

<u>GFA-1, 1a</u> AMPLIFIER



<u>SERVICE MANUAL</u>



11 Elkins Road E. Brunswick, NJ 08816 (908) 390-1130 GFA-1 Service Manual

1

CONTENTS

Introduction

Section 1Circuit and Theory
Section 2Service information
Section 3Operational Specifications
Section 4Schematic Diagrams
Section 5Board views
Section 6Parts listing

INTRODUCTION

This manual provides the technical and service information required to perform all forms of maintenance to the GFA-1 and GFA-1a Power Amplifiers.

	Section 1 comparts the theory of created or and tootday of the condition
{:	
) 2	
(- <u>* *</u>	
·	Sactions 2 3. (Emplie are vide the information according to the country

2

CIRCUIT and THEORY

GENERAL DESCRIPTION

The ADCOM GFA-1 (and GFA-1a) Balanced Bridge Power Amplifiers are 2 pairs of true complementary-symmetric power amplifiers (4 amplifiers) mounted on a common chassis. Two of the four power amplifiers are driven out of phase as a pair of "bridging" amplifiers. This technique creates a balanced output from an un-balanced input. The amplifier employs input bandwidth limitation to control RF and T.I.M. related high-frequency aborations. The amplifier features a unique main-frame construction with a high efficiency forced-air cooling system. The la version incorporates an advanced protection technique offering "full coverage" electronic operating protection.

BRIDGING FOR POWER

Bridging two power amplifiers is an engineering technique which permits the combining of the safe operating aspects of a smaller amplifer with the nower and price peeds of the bight fidelity permission of the safe peeds of the bight fidelity permission.

L

and looking at the voltages that appear between the two outputs, we get the sum of the two outputs. This output is twice the voltage of either separate output. As the mathematics for power are a squared function, doubling the voltage means four times the power. Thus, the bridging configuration yields low-cost high power safely.

CIRCUIT DESRCIPTION

POWER AMPLIFIERS

Referring to the GFA-la schematic (section 3) the amplifier operates as follows:

The incoming signal is DC decoupled by Cl with Rl and C3 providing frequency limiting and R.F. protection. This signal is then applied to the bases of Ql and Q4 as one of the bridging signals and Q2 and Q3 for the other. Ql and Q4 drive transistors Q5 and Q6 completing the voltage drive portion of the positive amplifier. These signals are then fed to the output stage made up of Q10, Q11, Q12, and Q13. This output section is biased and thermally tracked by the network made up of CR30 and Q16. Feedback from this positive amplifier is returned to Q1 and Q4 via resistor R24. This same signal via R25 is fed to O2 and O3 which form the input

· · · · · · · · · · · · · · · · · · ·	
I	section of the negative signal amplifier. Q6 and Q7 comprise the remainder
	of the voltage gain stage for the negative side. This negative signal
	then drives the output section made up of Q14, Q15, Q16 and Q17 which
	is biased and thermally tracked by Q18 and the diode CR31. The two power
	amplifiers making up the bridging amplifier channel share a common power

supply and common floating voltage regulation provided by diode CR3.

POWER SUPPLY

All power is provided by a common power transformer utilizing separate power diode rectification and separate filtering capacitors (C26 through C29). Two speed fan operation is provided by switch S2 and limiting resistor R89.

VARIATIONS BETWEEN THE GFA-1 and the GFA-1a

In our description of the operation of the GFA-la and our reference to the schematic we made no mention of the protection circuits employed.

These protection aircuite and the major difference have the OFA 1 and

the GFA-la. Please note the short protection schematic in section 3. This is the GFA-la protection schematic. The protection integrated circuit U1 has been added and the old protection system of the GFA-l obsolete. Transistors Q19 and Q20 (along with their adjacent channel equivalents of Q22 and Q23) constantly monitor the positive going output current to .establish dynamic current limiting.

The GFA-la also utilizes an improved thermal tracking network by attaching diodes CR30 and CR31 to the heat sink and has replaced the power supply rectification diodes (originally on the PCB) with a set of full- wave bridge rectifiers mounted on the heat sink for superior cooling. In addition the GFA-la incorporates a set of peak power monitors in the form of transistors Q25 and Q26 driving LED's CR28 and CR29.

1

SERVICE INFORMATION

Test Set-Up

A-INTRODUCTION

٤.	· · · · · · · · · · · · · · · · · ·
_	
· "	
Ť	
λŋ.	
۲ ب	
٣	
	,
-	

of bridged amplifiers. The use of common grounds in the output system will cause considerable problem. Testing will require a FIRST-CLASS test set-up consisting of good equipment and good connections. SHOULD EITHER OF THESE REQUIREMENTS FALL SHORT, NO SERVICE SHOULD BE ATTEMPTED.

Throughout the course of this manual we strive to present the shortest and most practical service pathway. The technician is advised to read the manual before attempting service to assure the best use of his time.

B-EQUIPMENT

Servicing the GFA-1 series of power amplifiers will require the following types of equipment. We have identified appropriate manufacturers and models as guidelines.

f

3. Audio generator- An unbalanced output audio generator with less than 0.002% T.H.D. over the frequency range of 20 Hz to 20 kHz at a 3 volt output level. We suggest the use of the generator portion of the Sound Technology 1701A.

4. Oscilliscope- Capable of balanced input and a verticle sensitivity of 30 mv. The unit should have triggered sweep and a 10 MegaHertz bandwidth.

5. Line Controller- A "Variac" type of main power line controller. Adjustable from 0 to 130 volts, this unit should have a 25 amp capability. As all IHF tests require a main voltage of 120 volts throughout the test, only a high quality controller with good high current line regulation should be used (Staco, General Electric, General Radio, Superior Electric, etc..).

6. Load- a fully isolated 8 ohm non-inductive load with less than 500 pfd intrinsic capacity. The load should be capable of dissipating over 400 watts and be connected to the power amplifier with at least #14 wire.

1

screwdriver (we suggest an electric drive), a soldering iron of at least

35 wats, a solder sucker or equal, pliers, and diagonal cutters.

Attach the load to the output of the power amplifier. Make sure that the load has no connection with any other part of the test set-up. This means that the load has no "hot" and "ground" only a "+" and a "-". When

7 · •	
· · · · · · · · · · · · · · · · · · ·	i
	1
	I
	-

input of the distortion measuring unit should be attached to the amplifier's output in the same manner.

UNBALANCED TEST EQUIPMENT

If there is no alternative to the use of unbalanced test equipment the technician is reminded that a 200 watt bridging amplifier is really a pair of 50 watt power amplifiers, one of which is operating out-of-phase with the other. Measuring from chassis ground to either the "+" or "-" output you will get roughly 60 watts into 8 ohms. Remember that the "-" output is NOT ground but an out-of-phase signal. The distortion measurement will be better than specified and the slew rate will be about k_{1} All

DISASSEMBLY

Once the unit has been assessed as defective further service will require opening the unit. Place the GFA-la on the bench in front of you with the POWER SWITCH end towards you.

Using a #6 phillips screwdriver follow these steps:

a- Remove the 8 end screws.

b- Remove the 10 screws around the edge of this end cap.

c- Remove the 10 screws around the other end cap (this is the end with the speaker outputs).

d- Slide off the end cap facing you (the one with the power switch).

e- Slide the top cover piece out towards you and lift it away. At this point the printed circuit board is fully accessable for voltage measurements.

POWER TRANSISTOR REPLACEMENT

Once the unit has been opened and the fault mode assessed as including the failure of an output transistor, the following additional disassembly procedure must be followed:

f- Remove the 6 side screws on the bottom cover (three on each side).

g- Slide the bottom cover off.

h- Carefully roll the unit over onto the printed circuit board.

i- Remove the 4 standard screws securing the black power transformer. Set the transformer to the right of the unit and remove the steel plate securing it.

j- Using a long phillips screwdriver, remove the four screws securing the power transistor covers and slide these covers out of the heat sink.

k- Remove and replace the appropriate power transistors.

After completing repairs reassemble the unit in reverse order. Be especially careful not to pinch wires or drop debris into the unit while reassembling.

Operational Specifications (As per IHF A-202, 1978)

1- CONTINUOUS AVERAGE POWER OUTPUT is the minimum power available over the frequency range of 20 Hertz to 20 kiloHertz at less than the rated distortion (IHF 3.1) this output level is 200 watts per channel into 8 ohms and 350 watts per channel at 4 ohms.

2- DYNAMIC HEADROOM is the ratio between the power at 3% THD and the continuous power noted in step 1 at 1 kiloHertz (IHF 3.2.3) and is 1.3 dB.

3- FREQUENCY RESPONSE is the change in output compared to the input with a frequency of 1 kiloHertz as the "O" reference ponint (IHF 3.13.1) and is +, -0.25 dB from 20 Hertz to 20 kiloHertz at 200 watts, both channels driven, onto 8 ohm loads.

4- SENSITIVITY is the input voltage required to produce an output of 1 watt into 8 ohms (2.83 volts RMS) (IHF 3.7) and is 72 millVolts RMS for a gain of 31.5 db.

5- "A" WEIGHTED SIGNAL TO NOISE RATIO is the ratio between a 1 watt into 8 ohm output signal level and the output when the input has no signal and in terminated with a 1 kilohm resistor. The noise is filtered through a standard "A" type network (IHF 3.12.2) and is 90 db.

6- LOW FREQUENCY DAMPING FACTOR is the ratio between an 8 ohm load and the 50 Hertz output impedance (IHF 3.11.2) and is 60.

7- CROSSTALK is the ratio of the worst cross channel leakage over a range of 100 Hertz to 10 kiloHertz (IHF 3.14.1) and is 50 dB at 10 kiloHertz.

8- SMPTE INTERMODULATION DISTORTION is the distortion resulting from the amplification of a signal consisting of a 4 to 1 mixture of 60 Hertz and 7 kiloHertz (IHF 1.18 and 3.15.4) and is less than 0.1% at an output level of 200 watts into 8 ohms.

SCHEMATIC DIAGRAM WITH VOLTAGES

ADCOM GFA-la

-

.

12

.

.



. ·





ı ا 1 ð tur sta U m 'ą h ч. Т

	- ··· · ··· ··· ·	
DEL GFA-la	DATE 09-11-80 PREVIOUS PAGE 1 OF	3
5/1/ 22-001-A	ASSEIN. DESC. PC ASSEMBLY	
ART Nº QTY	DESCRIPTION REF. DESIG.	
01-003-2 6	R: 2KOHM 2% 4W CF	
01-002-2 16	R: 1KOHM 2% ¼W CF	
01-010-2 8	R: 39KOHM 2% ¼W CF	
01-005-2 8	R: 10KOHM 2% 4W CF	
01-009-2M 8	R: 1.2KOHM 2% 4W CF-M	
01-008 12	R: 68 OHM 5% 4W MOF	
01-004-2 4	R: 3.3KOHM 2% 4W CF	
01-013 8	R: 10 OHM 5% 4W MOF	
01-006 2	R: 330 KOHM 5% 4W CF	
01-040 2	R: 27 KOHM 5% 4W MOF	
01-016 5	R: 15 KOHM 5% W CF	
01-011 6	R: 1 KOHM 5% 4W MOF	
4	R: 12 KOHM 5% 5W CF	
01-018 4	R: 330 OHM 5% 1/2 MOF	
<u>~1-019 4</u>	R: 120 KOHM 5% 4W CF	
01-020 5	R: 47 KOHM 5% 4W CF	
01-021 1	R: 270 KOHM 5% 4W CF	
01-022 1	<u>R: 18 KOHM 5% ½W CF</u>	
01-023 1	R: 150 KOHM 5% 1/2W CF	
01-024 1	<u>R: 22 КОНМ 5% ½W CF</u>	
01-025 2		
		•
· · · · · · · · · · · · · · · · · · ·		
	·	
03-001 1	R: 10 OHM 5% 5W MOF	
03-002 1	R: 240 OHM 5% 1/2W MOF	
04-011 1	R: 620 OHM 5% 1W MOF	
04-002 4	<u>R: 62 OHM 5% IW MOF</u>	
4-004 4	<u>R: 10 OHM 5% 2W MOF</u>	
04-007 1	R: 100 OHM 5% 1W MOF	
_04-0031	<u>R: 3.9 KOHM 5% IW MOF</u>	
04-005 4	R: 2.2 OHM 5% 2W MOF	
04–006 s ⁻¹	D- 125 OHM 109 1017 101	1

	DATE 09-11-80 PREVIOUS	PAGE 2 OF 3
5id 22-001-A	ASSEM. DESC. PC ASSEMBLY	
ART Nº QTY	DESCRIPTION	REF. DESIG.
07-006 12	C: .1 MF + 80 100v GPC	
07-004 4	C: 10PF 10% GPC	:
07-003 8	C: 47PF 10% GPC	
	C: 220PF 10% GPC	
9	C: .01MF +80 100v GPC	
08-006 4	C: MY .1MF 100V RA DIP	
09-002 6	C: EL 100MF 10v RA	
09-001 4	C: EL 10 MF 50V RA	I
09-004 2	C: EL 4.7 MF 50V RA	
09-006 2	C: EL 47 MF 16V RA	•
09-0071	C: EL .47 MF 50V RA	
09-008 1	C: EL 1.MF 50V RA	
<u>19-0091_</u>	C: EL 22 MF 16V RA	
	<u>C: EL 10 MF 25V RA</u>	
09-005 4	C: EL 8200 MF 63V RA	
· · · · · · · · · · · · · · · · · · ·		
	DL: IN 4004	
<u>11-005</u> 2	DL: IN 5262 B 51V 5% ZEN	
11-003 10	DL: IN 4148	
11-018 2	DL: IN 5252 B 24V 5% ZEN ·	
<u>11-007</u> <u>6</u>	TR: MPS AO6 NPN	
11-006 2	TR: MPS A56 PNP	
4	TR:2\$A798	:
4		
11-013 4	TR: 2SA914	
11-012 4	TR: 2SC1953	
11-019 1	<u>IC: TA7317-P</u>	
1-022 4	TR: MPS A06 SEL (Beta 70-120)	
12-003 2	RELAY: FRL264 D048/02CK	

•

•	<u> </u>	
DDEL GFA-1a	DATE 09-11-80 PREVIOUS PAGE 3 OF	3
3M 22-001-A	ASSEM. DESC. E PC ASSEMBLY	4
-ART Nº QTY	DESCRIPTION REF. DESIG.	
15-003 4	CHOKE: OUTPUT	
·		
17-006-A 1	PC BD: MAIN (GFA-la)	
8	SOCKET: TR EMUDEN M 1629	
18-006 1	JACK: EMUDEN 5526	
18-0041	LUG: #6 SOLDER	
18-018 8	LUG: 'z" PUSH, CRIMP # 16 GA	
21-026 5	JUMPER: #22 GA SLD BLK PVC .4"	<u> </u>
?1-027 1	JUMPER: #22 GA SLD BLK PVC .2"	
<u>21-010</u> 15	JUMPER: #22 GASLD_PVC_BLK5"	
21-012 7	JUMPER: #22 GA SLD PVC BLK .75"	
21-015 1	JUMPER: #22 GA SLD PVC BLK 1"	
21-013 8	JUMPER: #22 GA SLD PVC BLK 1.5"	
21-011 5	JUMPER: #22 GA SLD PVC BLK 2"	
<u>21–008–06</u> 6	WIRE: #16 GA_STRD_RED	
21-007-06 2	WIRE: #16 GA STRD GRY	
21-005-03 1	WIRE: #16 GA STRD BLK	
21-005-11 1	WIRE: #16_GA_STRD_BLK	
<u>21-016-12</u> 1	WIRE: #22 GA STRD RED	
21-017-12 1	WIRE: #22 GA STRD GRY	· * *
21-018-12 1	WIRE: #22 GA STRD ORG	
		1 1

-

•

'ODEL GFA-1a		A
ODEL GFA-1a	DATE 09-22-80 PREVIOUS PAGE 1 OF	3
<u>5M 50-003</u>	ASSEM. DESC. FINAL ASSEMBLY	
ART Nº QTY	DESCRIPTION REF. DESIG.	
04-010 1	R:500 ohm 10% 20W WW	
		·
·		
11-016 2	DI: BRIDGE 25A	
11-014 4	TR: 2SB554 PNP (R)	-
11-015 4	TR: 2SD424 NPN (R)	
<u>11-020</u> 4	TR: 2SA1111 PNP	
11-021 4	TR: 2SC2591 NPN	
11-017 4	DI: STV - 3H - Y	
	<u> </u>	
		· :
14		
		•
		1 - 1
12-001 1		
	FUSE: 10A 250V MDA	
12-002 1	THERMOSTAT: 100 DEG	
12-002 1	THERMOSTAT: 100 DEG	
12-002 1	THERMOSTAT: 100 DEG	
12-002 1	THERMOSTAT: 100 DEG	
12-002 1	THERMOSTAT: 100 DEG	
<u>12-002</u> <u>1</u> 12-005 2	THERMOSTAT: 100 DEG	
<u>12-002</u> <u>1</u> 12-005 2	THERMOSTAT: 100 DEG	
<u>12-002</u> <u>1</u> <u>12-005</u> <u>2</u>	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
<u>12-002</u> 1 12-0052	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
<u>12-002</u> <u>1</u> <u>12-005</u> <u>2</u>	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
<u>12-002</u> <u>1</u> <u>12-005</u> <u>2</u>	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
<u>12-002</u> <u>1</u> <u>12-005</u> <u>2</u>	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
12-002 1 12-005 2	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
12-002 1 12-005 2	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	
	THERMOSTAT: 100 DEG SWITCH: POWER (OSLO)	

•

•		
DDEL GFA-1a	DATE 09-12-80 PREVIOUS PAGE 2 OF	3
Biel 50-003	ASSEM. DESC. FINAL ASSEMBLY	
-ART Nº QTY	DESCRIPTION REF. DESIG.	
18-001 1	FUSE HOLDER: BUSS HKP	
18-002 1	RELIEF: HEYCO SR-5KN-4	
18-008 8	INS: TO-220	
-18-007 1	TERM: SMK XQ 2754-01	
18-003 1	CONN: 10-18 GA WAT	
18-027 1	TERM: HHS-863	
18-020 8	INS: TO-3	
18-015 4	BUSHING: HEYCO B-187-125	
18-021 · · · · 2	BUSHING: HEYCO SB-375-4	
4	FEET: 3M SJ-5023 BLK	
19-006 41	SCREW: 6-32 x ½ REV PH BLK	
19-005 2	SCREW: #4 x 5/16 PH	
19-003 6	NUT: PRE6S 10-32-2	
19-011 8	NUT: PRESS 4-40-2	
	SCREW: 10-32 x 2 PHSS BLK	
<u>19-001</u> 4	SCREW: 10-32 x 3/8 PH NP	
19-002 4	WASHER: #10 INT STAR ZP	
<u>19-0 36 4</u>	SCREW: 6-32 x 5/16 PH REV BLK	
19-025 4	STANDOFF: ½ x 7/16 x 6-32 BR NP	
19-032 2	SCREW: 10-32 x 3/4 PH NP	
21-001 1	FAN: HOWARD	
	TIE RAP: 3/4 DIA TY-23-M	
<u></u>	LINE CORD: C - 1248 MESS	
<u></u>		
af ' -		
r		
· / 1 3 g		
Ł		
°° ∲ ⊑		
· •		

.

•							
IDDEL	GFA-la	DATE	09-12-80	PREVIOUS		PAGE 3	OF 3
<u>5</u> M	<u>50-003</u>	ASSEM D	-SC FINA				
	ž 1					·	
		e	·		· · · · · · · · · · · · · · · · · · ·		
	••••						· · · · · · · · · · · · · · · · · · ·
<u>}</u>							
<u></u>					-		
						(
. =						^ <u>,</u>	
		· · · · · · · · · · · · · · · · · · ·					