4.11 External X Operation

Apply a 50kHz sine wave to the EXT X socket with the TIME/CM switch set to EXT X and the PULL X10 XAMP control pulled. Adjust the amplitude to give 10cm deflection. Increase frequency until the trace reduces to 7cm and ensure that this frequency is greater than 1.5MHz.

5.4.12 Z Modulation

Set the CH1 attenuator to 1V/cm and apply both to the CH1 input and to the Z MOD socket at 10V 1kHz square wave. Check that blanking occurs at normal brilliance levels.

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ABBREVIATIONS USED FOR COMPONENT DESCRIPTIONS

RESISTORS				
CC	Carbon Composition	$\frac{1}{2}W$	10%	unless otherwise stated
CF	Carbon Film	¹ / ₈ ₩	5%	unless otherwise stated
MO	Metal Oxide	$\frac{1}{2}W$	2%	unless otherwise stated
MF	Metal Film	ΞΨ	1%	unless otherwise stated
WW	Wire Wound	6W	5%	unless otherwise stated
CP	Control Potentiometer			
PCP	Preset Potentiometer Type	e MPD, PO	20%	unless otherwise stated
MG	Metal Glaze	$\frac{1}{2}W$	0.5%	unless otherwise stated
CAPACITORS				
CE (1)	Ceramic		+ 80% 25%	
CE(2)	Ceramic	500V	± 10%	unless otherwise stated
SM	Silver Mica	350V		
PF	Plastic Film and Foil		± 10%	unless otherwise stated
PS	Polystyrene			
PE	Polyester		± 10%	unless otherwise stated
PC	Polycarbonate			
Е	Electrolytic (aluminium)		+ 50%	
_			- 10%	
Т	Tantalum		+ 50%	
-			- 10%	

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Fig. 2 Top view

Section 6



Fig. 3 Bottom view

'Y' PRE-AMP



Section 6

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	E-400								
Ref	Value	Description	Toi %±	Part No	Ref	Value	Description	To/ % ±	Part No
RESIST	rors								
R201	10k1	MF		26338	R262	2k7	CF		28726
R202	470	CF		21797	R263	2k7	ĊF		28726
R203	22k	СР	A	4/32894	R264	1k8	MO		26732
R204	6k8	ĊF	1	21807	R265	47	CF		28714
R205	10k	CF		21807	R265	47	CF		28714
R206	3k3	CF		21803	R267	10k	MO		
R200	10k	MO				470			28800
R207	6k8	CF		28800	R268		PCP		37419
R208				21807	R269	2k7	CF		28726
	100	CF		21794	R270	180	MO		26744
R210	47k	CF		21815	R271	2k7	CF		28726
R211	1k8	MO		26732	R272	100	CF		21794
R212	2k7	CF		28726	R273	5k6	CF		21806
R213	2k7	CF		28726	R274	470	CF		21797
R214	1k8	MO		26732	R275	12k	CF		21810
R215	47	CF		28714	R276	1k5	CF	½W	/ 18552
R216	47	CF		28714	R277	47	CF		28714
R217	10k	МО		28800	R278	1k2	CF	½W	
R218	470	РСР		37419	R279	10	CF		21793
R219	2k7	CF		28726	R280	10	CF		21793
R220	180	MO		26744	R281	150	CF		28719
R221	2 k 7	CF		28726	R282	180k	CF	A.O.T.	21822
R222	100	CF		21794	R283	270	CF	A.U.1.	21822
R223	5k6	CF		21794	R283	470	CF		28720
R224	470	CF		21797	R285	62			28778
R225	12k	CF		21797	R285 R286		MO		
R225	1k5	CF		18552		180	CF		21795
R220 R227	47	CF			R287	150	CF		28719
R228	1k2	CF	1/11/	28714	~ ~ ~ ~ ~				
R228 R229	10	CF	½W		CAPACI		TOULTD		05750
R229 R230	10			21793	C201	6pF	TRIMMER		25750
R230		CF		21793	C202	6pF	TRIMMER		25750
	150	CF		28719	C203	.01µF	CE(2)	250V	22395
R232	180k	CF	A.O.T.	21822	C204	.01µF	CE(2)	250V	22395
R233	270	CF		28720	C205	15pF	CE(2)		22366
R234	470	CF		21797	C206		FITTED IF R	LEQUIRED	
R235	62	MO		28778	C207	0.1µF	CE(2)		36709
R236	180	CF		21795	C208	.01µF	CE(2)	250V	22395
R237	150	CF		28719	C209	3.0pF	S/M		34225
R238	1k5	CF		21801	C221	6pF	TRIMMER		25750
R239	1k5	CF		21801	C222	6pF	TRIMMER		25750
R240	4k7	CF		21805	C223	.01µF	CE(2)	250V	22395
R241	4k7	CF		21805	C224	.01µF	CE(2)	250V	22395
R242	27k	CF		21813	C225	15pF	CE(2)		22366
R243	56k	CF		28729	C226		FITTED IF R	EOUIRED	
R244	5k6	CF		21806	C227	0.1µF	CE(2)		10647
		01		21000				2501	19647
R251	10k1	MF		26338	C228	.01µF	CE(2)	250V	22395
R251	470	CF			C229	3.9pF	S/M		34225
R252				21797	C240	.01µF	CE(2)	250V	22395
	22k	CP	A	4/32894	C241	.01µF	CE(2)	250V	22395
R254	6k8	CF		21807					
R255	10k	· CF		21809					
R256	3k3	CF		21803	TRANSI	STORS			
R257	10k	MO		28800	TR201		AE31	Dual F.E.T.	436243
R258	6k8	CF		21807	TR202			Juai 1.15.1.	AJU24J
R259	100	CF .		21794	TR203		ZTX313 Mata	had Dat-	121251
R260	47k	CF		21815	TR204		ZTX313 ZTX313 Mate	neu rair	A31254
R261	1k8	MO		26732	TR205		2N3906		21533

Ref	Description	Part No
1	Frame Front	30575
2	Frame Rear	37502
3	Bracket Support Side	34460
4	Bracket Support Top	34462
5	Trim Side	29297
6	Insert Threaded 4–40	29905
7	Panel Front (Gould)	38762
8	Panel Front Inner (Timebase)	36660
9	Panel Front Inner (Y Amp)	36661
10	Terminal Earth	32310
11	Escutcheon	36351
12	Graticule	36048
13	Filter (Blue)	33749
14	Moulding Tube Support Assy.	36238
15	Foot Moulded	36329
16	Plate, P.C.B. Support	37071
17	Screen	37073
18	Bracket Support, Transformer	37051
19	E.H.T. Assy.	37176
20	Panel Rear	37070
21	Cover Rear	37076
22 23	Handle Assy.	36656
23 24	Title Strip	37122
24	Spindle Spring	36358
26	Block Indexing	29206
27	Circlip	30578
28	Screw 6-32 x $\frac{3}{8}$ Pan Head	10016
29	Screw M3 x 8 C'sk Head	22816 33069
30	Button Handle	36681
31	Plate Support E.H.T.	37075
32	Holder Fuse	32210
33	Fuse 1A (115V Supply)	34790
34	Cover Top	37088
35	Cover Bottom	37089
36	Latch	37864
37	'O' Ring	37915
38	Screw 4-40 x $\frac{5}{16}$ Pan Head T.T.	22695
39	Screw 4–40 x 🖁 Pan Head T.T.	22696
40	Screw 4–40 x $\frac{1}{4}$ C'sk Head	22780
41	Screw 4—40 x 🚦 Pan Head	22844
42	Screw 6–32 x $\frac{3}{8}$ C'sk Head	22772
43	Washer 4–40	1200
44	Washer 4–40 Wavey	4591
45	Washer 6–32 Wavey	4590



Section 6

Ref	Value	Description	Tol %±	Part No	Ref	Value	Description	Tol %±	Part No
TR206		ZTX313			DIODES	5			
TR207		ZTX313 ZTX313 Mate	hed Pair	A31254	D201		IN3595		29330
TR208		2N3906		21533	D202		IN3595		29330
TR209		2N3906		21533	D203		IN4148		23802
TR210		2N3906		21533					
TR212		BC182B		33205	D206		IN4148		23802
TR212		ZTX313 Matc	hed Pair	A31254	D207				
		with	TR232		D208	3V3	ZENER		33923
					D209		IN4148		23802
TR221		AE31	Dual F.E.T.	A36243					
TR222			Dual F.E.T.	A30243	D221		IN3595		29330
TR223		ZTX313 Mate	had Pair	A31254	D222		IN3595		29330
TR224		ZTX313 ZTX313 Matc			D223		IN4148		23802
TR225		2N3906		21533	D224				
TR226		ZTX313 ZTX313 Mate	hèd Pair	A31254	D225				
TR227			nou i un		D226		IN4148		23802
TR228		2N3906		21533	D227				
TR229		2N3906		21553	D228	3V3	ZENER		33923
TR230		2N3906		21533	D229		IN4148		23802
TR231		77321214			D a 46		~~\ T>		
TR232		ZTX313 Matc		A31254	D240	8V2	ZENER		33933
		with	TR212		D241	8V2	ZENER		33933

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'Y' PRE-AMP (Cont.)

Section 6

Ref	Value	Description	Tol %±	Part No
DIODES				
D201		IN3595		29330
D202		IN3595		29330
D203		IN4148		23802
D206		IN4148		23802
D207				
D208	3V3	ZENER		33923
D209		IN4148		23802
D221		IN3595		29330
D222		IN3595		29330
D223		IN4148		23802
D224				
D225				
D226		IN4148		23802
D227				
D228	3V3	ZENER		33923
D229		IN4148		23802
D240	8V2	ZENER		33933
D241	8V2	ZENER		33933

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			R3		R4		R5	R
RESIS		R2 R22	R23		R24		R 2 5 R 240 R 25	ş
CAP		C 2		C3 C23	C 201 C 2 21 C 24	C 2 0 2 C 2 2 2	C 24	. 1
MISC.	SKA SKB			520 525	5 2 52	1a 5a D240		_



Y' PRE-AMPLIFIER. PRINTED CIRCUIT ROARD ASSEMBLY No 36983

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Fig. 4 Y Preamplifiers Circuit Diagram

TIMEBASE

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Ref	Value	Description	To/ % ±	Part No	Ref	Value	Description	To l %±	Part No
		Description	101 % -	1 21 (100				101 /6 -	
RESIST				24020	R142	8k2	CF		21808
R85	2M2	CF		24838	R143	1k5	CF		21801
R86	150k	CF		21821	R144	10k	CF		21809
R 87	680k	CF		31839	R145	3k3	CF		21803
R88	1 M	CF		31840	R146	4k7	CF		21805
R89	10k	CF		21809	R147	27k	CF		21813
R90					R148	1k	CF		21799
R91	4k7	CF		21805	R149	1M	CF		31840
R92	4 k 7	CF		21805	R150	100k	CF		21819
R93	100	CF		21794	R151	1k	CF		21799
R94	10k	CF		21809	R152	3k9	CF		21804
R95	3k3	CF		21803	R153	10k	CF		21809
R96	1 k 8	CF	½W	18553	R154				
R97	100	CF	,	21794	R155				
R98					R156	100k	CF		21819
R99					R157	10M	CF		32661
R100					R158	680	CF		28723
R101	620	МО		22485	R150	2k2	CF		21802
R101	620	MO		22485	R159	15k	CF		21802
R102	020	WIO		22403					
	200	MO		26740	R161	3k9	CF		21804
R104	390	MO		26740	R162	3k9	CF		21804
R105	390	MO		26740	R163	15k	CF		28727
R106	820	CF		28724	R164	12k	CF		21810
R107	3k3	CF		21803	R165	47k	CF		21815
R108	2k5	CP		36265	R166	100k	CF		21819
R109	3k3	CF		21803	R167	100k	CF		21819
R110	2k5	СР		36265	R168	10k	CF		21809
R111	3k9	CF		21804	R169	1 k	CF		21799
R112	22k	CF		21812	R170	1k5	CF		21801
R113	330	CF		28721	R171	270k	CF		32356
R114	330	CF		28721	R172	680k	CF		31839
R115	2k7	CF		28726	R173	100	CF		21794
R116	56	CF		35352	R174	56k	CF	1 W	19058
R117	47	CF		28714	R175	3k9	CF		21804
R118	220k	CF		21823	R176	3k9	CF		21804
R119	3k9	CF		21804	R177	56k	CF	1 W	19058
R120	820k	CF		32360	R178	10k	CF	4W	29481
R121	22k	CF		21812	R179	100	CF		21794
R122	22k	CF		21812	R180	100	CF		21794
R123	820k	CF		32630	R181	10k	CF	4W	29481
R124	10	CF		21793	R182	56k	CF	1W	19058
R125	390	CF		28722	R183	68k	CF		21816
R126	47	CF		28714	R184	910	CF		52991
R127		01		20711	R185	2k2	CF		21802
R128	1k2	CF		21800	R186	27k	CF		21803
R120	47	CF		21300	R187	100	CF		21803
R129	15	CF		28708	R187 R188	270	CF		28720
R130 R131	15	CF							
				28708	R189	2k7	CF		28726
R132	2k5	CP		36265	R190	100	CP		36261
R133	3k3	CF		21803	R191	1k	CP		36264
R134	10	CF		21793	R192	1k2	CF		21800
R135	10	CF		21793	R193	1k5	CF		21801
R136	10	CF		21793	R194	180	CF		21795
R137	1k	CF		21799	R195	100	CF		21794
R138					R 196	1k2	CF		21800
R139	10	CF		21793	R 197	1k6	MO		29793
R140	330	CF		28721	R198	1k6	CF		29793
R141	390	CF		28722	R199	1 k 6	MO		29793

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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CAPAC	ITORS								
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	C101	100pF	CE(2)		22376	TR112		BCB2B		33205
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		100pF	CE(2)		22376					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								2N2369 (I.T.T	. Only)	33701
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					24902					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					22388					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					24902					23307
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.01µF	CE(2)		24902					
C109 JµF CE(2) 25V 36709 TR120 BC212 29327 C110 33pF CE(2) 22370 TR121 BC182B 33205 C112 27pF CE(2) 22370 TR121 BC182B 33205 C112 27pF CE(2) 22369 TR123 BF258 31490 C113 .01µF CE(2) 24902 TR124 BF258 31490 C114 .0µF CE(2) 24902 TR126 BC212 29327 C115 .01µF CE(2) 24902 TR126 BC212 29327 C116 .47µF CE(2) 24902 TR126 BC212 29327 C116 .47µF CE(2) 24902 TR126 BC212 29327 C116 .47µF CE(2) 22369 D101 IN4148 23802 C121 100pF CE(2) 22376 D103 IN4148 23802 C121 100pF		.01µF	CE(2)		24902			BC212		29327
C110 33pF CE(2) 22370 TR121 BC182B 33205 C111 33pF CE(2) 22370 TR122 BC212 29327 C112 27pF CE(2) 22369 TR123 BF258 31490 C113 .01µF CE(2) 24902 TR124 BF258 31490 C114 .1µF CE(2) 25V 36709 TR125 BC212 29327 C116 .47µF CE(2) 2358 TR126 BC212 29327 C116 .47µF CE(2) 23369 DioDES C119 27pF CE(2) 23369 DioDES C120 100pF C120 10pF CE(2) 23369 Di01 IN4148 23802 C120 10pF CE(2) 22364 Di02 IN3595 29330 C121 10pF CE(2) 22376 Di03 IN4148 23802 C123 .01µF CE(2) 24902 Di05 IN4148 23802 C124 100pF CE(2) 24902 Di08	C109	.1µF	CE(2)	25V	36709					29327
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C110	33pF	CE(2)		22370					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C111	33pF	CE(2)		22370					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C112	27pF								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C113	.01µF								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C114	$.1\mu F$		25V						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C115									
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	C116							00112		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	C117									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C118					DIODES				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C119							IN4148		23802
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C120									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C121									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C122						15V			
C124 100pF CE(2) 22376 D106 IN4148 23802 C125 D107 IN4148 23802 C126 .01µF CE(2) 24902 D108 8V2 ZENER 33933 C127 A.O.T. D109 IN4148 23802 TRANSISTORS D110 IN4148 23802 TR101 BC182B 33205 D112 IN4148 23802 TR102 2N2369 23307 D113 IN4148 23802 TR103 2N2369 23307 D114 3V9 ZENER 33925 TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D114 3V9 ZENER 33925 TR104 BC182B 33205 D115 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR107 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TIC101 MC14001 36195 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>15,</td> <td></td> <td></td> <td></td>							15,			
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C125									
C127 A.O.T. D109 IN4148 23802 TRANSISTORS D110 IN4148 23802 TR101 BC182B 33205 D111 IN4148 23802 TR102 2N2369 23307 D113 IN4148 23802 TR103 2N2369 23307 D113 IN4148 23802 TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D114 3V9 ZENER 33925 TR105 2N2369 23307 D116 IN4148 23802 TR105 2N2369 23307 D114 3V9 ZENER 33925 TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR107 2N2369 23307 INTEGRATED CIRCUITS TR108 2N2369 23307 TR108 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TR101 MISCELLANEOUS <td>C126</td> <td>.01µF</td> <td>CE(2)</td> <td></td> <td>24902</td> <td></td> <td>8V2</td> <td></td> <td></td> <td></td>	C126	.01µF	CE(2)		24902		8V2			
TRANSISTORS D110 IN4148 23802 TR101 BC182B 33205 D111 IN4148 23802 TR102 2N2369 23307 D112 IN4148 23802 TR103 2N2369 23307 D113 IN4148 23802 TR103 2N2369 23307 D114 3V9 ZENER 33925 TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D114 3V9 ZENER 33925 TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 INTEGRATED CIRCUITS TR107 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TR101 MSCELLANEOUS TR100 2N2369 23307 MISCELLANEOUS TR102 MSCELLANEOUS		•	(-)	A.O.T.	2		0,2			
TRANSISTORS D111 IN4148 23802 TR101 BC182B 33205 D112 IN4148 23802 TR102 2N2369 23307 D113 IN4148 23802 TR103 2N2369 23307 D113 IN4148 23802 TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D114 3V9 ZENER 33925 TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR107 2N2369 23307 INTEGRATED CIRCUITS TR107 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TR109 BC182B 33205 TR110 2N2369 23307 MISCELLANEOUS IM1401 36195										
TR101 BC182B 33205 D112 IN4148 23802 TR102 2N2369 23307 D113 IN4148 23802 TR103 2N2369 23307 D114 3V9 ZENER 33925 TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D116 IN4148 23802 TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR107 2N2369 23307 INTEGRATED CIRCUITS 7 TR108 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 T T 111 36195 TR100 2N2369 23307 MISCELLANEOUS 36195	TRANSI	STORS								
TR1022N236923307D113IN414823802TR1032N236923307D1143V9ZENER33925TR104BC182B33205D115IN414823802TR1052N236923307D116IN414823802TR1062N236923307D116IN414823802TR1072N236923307INTEGRATED CIRCUITS36195TR1082N236923307IC101MC1400136195TR109BC182B33205TR1102N236923307MISCELLANEOUS	TR101		BC182B		33205					
TR103 2N2369 23307 D114 3V9 ZENER 33925 TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR107 2N2369 23307 INTEGRATED CIRCUITS 36195 TR108 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TR110 2N2369 23307 MISCELLANEOUS	TR102		2N2369		23307					
TR104 BC182B 33205 D115 IN4148 23802 TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 INTEGRATED CIRCUITS 2802 TR107 2N2369 23307 INTEGRATED CIRCUITS 36195 TR108 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TR110 2N2369 23307 MISCELLANEOUS	TR103		2N2369		23307		3V9			
TR105 2N2369 23307 D116 IN4148 23802 TR106 2N2369 23307 INTEGRATED CIRCUITS 20000 2000 2000	TR104		BC182B							
TR106 2N2369 23307 INTEGRATED CIRCUITS TR107 2N2369 23307 INTEGRATED CIRCUITS TR108 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 TR110 2N2369 23307 MISCELLANEOUS	TR105		2N2369							
TR107 2N2369 23307 INTEGRATED CIRCUITS TR108 2N2369 23307 IC101 MC14001 36195 TR109 BC182B 33205 33205 TR110 2N2369 23307 MISCELLANEOUS	TR106		2N2369							20002
TR109 BC182B 33205 TR110 2N2369 23307 MISCELLANEOUS	TR107		2N2369			INTEGR	ATED CIRC	CUITS		
TR109 BC182B 33205 TR110 2N2369 23307 MISCELLANEOUS	TR108									36195
TR110 2N2369 23307 MISCELLANEOUS	TR109									
	TR110					MISCELL	ANEOUS			
	TR111									29496

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TIMEBASE (Cont.)

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Section 6

Ref	Value	Description	To/ % ±	Part No
TR112		BCB2B		33205
TR1 13				
TR114		2N2369 (I.T.T. (33701
TR115		2N2369 (I.T.T. C	Only)	33701
TR116		2N2369		23307
TR117		2N2369		23307
TR118		D.C.2.1.2		00000
TR119		BC212		29327
TR120		BC212		29327
TR121		BC182B BC212		33205
TR122				29327
TR123		BF258		31490
TR124		BF258 BC212		31490
TR125 TR126		BC212 BC212		29327
1 K1 20		BC212		29327
DIODES				
D101		IN4148		23802
D102		IN3595		29330
D103		IN4148		23802
D104	15V	ZENER		33939
D105		IN4148		23802
D106		IN4148		23802
D107		IN4148		23802
D108	8V2	ZENER		33933
D109		IN4148		23802
D110		IN4148		23802
D111		IN4148		23802
D112		IN4148		23802
D113		IN4148		23802
D114	3V9	ZENER		33925
D115		IN4148		23802
D116		IN4148		23802
	ATED CIRCU			
IC101		MC14001		36195
				20.40.4
L101	15μH			29496

RESIS	R101 R102	R104 R105 R106		R 107 A109	R106 R110	R112 R120	R113 R121 R116 R117	R114 k' R122 R1
CAP	C101 C102	C17	CIB		C104	C127	C1	05
	SKC S13aF	\$12			T	R101 TR102		TRIO3

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Fig. 5 Timebase Circuit Diagram

Section 6

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POWER SUPPLY & 'Y' O/P

RESIS [®] R301 R302 R303 R304 R305 R306 R307 R308 R309 R310 R311 R312 R313 R314	120 390k 3k3 100k 4k7 500k 390k 270k 100 500k 100k 100k 1M 25k	CF CF CF PCP CP CF CF CF CF CF CF	₩	18539 32358 21803 21819 28279 36271 32358 32356 21794	R357 R358 R359 R360 R361 R362 R363 R364 R365	2k4 100 2k2 10 820 330 82 100	MF CF CF CF CF CF CF		37208 21794 21802 21793 28724 28721
R302 R303 R304 R305 R306 R307 R308 R309 R309 R310 R311 R312 R313 R314	390k 3k3 100k 4k7 500k 390k 270k 100 500k 100k 1M 25k	CF CF PCP CP CF CF CF CF CF	₩	32358 21803 21819 28279 36271 32358 32356	R358 R359 R360 R361 R362 R363 R364	100 2k2 10 820 330 82	CF CF CF CF CF		21794 21802 21793 28724
R303 R304 R305 R306 R307 R308 R309 R310 R311 R312 R313 R314	3k3 100k 4k7 500k 390k 270k 100 500k 100k 1M 25k	CF CF PCP CF CF CF CF CF CF		21803 21819 28279 36271 32358 32356	R359 R360 R361 R362 R363 R364	100 2k2 10 820 330 82	CF CF CF CF CF		21794 21802 21793 28724
R304 R305 R306 R307 R308 R309 R310 R311 R312 R313 R314	3k3 100k 4k7 500k 390k 270k 100 500k 100k 1M 25k	CF CF PCP CF CF CF CF CF CF		21803 21819 28279 36271 32358 32356	R360 R361 R362 R363 R364	10 820 330 82	CF CF CF CF		21802 21793 28724
R305 R306 R307 R308 R309 R310 R311 R312 R313 R314	100k 4k7 500k 390k 270k 100 500k 100k 1M 25k	CF PCP CF CF CF CF CP CF		21819 28279 36271 32358 32356	R361 R362 R363 R364	10 820 330 82	CF CF CF		21793 28724
R306 R307 R308 R309 R310 R311 R312 R313 R314	4k7 500k 390k 270k 100 500k 100k 1M 25k	PCP CF CF CF CF CP CF		28279 36271 32358 32356	R361 R362 R363 R364	820 330 82	CF CF		28724
R307 R308 R309 R310 R311 R312 R313 R314	500k 390k 270k 100 500k 100k 1M 25k	CP CF CF CF CP CF		36271 32358 32356	R362 R363 R364	330 82	CF		
R308 R309 R310 R311 R312 R313 R314	390k 270k 100 500k 100k 1M 25k	CF CF CF CP CF		36271 32358 32356	R363 R364	82			20721
R309 R310 R311 R312 R313 R314	270k 100 500k 100k 1M 25k	CF CF CP CF		32358 32356	R364		<u></u>		28717
R310 R311 R312 R313 R314	100 500k 100k 1M 25k	CF CP CF		32356		1111	CP		36958
R311 R312 R313 R314	500k 100k 1M 25k	CP CF			נחרא	10	CF		21793
R312 R313 R314	100k 1M 25k	CF			R366	2k7	CF		28726
R313 R314	1M 25k			36271	R367	250	PCP		
R314	25k			21819	R368	250 2k2	CF	1/ 117	29371
				31840	R369	2k2 2k4	MF	¹∕8 W	21802
		СР		36268	R309 R370	2 K 4 39			37208
R315	82k	CE		21010	R371		CF	. /	28713
R316	33k	CF MAURITRO	ice Manuals Conta N TECHNICAL SERVI	21818		1M5	CF	½₩	18588
R317	5k6	CF 8 Cherr	N TECHNICAL SERVI y Tree Rd, Chinno	CES-1014	R372	5k6	CF		21806
R318	6M8	MG_O	kon OX9 4QY		R373	470	CF		21797
R319	25k	CD Tel:- 01844-3	51694 Fax:- 01844-35	37201	R374	120	CF		28718
R320	100	CF Email:-en	quiries@mauritron.co.	uk 36268	R375	10	CF		21793
R321	680k			21794	R376	47	CF		28714
R322	1k	CF		31839	R377	620	MF		37207
R323		CF		21799	R378	2k4	MF		37208
	22k	CF		21812	R379	100	CF		21794
R324	3k3	CF		21803	R380	2k2	CF		21802
R325	500k	CP		36271	R381	33k	CF		21814
R326	6M8	MG		37201	R382	150	CF		28719
R327	470k	CF		32330	R383	4k7	CF		21805
R328	10k	PCP		29574	R384	4k7	CF		21805
R329	8k2	CF		21808	R385	4k7	CF		21805
R330	5k6	CF		21806	R386	4k7	CF		21805
R331	1 k	CF		21799	R387	100k	CF		21819
R332	680k	CC		5024	R388	4k7	CF		21805
R333	680k	CC		5024	R389	270k	CF		32356
R334	100k	CF		21819	R390	220k	CF		21823
335	22k	CF		21812	R391	100	CF	½W	18538
336	100	CF		21794	R392			A.O.T.	10550
337	220k	CF		21823	R393			А.О.Т.	
338	10	CF		21793	R394			A.O.T.	
339	330	CF		28721	R395			A.O.T.	
340	820	CF		28724				1.0.1.	
341	82	CF		28717	R901	4M7	MG	1 W	37171
342	100	СР		36958	R902	68M	MG	1W	37173
343	10	CF		21793	R903	27M	MG	1W 1W	37172
344	2k7	CF		28726	1000	2714	110	1 11	5/1/2
345	250	PCP		29371	CAPACI	TOPS			
346	2k2	CF		21802	C301	4.7μF	Е	4501	74941
347	2k4	MF		37208	C301	4.7μF 4.7μF		450V	34841
348	39	CF		28713	C302		E	450V	34841
349	680	CF		28723	C303 C304	4.7μF	E	450V	34841
350	5k6	CF		21806		4.7μF	E	450V	34841
351	470	CF			C305	4.7μF	E	450V	34841
352	120	CF		21797	C306	4.7μF	E	450V	34841
353	620	MF		28718	C307	4.7μF	E	450V	34841
354	10	CF		37207	C308	$4.7\mu F$	E	450V	34841
355	47			21793	C309	10µF	E	25V	32180
355 356	47	CF		28714	C310	10µF	E	25 V	32180
550	100	CF		28719	C311	1000pF	CE(2)	500V	22387

Section 6

POWE	R SUPPLY 8	ዿ Ύ O/P (Con	t.)						
Ref	Value	Description	Tal %±	Part No	Ref	Value	Description	Tol %±	Part No
C312	1000pF	CE(2)	500V	22387	TR313		2N2369		23307
C312	4.7μF	E	63V	32195					32902
					TR314		BF380		
C314	56pF	CE(2)	2kV	37202	TR315		BF380		32902
C315	56pF	CE(2)	2kV	37202	TR316		2N2369		23307
C316	4.7μF	E	63V	32195	TR317		2N3904		24146
C317	$1\mu F$	E	63V	32193	TR318		2N2369		23307
C318	2.2µF	Е	350V	37214	TR319		2N2369		23307
C319	2.2µF	E	350V	37214	TR320		BF380		32902
C320	.08µF	PE	5kV	36277	TR321		BF380		32902
C321	1000pF	CE(2)	500V	22387	TR322		2N2369		23307
C322	68pF	PS		35911					
C323	10/70pF	TRIMMER		37219	DIODES				
C324	10/70pF	TRIMMER		37219	D201		REMO HS 2-6		37809
C325	27pF	CE(2)	500V	22369	D301		or H691 8kV		or 37174
C326	•		A.O.T.		D302	10V	ZENER		33935
C327	15pF	PS		35907	D303	4V7	ZENER		33927
C328	68pF	PS	A.O.T.	35911	D304		IN4003		23462
C329	.1μF	CE(2)	25V	36709	D305		IN4003		23462
C330	.1μF	CE(2)	25V	36709	D306		IN4003		23462
C331	.1μF	CE(2) CE(2)	25V 25V	36709	D307		ZENER		27957
C332	1000pF	CE(2) CE(2)	500V	22387	D308		IN4148		23802
C333	68pF	PS	300 v	35911	D309		IN4148		23802
C334		TRIMMER		37219	D310		IN4148		23802
C334 C335	10/70pF 10/70pF	TRIMMER		37219	D310 D311		IN4148		23802
C335			500V		D311 D312		IN4148 IN4007		52337
C330 C337	27pF	CE(2)	500V	22369	D312 D313		IN4007 IN4007		52337
C338	15-15	DC	A.O.T.	25007	D313 D314	160 V	ZENER		37212
	15pF	PS	251	35907		160 V			37212
C339	.1μF	CE(2)	25V	36709	D315		ZENER ZENER		29485
C340	68pF	PS	A.O.T.	35911	D316 D317	150V	IN4148		23403
C341	$.1\mu F$	CE(2)	25V	36709					23802
C342	.1µF	CE(2)	25V	36709	D318	8V2	IN4148 ZENER		33933
C343	.1μF	CE(2)	25V	36709	D319 D320	8V2 8V2	ZENER		33933
C344	4700pF	CE	4kV	26863					33935
C345	$.01 \mu F$	CE(2)	250V	22395	D321	10V	ZENER IN4148 Fitt	ed if req.	23802
C346	0.47µF	PE	63V	31362	D322			ed if Req.	
C347	4.7μF	E Fitted i		34841	D323		IN4148 Fitt	eu n Keq.	23802
C348	4.7µF	E Fitted in	f req. 63V	32195	D001		REMO HS 2-6		37809
					D901		or H691 8kV		or 37174
C901	.08µF	PE	5kV	36277	D 0 0 0		REMO HS 2-6		37809
C902	.08µF	PE	5kV	36277	D902		or H691 8kV		or 37174
C903	.08µF	PE	5kV	36277			REMO HS 2-6		37809
C904	.08µF	PE	5kV	36277	D903		or H691 8kV		or 37174
							REMO HS 2-6		37809
TRANS	ISTORS				D904		or H691 8kV		or 37174
TR301		BFY50		26112					
TR302		BF380		32902	INTEGR	ATED CI	RCUITS		
TR303		BC182B		33205	IC301		78M20CP		37213
TR304		BC212		29327	IC302		7915		36185
TR305		BC212		29327					
TR306		BC212		29327	MISCEL	LANEOUS	5		
TR307		BUX86		37562	BR301		WO6		21150
TR308		BC182B		33205					
TR309		BC182B		33205	L301	15µH			29496
TR310		BC182B		33205	L301	$15\mu H$			29496
TR311		2N3904		24146	L302 L303	15μH			29496
TR312		2N2369		23307	L303 L304	$15\mu H$			29496
		2012207		20001	LUUT	1.5µ11			22120

POWER SUPPLY & 'Y' O/P (Cont.)

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t No	Ref	Value	Description	Tol %±	Part No
387	TR313		2N2369		23307
195	TR314		BF380		32902
202	TR315		BF380		32902
202	TR316		2N2369		23307
.95	TR317		2N3904		24146
.93	TR318		2N2369		23307
214	TR319		2N2369		23307
214	TR320		BF380		32902
277	TR321		BF380		32902
87	TR322		2N2369		23307
911					
219	DIODES	5			
219	D301		REMO HS		37809
69	D202	1017	or H691 8kV		or 37174
0.7	D302	10V	ZENER		33935
07	D303	4V7	ZENER		33927
11	D304		IN4003		23462
709	D305		IN4003		23462
709 100	D306		IN4003		23462
09	D307		ZENER		27957
87	D308		IN4148		23802
11	D309		IN4148		23802
.19	D310		IN4148		23802
.19	D311		IN4148		23802
69	D312 D313		IN4007		52337
07	D313 D314	160V	IN4007 ZENER		52337
09	D314 D315	160V 160V	ZENER		37212 37212
11	D316	150V	ZENER		29485
09	D317	1301	IN4148		23483
09	D318		IN4148		23802
09	D319	8V2	ZENER		33933
63	D320	8V2	ZENER		33933
95	D321	10V	ZENER		33935
62	D322		IN4148	Fitted if req.	23802
41	D323		IN4148	Fitted if Req.	23802
95			REMO HS	•	
	D901		or H691 8kV	- •	37809
77			REMO HS		or 37174
77	D902		or H691 8kV		37809
77			REMO HS		or 37174 37809
77	D903		or H691 8kV		or 37174
			REMO HS		37809
	D904		or H691 8kV		or 37174
12					01 57174
02		ATED CIR			
05	IC301		78M20CP		37213
27	IC302		7915		36185
27					
27		LANEOUS			
62	BR301		WO6		21150
05					
05	L301	15µH			29496
05	L302	15µH			29496
46	L303	15µH			29496
07	L304	15µH			29496



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Fig. 6 Power Supplies and Y Output Am

Section 6

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INTERCONNECTIONS

Ref	Value	De	scription	To/ % ±	Part No	Ref	Value	Description	To/ %±	Part No
RESIS	TORS					CAPAC			101 /02	1 01 (100
R2	22	CF	7		28710	C2	3.3pF	CE(2)		o
R3	22	CF			28710	C2 C3		CE(2)		817
R4	990k	MF			26345		.1μF	CE(2)		29495
R5	22	CF				C4	470pF	PS		11492
R6	1M	MF			28710	C5	.01µF	CE(2)		24902
R7	470k	CC			26346					
	17 OK	CC			4906	C10	6/25pF	TRIMMER		23593
R10/I		USTOI	R NETWORK			C11	68pF	SM		4513
R16	1M			1	43/36455	C12	.01µF	PS		24886
R10 R17	1k + 1k	CF			31840	C13	$1 \mu F$	PC		33206
R17 R18	4k7	CP	R17a + R17t		44/36069	C14	.047µF	CE(2)	30V	2793
		CF			21805	C15	4.7µF	E	63V	32195
R19 R20	470	CF			21797	C16	680pF	CE(2)		22385
		CP	With S10		4/32897	C17	470pF	CE(2)	10V	22383
R21	22	CP	With S11	A	4/32898	C18	.47µF	CE(2)	63V	31362
R22	22	CF			28710		•	(-)	001	51502
R23	22	CF			28710	C22	8.2pF	CE(2)		22363
R24	990k	MF			26345	C23	$.1\mu F$	PE		22303
R25	22	CF			28710	C24	470pF	PS		11492
R26	1M	MF			26346	C25	.01µF	CE(1)		
R27	470k	CC			4906					24902
R28	100k	CF		1W		C31	2200µF	Е	4017	26022
						C32	2200µF	Ē	40V	36022
R31	47	WW	,		18739		$100\mu F +$	Ľ	40V	36022
R32	68k	CF			21816	C33	100µF	E C33a +	C33b A	4/36023
R33					21010		ΙΟΟμι			,
R34		СР		Δ	4/37180					
				1.	1,57100	DIODES				
R38		СР	With S30	۵	4/37179	D11				35202
R39		CP			4/37181					
R40	16k	MF		Л	29361	ILP1				37178
R41	15k8	MF			33291	ILP2				37178
R42	5k23	MF								5/1/6
R43	1k72	MF	5		33290		-			
R44	787	MF	5		33289	SOCKET	5			
R45	360	MF			33288	S10				4/32897
R46	16k	MF			33287	S11		W	ith R21 A4	1/32898
R40 R47	15k8	MF			29361	S12				34991
R47 R48	5k23				33291	S13				32636
R49	1k72	MF			33290	S14				37199
R49 R50	787	MF			33289	S15				4881
R51		MF			33288	S16				36662
	360	MF	West con		33287					
R52	22k	CP	With S27		4/32895	S20				34991
R53	22k	СР	With S28	A	4/32895	S21		Wi	th R58/S41	37216
R54	10									-
R55	18	CF			28709	S25				34991
R56	18	CF			28709	S26		Wi	th R59/S42	37216
R57						S27			•	/32895
R58	500	CP	With S21/S41		37216	S28				/32895
R59	500	СР	With S26/S42		37216	S29				122075

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Section 6

			•						
Ref	Value	Description	Tol % ±	Part No	Ref	Value	Description	Tol % ±	Part No
					MISCEL	LANEOUS			
S30			With R38 A	44/37179	BR31		WO2		19725
S31				36815	BR32		WO4		29367
					2102				27507
S41			With S21/R58	37216	L31				A3/31329
S42									
342			With S26/R59	37216	T31				A1/37168
SKA				26587	E021		500mA 230V	Supply	33685
SKB				26587	FS31			Supply	34790
SKC				26587			111 115 (ouppij	51790
JIC				20307	DI .				
					PLA				33787
SKE				29492					
SKF				29492	V31		C.R.T. E14-101G	н	37194
SKG							0.1.1. 214-1010	11	
OVC				29492	V32				26586

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INTERCONNECTIONS (Cont.)

Section 6

Value	Description	Tol % ±	Part No
ELLANEOUS			
1	WO2		19725
2	WO4		29367
			A3/31329
			A1/37168
1		230V Supply	33685
L	1A	115V Supply	34790
			33787
	C.R.T. E14	-101GH	37194 26586

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Fig. 7 Interconnection diagram

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Guarantee and Service Facilities

Section 7

This instrument is guaranteed for a period of two years from its delivery to the purchaser, covering faulty workmanship and replacement of defective parts other than cathode ray tubes and batteries (where fitted). Cathode ray tubes are subject to the manufacturers guarantee. This assumes fair wear and tear and usage in the specified environment and does not cover routine recalibrations and mechanical adjustments.

We maintain comprehensive after sales facilities and the instrument should be returned to our factory for servicing if this is necessary. The type and serial number of the instrument should always be quoted, together with full details of any fault and service required.

Equipment returned for servicing must be adequately

packed, preferably in the box in which the instrument was supplied and shipped with transportation charges prepaid. We accept no responsibility for instruments arriving damaged. Should the cause of failure during the guarantee period be due to misuse or abuse of the instrument, or if the guarantee has expired the repair will be put in hand without delay and charged unless other instructions are received.

Our Sales, Service and Engineering Departments are ready to assist you at all times.

The Service Department can provide maintenance and repair information by telephone or letter, if required.

Note: Please check fuses before returning instruments for service.